Attachment I-9: Diversion Channel Analysis – Phase 2



Fargo-Moorhead Metro Feasibility Study

Minnesota Diversion Modeling Results

Computed By: KAH

Date: 4-Sep-08

Revised By: KAH

Date: 28-Dec-09

Diversion Channel

- Analyzed using GeoStudio (SEEP/W & SLOPE/W)
- Cross Sections revised based on Moore's revision on 7/20/09
- 500 ft Bottom Width Analyzed
- Stratigraphy Based on Boring Logs taken by USACE

Elevations

- Ground Surface and Bottom of Channel Elevations Based on Moore Engineering Report, revision 7/20/09
 - * The 3 different capacities (45k, 35k, and 25k CFS) all have same bottom channel elevation, but the channel has different widths.

Spoil Area

- Spoil Embankment Top Width Varies with Depth & Width of Diversion Channel
- Spoil Embankment Height of 10' 10
 Landside Slope 1':10' (Vert/Horz) 0.10
 Diversion Channel Slope 1':7' (Vert/Horz) 0.14

Seepage Analysis

- Only one half of the diversion channel was modeled (1/2 space)
- Model extended to 1750' (~1/3 mile) beyond toe of ditch slope
- Total Head boundary conditions used at the extent of model.
- * Total Head equals ground water elevation observed during drilling
 - * Total Head in sand formation equals observed piezometric level (or if not observed, ground surface elevation)

Diversion Channel Stability

- Slope Stability computed using Spencer's Method with the Optimization function
- Two Factors of Safety's were analyzed for slope stability using entry/exit slip surface
 - * Global Failure is indicated by slip surface initiating above 3/4 of the slope
 - * Localized Failure is indicated by slip surfaces initiating in below 3/4 of the slope and 5' above bottom of channel
- Undrained global failure is indicated by a slip surface initiating above 1/2 of the slope
- Factor of Safety against uplift/heave was calculated for Sections containing a sand seam. Both short and long term Factor of Safety's were computed.

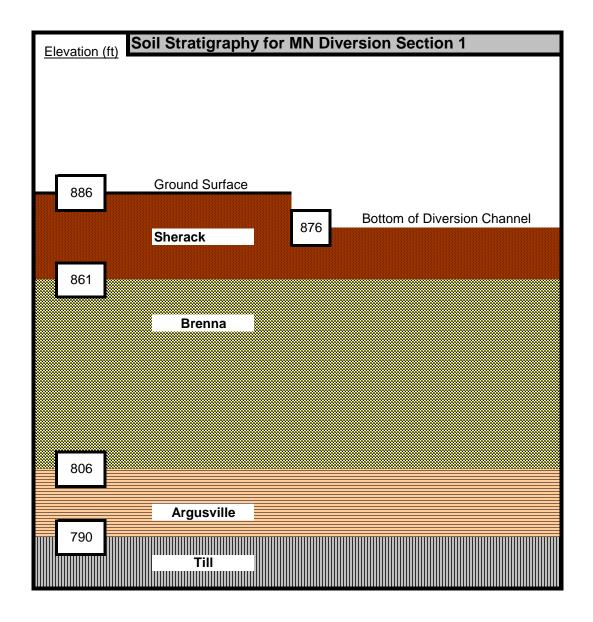
MN Diversion Channel Model Results

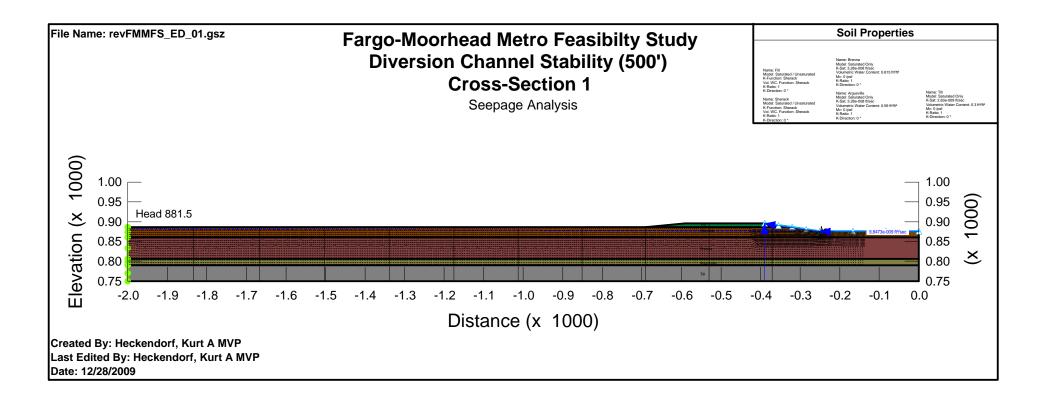
										Factor of Safety															
							Total Seepage into Channel			Uplift	Heave	Long Term / Drained Slope Stability					Short Term / Undrained Slope Stability		Extents for Failure Surface		Surface				
•	Cross- Section	Channel Bottom Width [ft]	Ground Surface Elevatioin [ft]	Water Table Depth [ft]	Channel Elevation [ft]	Elevation of Sand Formation [ft]	Channel Depth [ft]	[ft³/sec]	[gal/day/LF]	Y-Gradient	Total Head in Sand at Bottom of Channel [ft]	Piping	Short Term	Long Term	Global - Circular Opt	Global - Circular	Global Wedge Opt	Global Wedge	Localized Circular Opt			Global Circular	Global	Local	Undrained
	1	500	886	881.5	876		10	9.8473E-09	0.013	0.012		55.56			1.722	1.746			1.887		1.935	1.967	891	881	886
	2	500	911	906.1	882	848	29	3.4786E-06	4.497	0.51	894.676	1.30	1.21	1.79	0.886	0.928			0.386	0.408	1.607	1.693	911	892	902
	3	500	913	906.9	886		27	4.5601E-08	0.059	0.09		7.36			1.201	1.206	1.204	1.321	1.083	1.098	1.325	1.350	914	895	905
	4	500	910	906.6	892	864	18	1.6371E-06	2.116	0.10	893.061	6.80	1.61	17.59	2.689	2.705			2.484	2.536	2.874	3.142	913	899	906

 $v_{\rm sat} = 104$

^{*} Note: No Uplift/Heave was calculated for sections 1 and 3 due to the fact that there was no sand seam or permeable layer.

						_				Factor of Safety														
							Total See Cha	page into nnel				Uplift/	Heave		Long	Term / Drain	ed Slope S	tability		Short Term Slope S		Extents	s for Failure	Surface
Cross- Section		Ground Surface Elevatioin [ft]	Water Table Depth [ft]	Channel Elevation [ft]	Elevation of Sand Formation [ft]	Channel Depth [ft]	[ft ³ /sec]	[gal/day/LF]	Y-Gradient	Total Head in Sand at Bottom of Channel [ft]	Piping	Short Term	Long Term	Global - Circular Opt	Global - Circular	Global Wedge Opt	Global Wedge	Localized Circular Opt			Global Circular	Global	Local	Undrained
2	500	911	906.1	882	848	29	3.7446E-06	4.840	0.44	893.501	1.52	1.25	1.97	1.390	1.577			1.041	1.138	2.189	2.662	911	892	902
3	500	913	906.9	886		27	4.4353E-08	0.057	0.08		8.70			1.370	1.463	1.434	1.581	1.452	1.503	1.467	1.511	914	895	905





¹ Study 00')

Soil Properties

Model: Saturated Only K-Sat: 3.28e-008 ft/sec Name: Fill Model: Saturated / Unsaturated

K-Function: Sherack Vol. WC. Function: Sherack

K-Ratio: 1 K-Direction: 0 °

Name: Sherack Model: Saturated / Unsaturated

K-Function: Sherack Vol. WC. Function: Sherack K-Ratio: 1

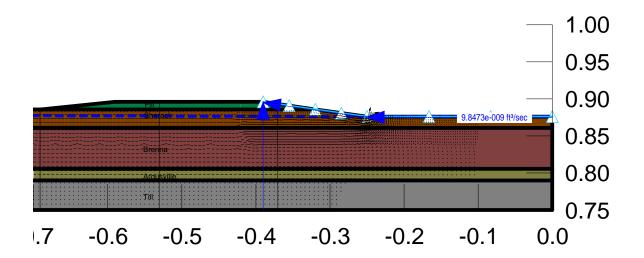
K-Direction: 0 °

Volumetric Water Content: 0.615 ft3/ft3 Mv: 0 /psf

K-Ratio: 1 K-Direction: 0 °

Name: Argusville Model: Saturated Only K-Sat: 3.28e-008 ft/sec Volumetric Water Content: 0.59 ft3/ft3

Mv: 0 /psf K-Ratio: 1 K-Direction: 0 ° Name: Till Model: Saturated (K-Sat: 2.63e-009 f Volumetric Water Mv: 0 /psf K-Ratio: 1 K-Direction: 0 °

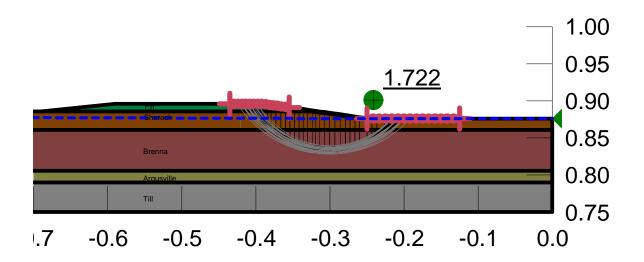


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Soil Properties

Name: Fill Unit Weight: 118 pcf Cohesion: 0 psf Phi: 28 ° Name: Brenna Unit Weight: 103 pcf Cohesion: 0 psf Phi: 13 °

Name: Sherack Unit Weight: 118 pcf Cohesion: 0 psf Phi: 28 ° Name: Argusville Unit Weight: 106 pcf Cohesion: 0 psf Phi: 15 ° Name: Till Unit Weight: 122 pcf Cohesion: 0 psf Phi: 31 °



Study00')

Soil Properties

Name: Fill Unit Weight: 118 pcf Cohesion: 0 psf Phi: 28 °

Name: Sherack

Cohesion: 0 psf

Phi: 28 °

Unit Weight: 118 pcf

Unit Weight: 103 pcf Cohesion: 0 psf Phi: 13 ° Name: Argusville Unit Weight: 106 pcf

Cohesion: 0 psf

Phi: 15 °

Name: Brenna

Name: Till Unit Weight: 122 pcf Cohesion: 0 psf Phi: 31 °

1.00 0.95 0.90 0.85 0.80 0.75 0.75

Study00')

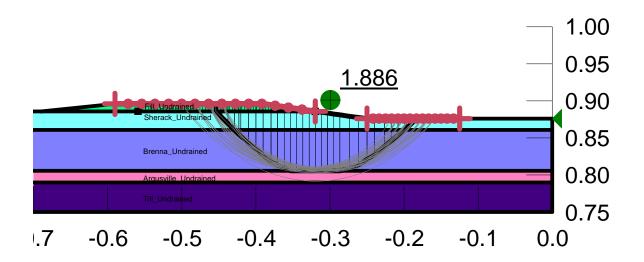
Soil Properties

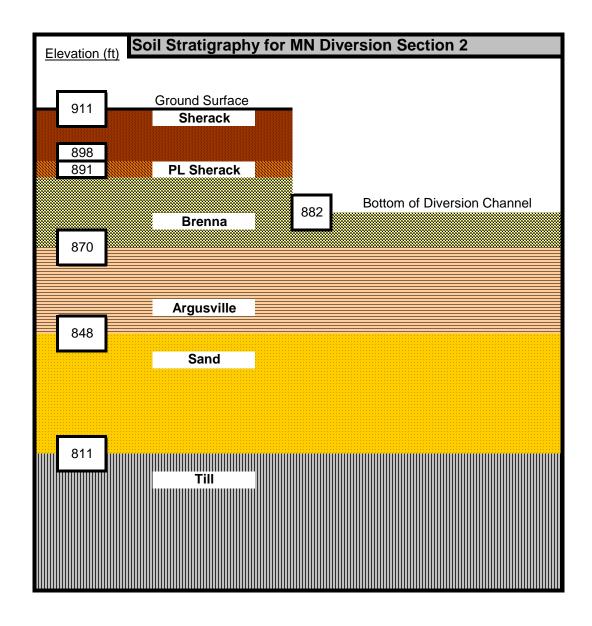
Name: Fill_Undrained Unit Weight: 118 pcf Cohesion: 1400 psf

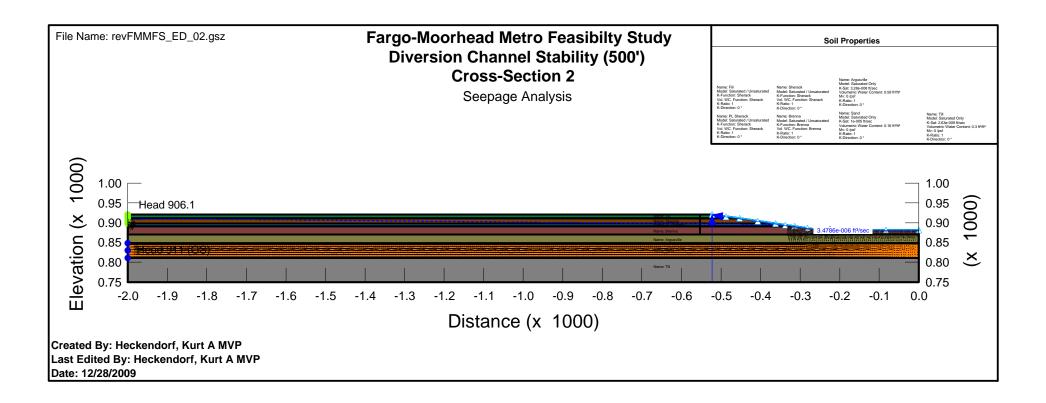
Name: Brenna_Undrained Unit Weight: 103 pcf Cohesion: 650 psf

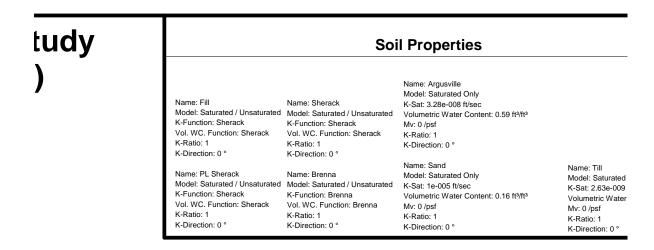
Name: Sherack_Undrained Unit Weight: 118 pcf Cohesion: 1400 psf

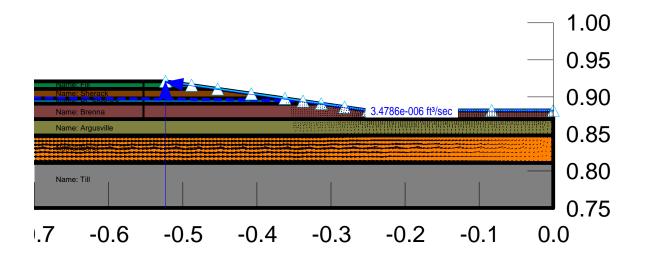
Name: Argusville_Undrained Unit Weight: 106 pcf Cohesion: 825 psf Name: Till_I Unit Weight Cohesion: 1

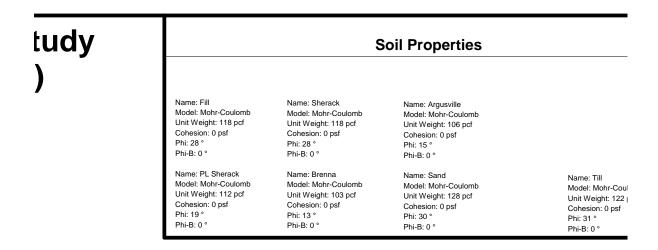


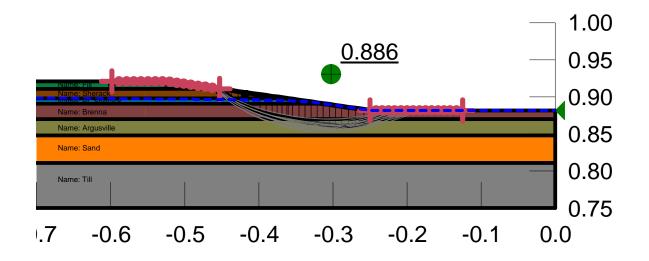


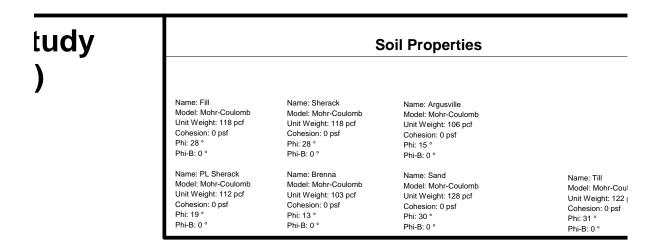


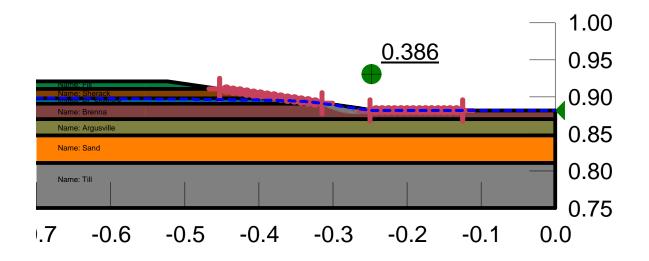


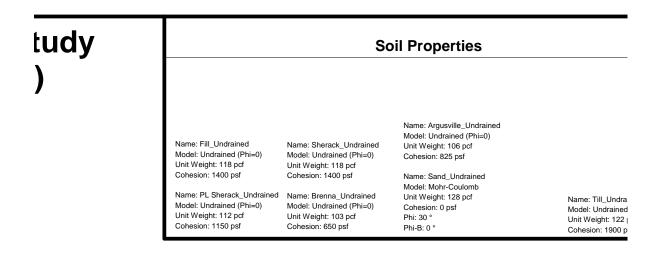


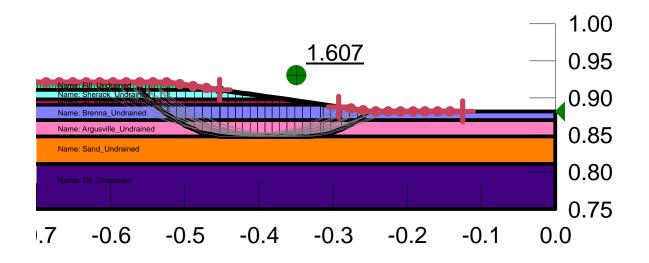


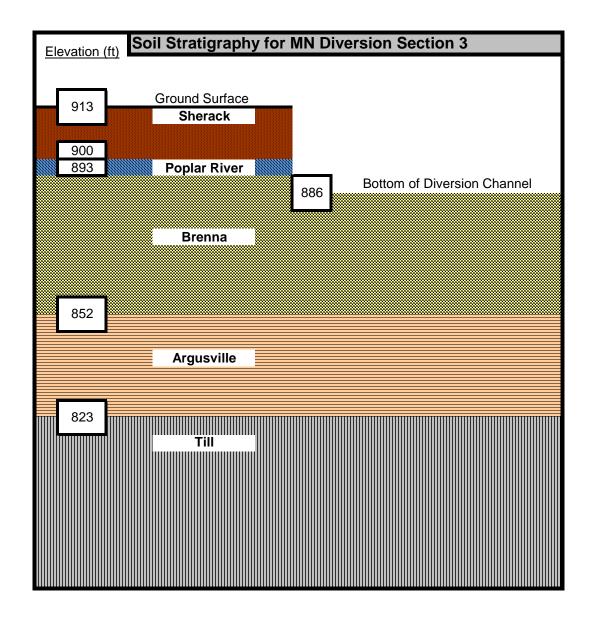


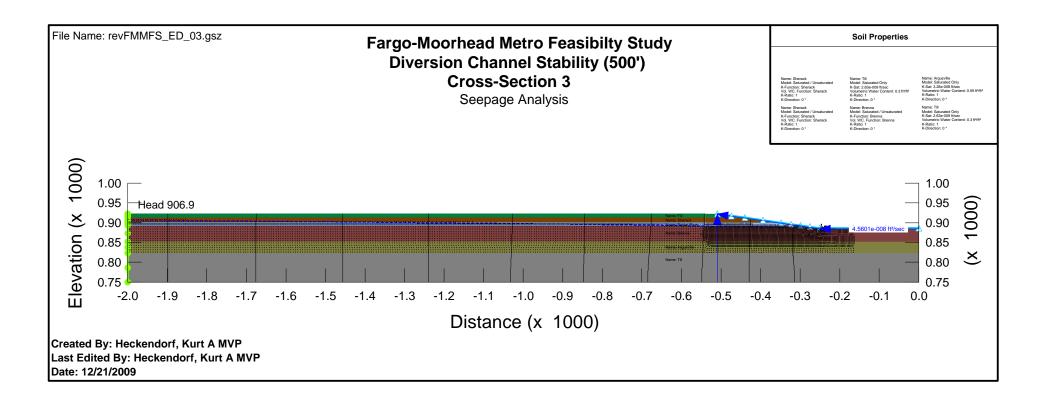


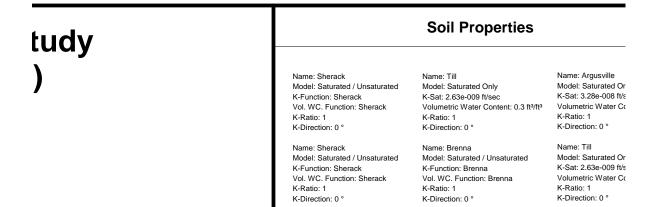


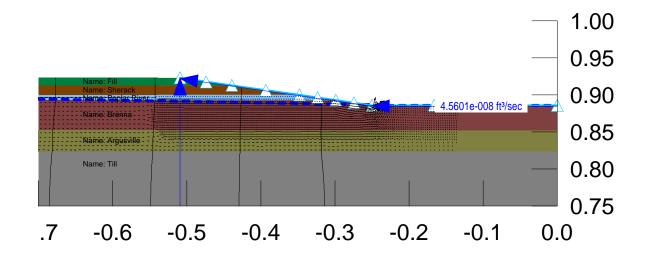


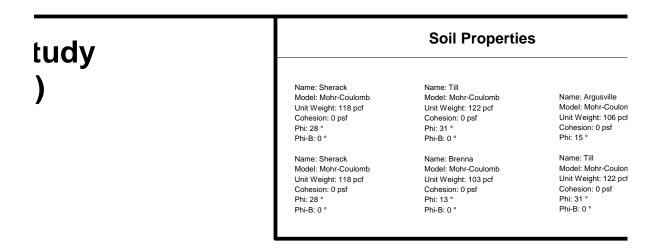


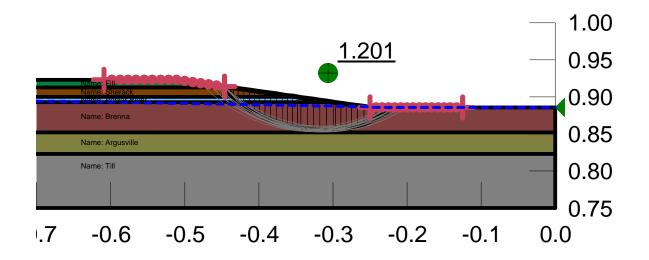


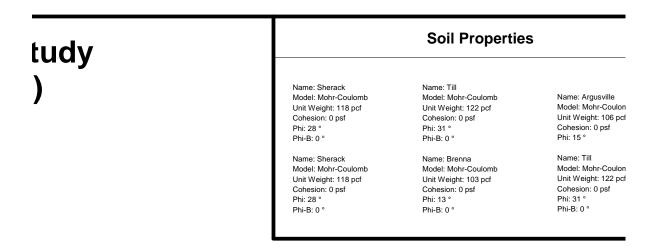


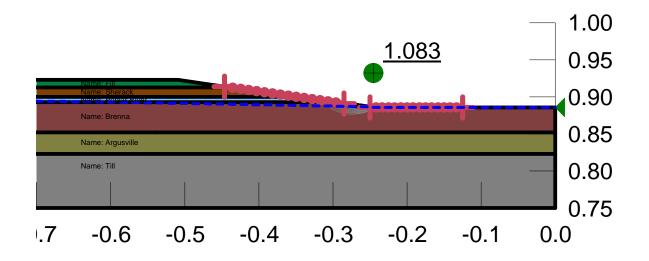


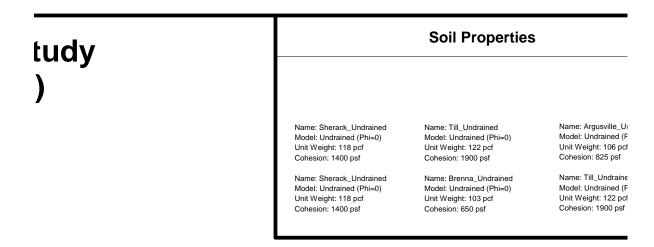


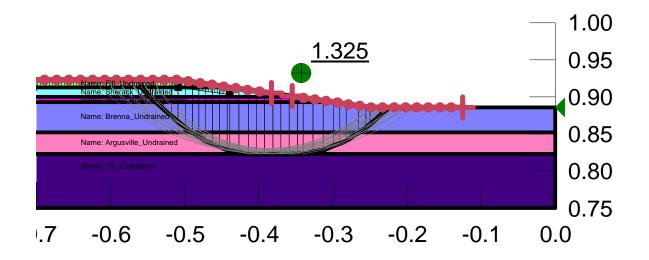


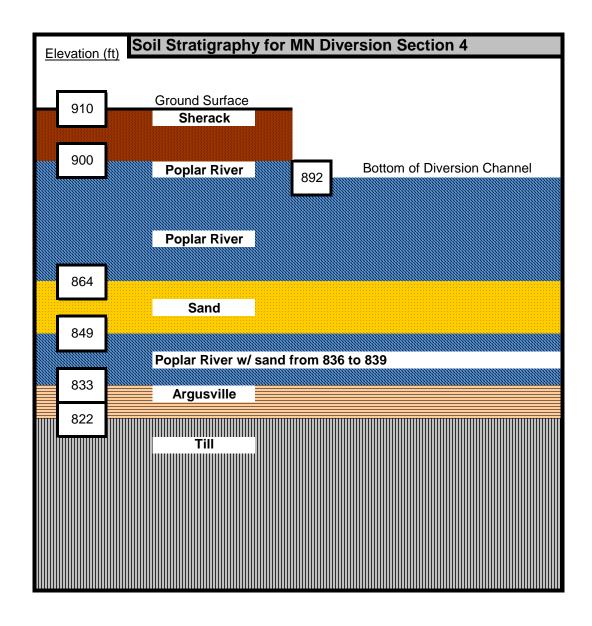


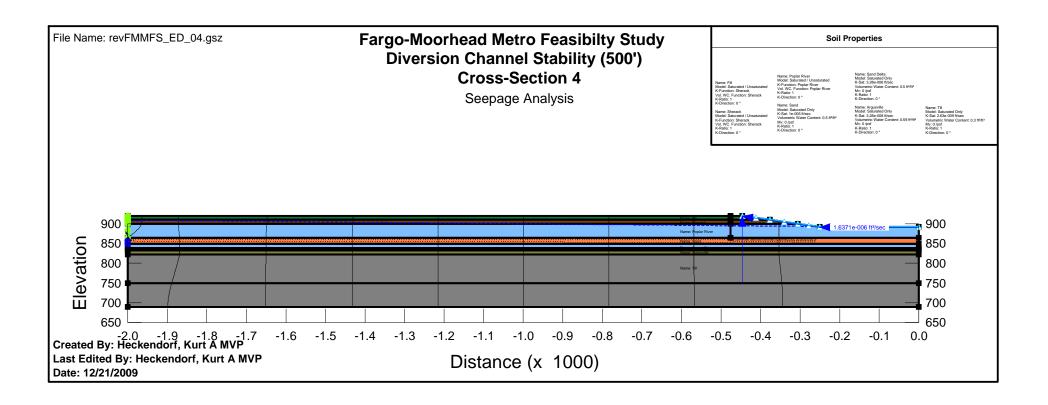


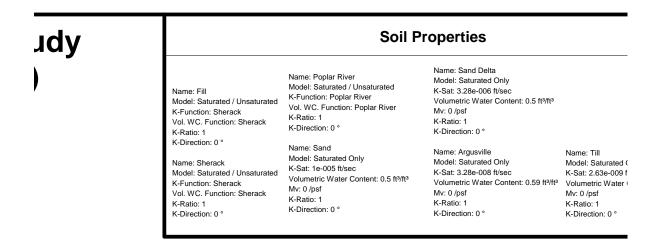


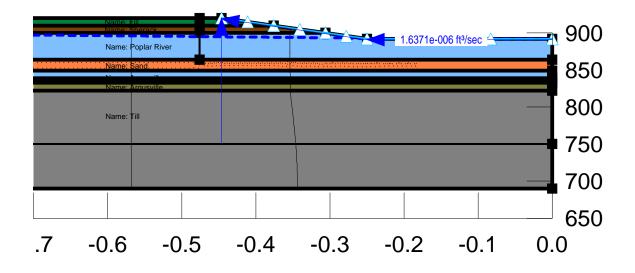


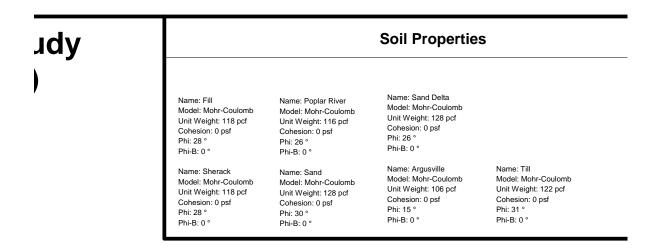


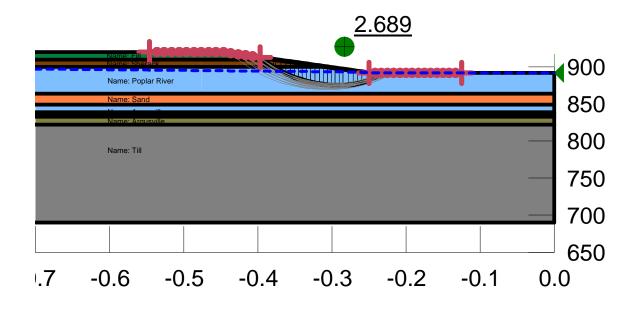


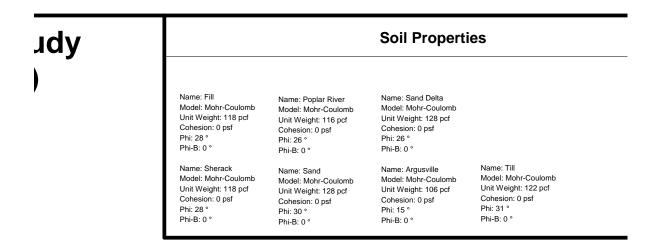


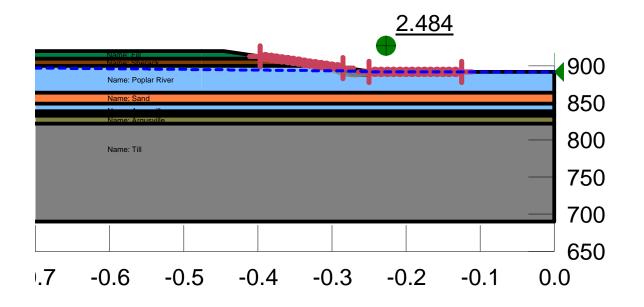


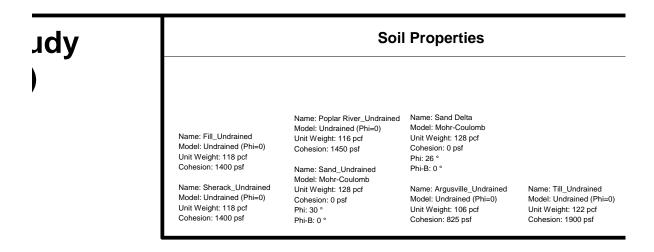


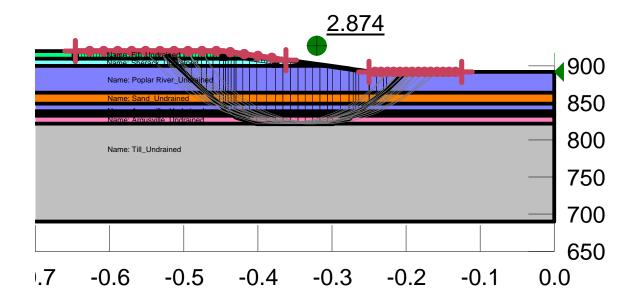








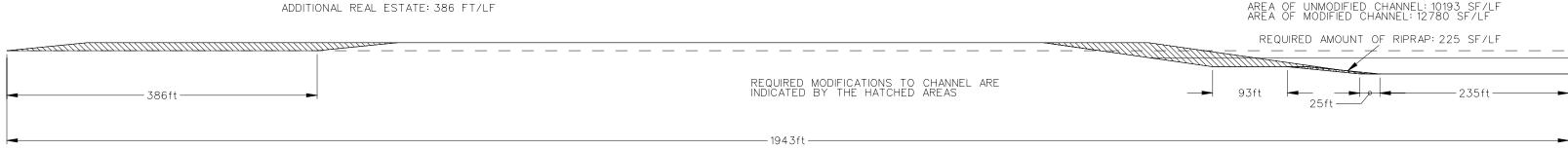


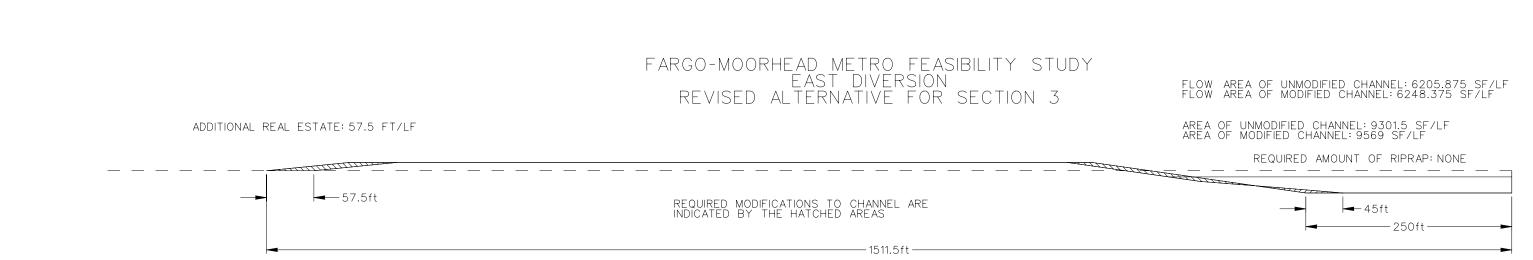


FARGO-MOORHEAD METRO FEASIBILITY STUDY EAST DIVERSION REVISED ALTERNATIVE FOR SECTION 2

FLOW AREA OF UNMODIFIED CHANNEL: 6400 SF/LF FLOW AREA OF MODIFIED CHANNEL: 7817 SF/LF

AREA OF UNMODIFIED CHANNEL: 10193 SF/LF AREA OF MODIFIED CHANNEL: 12780 SF/LF







Fargo-Moorhead Metro Feasibility Study

Minnesota Diversion Alternative Configurations

Computed By: KAH

Date: 4-Sep-08

Revised By: KAH

Date: 19-Mar-10

Due to seepage & slope stability concerns, the configuration of the diversion channel had to be modified

Based on discussion with Mike Lesher (3 SEP 09), the configuration of the channel could be modified but the flow area should be kept the same

Elevations for the ground surfce, channel bottom, and water surface profile along the diversion were obtained from Moore Enginnering's MN Short Diversion calculations

Summary of Required Modifications

		MN Short Diversion				Quantities Based on 1/2 of the Diversion Channel													
Section	n	Location (FT)	Ground Elevation (FT)	Bottom of Channel (FT)	Water Profile (FT)	Required Modification		Modified Channel Width (FT)	70	Ü		% Increase		Modified Excavation (SF/LF)	% Increase	Original Real Estate	Modified Real Estate (FT)	% Increase	Required Riprap (SF/LF)
		(FT)	(FT)	(ГТ)				(FT)		(SF/LF)	(SI/LI)		(SF/LF)	(SF/LF)		(F1)	(ГТ)		(SF/LF)
2		69000	911	882	902	Slope in Brenna flatten to 1V:10H, 9 FT up; 25 FT wide riprap berm added to slope cut in Brenna; 118 FT bench	250	235	6.0%	6,400	7,817	22.13%	10,193	12,780	25.38%	1,557	1,943	24.79%	225
3		96000	913	886	905.5	Slope in Brenna flatten to 1V:12H, 14 FT up	250	205	18.0%	6,206	6,248	0.68%	9,302	9,569	2.88%	1,454	1,512	3.95%	0

	MN Short Diversion					Quantities Based on the FULLDiversion Channel												
Section	Location	Elevation	Bottom of Channel	Profile	Required Length of Modification	Original Channel Width	Channel Width	0/2	Original Flow Area	Modified Flow Area	% Increase	Original Excavation	Modified Excavation	% Increase	Original Real Estate	Modified Real Estate	% Increase	1 1
	(FT)	(FT)	(FT)	(FT)	(FT)	(FT)	(FT)		(SF/LF)	(SF/LF)		(CY)	(CY)		(ACRE)	(SF)		(CY)
2	69000	911	882	902	16,000	500	470	6.0%	12,800	15,633	22.13%	12,080,593	15,146,667	25.38%	1,144	1,427	24.79%	266,667
3	96000	913	886	905.5	73,500	500	410	18.0%	12,412	12,497	0.68%	50,641,500	52,097,889	2.88%	4,907	5,101	3.95%	0

Mod Type	Start	End	Length
3	35,500	65,000	29,500
2	65,000	81,000	16,000
3	81,000	125,000	44,000

89,500 66.9%

22% 12% 33%

Total Diversion Channel Length 133,745 44,245

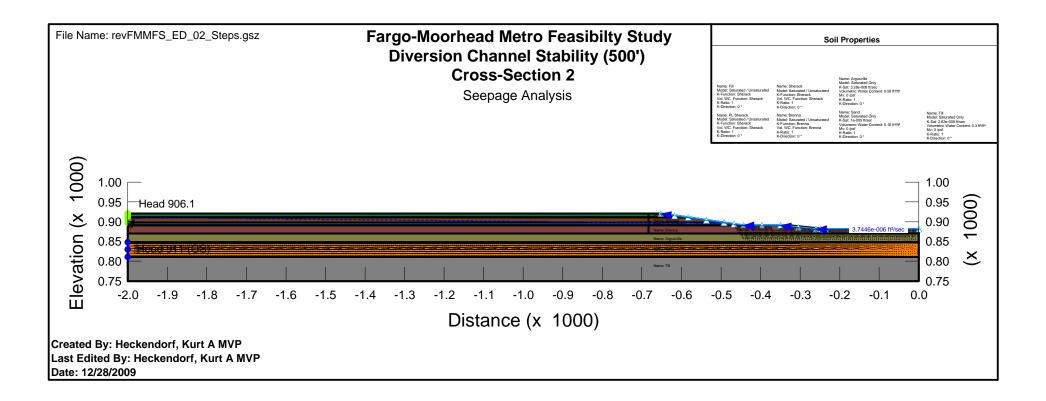
We	Weighted Average for Increased Quantities											
	Length	Increased Excavation	Increased Real Estate	Required Riprap (CY)								
No Mod	44,245	0	0	0								
Mod 2	16,000	25.4%	24.8%	266,667								
Mod 3	73,500	2.9%	4.0%	0								
Total Length	133,745											
Weighted Av	erage Increase	4.6%	5.1%	266,667								

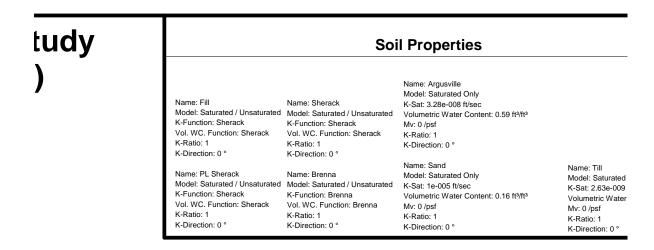


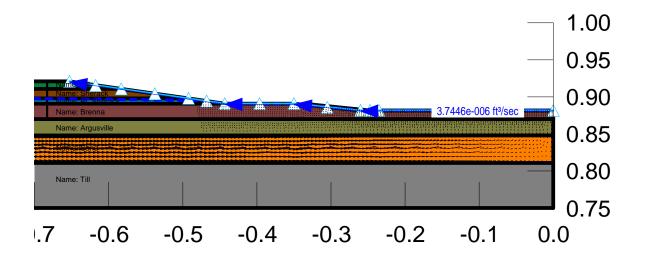
Fargo-Moorhead Metro Feasibility Study Minnesota Diversion Alternative Lengths

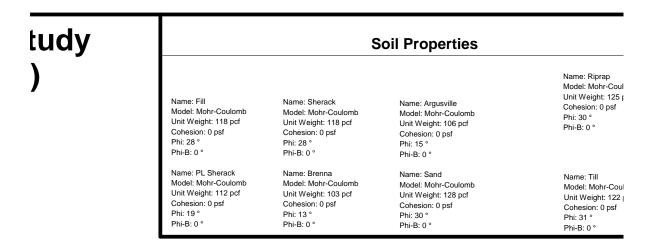
Revised By: Date: Computed By: KAH Date: 4-Sep-09

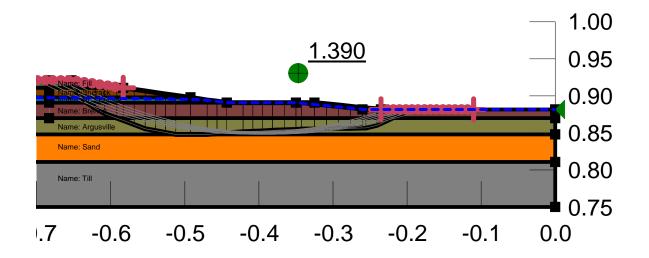
Sounding	Location	Elevation	Bottom Elevation	Top of	Sherack	Top of	Brenna		Notes
09-11C	0	888.2	875	-6	882.2	-25	863.2		
09-27C	3400	886.2	875	-5	881.2	-29	857.2		
09-28C	9000	888.4	876	-8	880.4	-30	858.4		
09-30C	15000	892.4	877	-6	886.4	-33	859.4		
09-29C	20100	891	877	-6	885	-38	853		
09-12C	24500	894	878	-2	892	-29.5	864.5		
09-31C	30100	895.8	878	-3	892.8	-26	869.8		
09-35C	35500	902.4	878	-4	898.4	-28	874.4	Questionable	Start Mod #3 at 35500
09-33C	50000	907.3	880	-2	905.3	-32	875.3	Questionable	
09-37C	57100	909.7	880	-2	907.7	-17	892.7	Brenna exposed	
09-38C	62500	907.8	881		907.8	-23	884.8	Brenna exposed	Continue with Mod #3 to 65000
09-14C	67600	913.1	882	-3	910.1	-28	885.1	Sand below	Start Mod #2 at 65000
09-39C	73000	910.5	882		910.5	-17	893.5	Brenna exposed	
09-40C	78700	912.8	883	-3	909.8	-20	892.8	Sand below	Continue with Mod #2 to 81000
09-42C	84100	912.2	884		912.2	-15	897.2	Brenna exposed	Start Mod #3 at 81000
09-43C	90000	912.7	885		912.7	-17	895.7	Brenna exposed	
09-15C	95000	914.9	886	-3.5	911.4	-14.5	900.4	Brenna exposed	
09-44C	100000	915.8	887		915.8	-15	900.8	Brenna exposed	
09-45C	108000	920.4	888		920.4	-19	901.4	Brenna exposed	
09-46C	114000	916.5	890		916.5	-18	898.5	Brenna exposed	
09-48C	120000	912.7	891		912.7	-20	892.7	Brenna exposed	Continue with Mod #3 to 125000
09-50C	130250	913.4	893		913.4	-26	887.4		
09-51C	133000	911.8	893		911.8	-25	886.8		

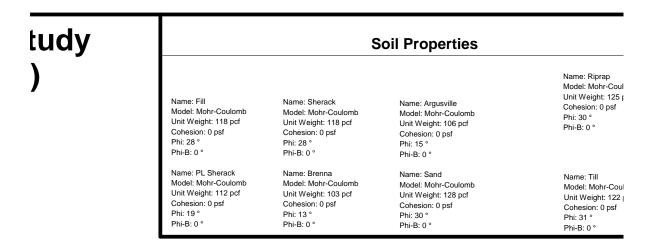


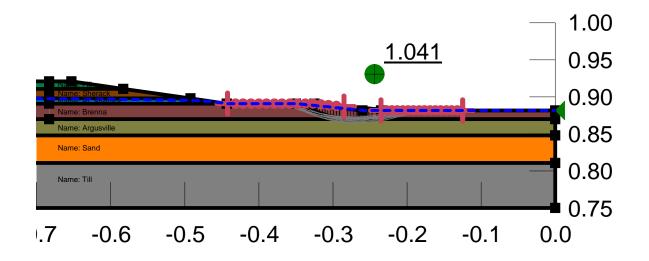


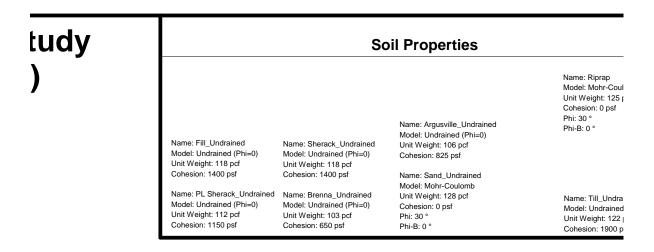


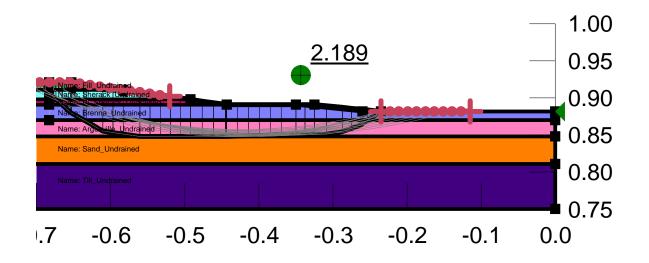


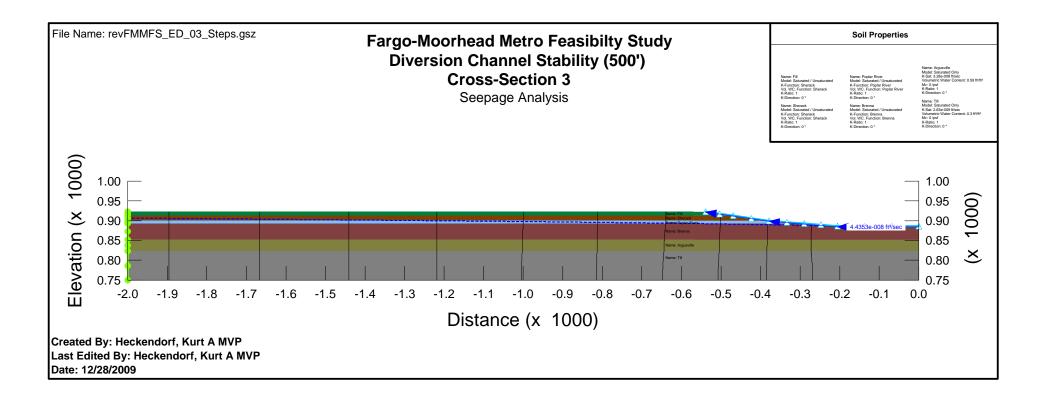














Soil Properties

Model: Saturated / Unsaturated

Vol. WC. Function: Poplar River

Name: Fill Model: Saturated / Unsaturated K-Function: Sherack Vol. WC. Function: Sherack K-Ratio: 1 K-Direction: 0 °

Name: Sherack Model: Saturated / Unsaturated K-Function: Sherack Vol. WC. Function: Sherack K-Ratio: 1 K-Direction: 0° K-Direction: 0 °

Name: Brenna
Model: Saturated / Unsaturated
K-Function: Brenna
Vol. WC. Function: Brenna
K-Ratio: 1

Name: Poplar River

K-Ratio: 1

K-Direction: 0 °

K-Function: Poplar River

Name: Argusville Model: Saturated Or K-Sat: 3.28e-008 ft/s Volumetric Water Cc Mv: 0 /psf K-Ratio: 1 K-Direction: 0 °

Name: Till Model: Saturated Or K-Sat: 2.63e-009 ft/s Volumetric Water Co My: 0 /psf K-Ratio: 1 K-Direction: 0 °

