SHEYENE AQUADUCT STRUCTURE

Client Name:	**U.S. ARMY CORPS OF ENGINEERS**	**Design By:**	**MBI**
Project Name:	**FARGO – MOORHEAD METRO FLOOD RISK MANAGEMENT PROJECT, FEASIBILITY STUDY, PHASE 4**	**Review By:**	
Work Describtion:	**Sheyenne Aquaduct Structure - Retaining Walls**	**Date:**	**2/10/2011**
	Panel C	**Job #:**	**34091004**
File Path:	P:\Mpls\34 ND\09\34091004 Fargo Moorhead Metropolitan Feas. Study\WorkFiles_Phase4\070 Structural\Aqueducts\Sheyene\[34091004 PH4 Sheyene Retaining Walls Panel C.xlsx]Case 6		
REF.	**1**		
	2		

ID#	**Case 1**	**Case 2**	**Case 3**	**Case 4**	**Case 5**	**Case 6**
Name	100 yr. flood	100 yr. flood + ice	500 yr. flood	T.O. Levee	Normal flow + ice	Construction
Load Category	Usual	Unusual	Unusual	Extreme	Usual	Unusual
Tributary - Water El. (ft)	914.56	914.56	914.67	916	903.24	**NA**
Diversion - Head Water El. (ft)	902.12	902.12	903.32	916	**NA**	**NA**
Diversion - Tail Water El. (ft)	901.91	901.91	903.06	916	**NA**	**NA**
Tributary - T.O. Wall El. (ft)	916					
Tributary - T.O. Deck L.P. El.(ft)	898.7					
Tributary - T.O. Deck H.P. El.(ft)	900.7					
Diversion - T.O. Mat El. (ft)	889.68					
Tributary - Deck Slab thickness @ L.P. (ft)	2					
Tributary - Deck Slab thickness @ H.P. (ft)	4					
Diversion - Mat Slab thickness (ft)	4					
Tibutary - Water height (ft)	**15.86**	**15.86**	**15.97**	**17.3**	**4.54**	**NA**
Diversion - Head Water height (ft)	**12.44**	**12.44**	**13.64**	**26.32**	**NA**	**NA**
Ice	**NA**	2ft Ice	**NA**	**NA**	2ft Ice	**NA**
Ice Load	**NA**	10 kips/ft	**NA**	**NA**	10 kips/ft	**NA**
Ice Laod El. (ft)	**NA**	**914.56**	**NA**	**NA**	**903.24**	**NA**
Uplift @ HW (ft)	**16.44**	**16.44**	**17.64**	**30.32**	**NA**	**NA**
Uplift @ TW (ft)	**16.23**	**16.23**	**17.38**	**30.32**	**NA**	**NA**
Pile Condition	**Undrained**	**Undrained**	**Undrained**	**Undrained**	**Drained**	**Undrained**
Load Category	**Usual**	**Unusual**	**Unusual**	**Extreme**	**Usual**	**Unusual**
Safety Factors	2	1.5	1.5	1.15	2	1.5
Allwable Lateral Capacity (tons)	**18**	**20.5**	**20.5**	**24**	**11.5**	**20.5**
Allowable Pile Capacity (tons) - Axial	**61.95**	**82.60**	**82.60**	**107.74**	**36.525**	**82.60**
Allowable Pile Capacity (tons) - Uplift	**38.65**	**51.53**	**51.53**	**67.22**	**5.9**	**51.53**

Pile Capacity	**Ultimate Axial Capacity (kips)**	**Allowable Lateral Capacity (kips)**		
		0.5" (Usual)	**0.67" (Unusual)**	**0.875" (Extreme)**
Undrained - Axial	247.8	36	41	48
Undrained - Uplift	154.6			
Drained - Axial	146.1	23	29	36
Drained - Uplift	23.6			

BARR ENGINEERING			DATE	2/11/2011	SHEET NO.	
			PROJECT NAME	FARGO – MOORHEAD METRO FLOOD RISK MANAGEMENT PROJECT, FEASIBILITY STUDY, PHASE 4		
COMPUTED	CHECKED	SUBMITTED	PROJECT NUMBER	34091004		
MBI 2/11/11		MBI	SUBJECT	Sheyenne Aquaduct Structure - Retaining Walls Panel C		

Monolith Structure

ITEM		UNIT	QUANITY	UNIT COST	TOTAL Cost
FURNISH HP14x73 WALL PILING		LF	2,112	0	$0
INSTALL HP14x73 WALL PILING		LF	2,112	0	$0
PILE TEST, 54.0 ft	Long	EA	4	0	$0
FOOTING CONCRETE		CY	282	0	$0
	Forming	SF	871		
STEM CONCRETE		CY	314	0	$0
	Forming	SF	4,490		
STEEL REINFORCEMENT		LB	117,700	0	$0
WALL RAILING		LF	81	0	$0
SHEET PILE CUT-OFF WALL		SF	1,610	0	$0
					$0

Structure Length = 80.5 ft

No. piles = 48 Each

Length = 44 ft

Note: HP14x73 pile used for design, use HP14x73 to allow for corrosion

LENGTH

(FRONT & Back FACE) 10 FT

Native Soil has low permeability assume cut-off minimal to prevent scour

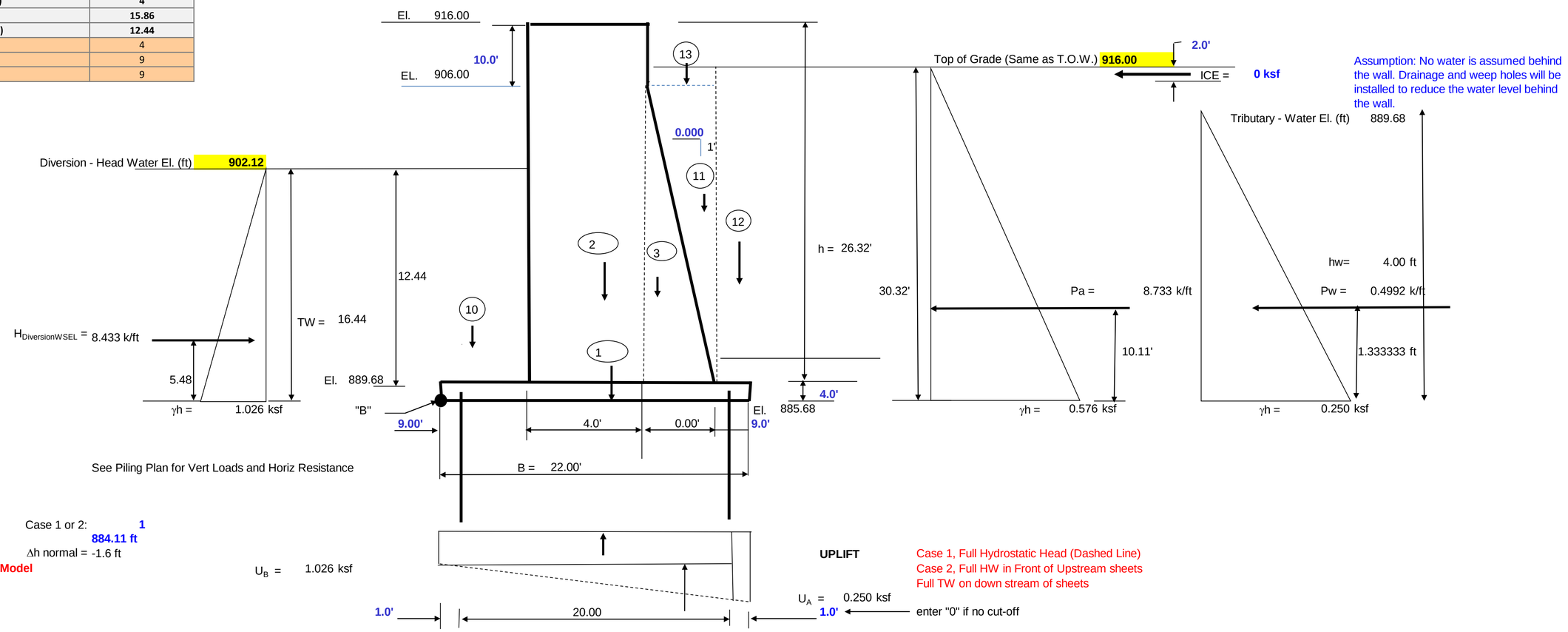
BARR ENGINEERING			DATE	2/11/2011	SHEET NO.
			PROJECT NAME	FARGO – MOORHEAD METRO FLOOD RISK MANAGEMENT PROJECT, FEASIBILITY STUDY, PHASE 4	
COMPUTED	CHECKED	SUBMITTED	PROJECT NUMBER	34091004	
MBI 2/11/11		MBI	SUBJECT	Sheyenne Aquaduct Structure - Retaining Walls Load Cases: Case 1 100 yr. flood Panel C	

ID#	Case 1
Name	100 yr. flood
Load Category	Usual
Tributary - Water El. (ft)	914.56
Diversion - Head Water El. (ft)	902.12
Diversion - Tail Water El. (ft)	901.91
Tributary - T.O. Wall El. (ft)	916
Tributary - T.O. Deck L.P. El.(ft)	898.7
Tributary - T.O. Deck H.P. El.(ft)	900.7
Diversion - T.O. Mat El. (ft)	889.68
Tributary - Deck Slab thickness @ L.P. (ft)	2
Tributary - Deck Slab thickness @ H.P. (ft)	4
Diversion - Mat Slab thickness (ft)	4
Tibutary - Water height (ft)	15.86
Diversion - Head Water height (ft)	12.44
Wall Thickness (ft)	4
Toe (Ft)	9
Heel (ft)	9

File:

MN State Building Codes
Frost Depth = **5.0 ft** provide min frost ftg protection during Dec, Jan, Feb, March
Water El. = **903.24 ft** DEC, JAN, FEB Mean Water Elevation

Non-Overflow Section **Length = 80.5 ft**
Stepped Ftg Ls = **2.0 ft** overlap distance at stepped ftg



See Piling Plan for Vert Loads and Horiz Resistance

Case 1 or 2: **1**
Normal Water Level, El. **884.11 ft**
Δh normal = -1.6 ft
See Geotechnical seepage Model

U_B = 1.026 ksf

UPLIFT
Case 1, Full Hydrostatic Head (Dashed Line)
Case 2, Full HW in Front of Upstream sheets
Full TW on down stream of sheets

U_A = 0.250 ksf
1.0' ← enter "0" if no cut-off

Vertical Loads	Section	L ft	W ft	H ft	γ kcf	shape	V K	arm ft	Mv ft-k
Ftg concrete	1	80.5	22.00	4.00	0.15	rec	1062.6	11.00	11,688.6
Stem	2	80.5	4.00	26.32	0.15	rec	1271.3	11.00	13,983.8
Batter	3	80.5	0.00	16.32	0.15	tri	0.0	13.00	0.0
					D.L. Concrete	ΣVc =	**2333.9**	ΣM_V =	**25,672.4**

← CONSTANT FOR ALL LOAD CASES

T.W on ftg Stem	10	80.5	9.00	12.44	0.0624	rec	562.4	4.50	2,530.8
H.W. on Stem Slope	11	80.5	0.00	16.32	0.12	tri	0.0	13.00	0.0
H.W. Above Slope	13	80.5	0.00	10.00	0.12	rec	0.0	13.00	0.0
Soil on Footing	12s	80.5	9.00	26.32	0.0626	rec	1193.7	17.50	20,889.9
H.W. on Footing	12w	80.5	9.00	0.00	0.0624	rec	0.0	17.50	0.0
					D.L. Water	ΣVw =	**1756.1**	ΣM_V =	**23,420.7**

Uplift Loads		L ft	W ft	Pressure ksf		U K	arm ft	Mu ft-k
	U_B	80.5	22.00	1.026	rec	-1816.8	11.00	-19,985
	U_A	80.5	22.00	-0.776	tri	687.4	14.67	10,081
					ΣU =	**-1129.4**	ΣM_U =	**-9,903**

BARR ENGINEERING			DATE	2/11/2011	SHEET NO.	
			PROJECT NAME	FARGO – MOORHEAD METRO FLOOD RISK MANAGEMENT PROJECT, FEASIBILITY STUDY, PHASE 4		
COMPUTED	CHECKED	SUBMITTED	PROJECT NUMBER	34091004		
MBI		MBI	SUBJECT	Sheyenne Aquaduct Structure - Retaining Walls		
2/11/11				Load Cases: Case 1 100 yr. flood	Panel C	

Horizontal Loads

	L	H	Pressure		**ICE**	arm	**Mu**
	ft	ft	ksf		K	ft	ft-k
ICE	80.5	2.00	0.00	rec	0.0	29.32	0.0

	L	Force		**H**	arm	**Mw**
	ft	k/ft		K	ft	ft-k
SOIL	80.5	-8.733		-703.04	10.11	-7105.36

Water Loads

H_{TW}	80.5	8.433	tri	678.82	5.48	3719.93
H_{HW}	80.5	-0.499	tri	-40.19	1.33	-53.58
			ΣWater =	**638.63**	ΣM_W =	**-3439.0**

Overturning Moments	$\Sigma M_{OT} = M_U + M_W + M_{ICE}$ =	-13342	kip-ft
Resisting Moments	$\Sigma M_R = M_V$ =	49093	kip-ft
Sum of Moments	$\Sigma Mnet = M_R + M_{OT}$ =	**35,751**	kip-ft
Sum of Vertical Forces	P = Conc + Water + Uplift =	**2,961**	kips
Sum of Horizontal Forces	H = Σhorizontal	**-64**	kips

Location of Resultant	Xr = ΣM / P =	12.08	ft from Toe
	e = B/2 - Xr =	(1.08)	ft
	B/6 =	3.667	ft

CONCRETE QUANTITIES

			forming	
Ftg conc:	269	cy (includes stepped)	871	sf
Stem Conc:	314	cy	4490	sf
Total =	583			

STEEL REINFORCEMENT: (assumed)

		Bar #	Spacing		Length	# of bars	Total wt		
a) Footing			in	LB /ft	ft	ea	lb		
Top mat	Transverse:	9	6	3.40	21.5	165	12,062		
	Longitudinal:	9	6	3.40	82	44	12,267		
Bot mat	Transverse:	9	6	3.40	21.5	165	12,062		
	Longitudinal:	9	6	3.40	82	44	12,267		
								cy	**LB/cy**
							48,657	269	180.9572727
b) Skin Reinf. On Monolith									
Vert Face	Vertical	9	6	3.40	25.82	161	14,134	28,267.74	
	Longitudinal:	9	6	3.40	80	52	14,144	28,288.00	
Top Face	Transverse:	9	6	3.40	3.5	161	1,916		
	Longitudinal:	9	6	3.40	80	8	2,176		
Dowels	Vertical I.F.	9	6	3.40	25.8	161	14,134		
	Vertical O.F.	9	6	3.40	25.8	161	14,134		
								cy	**LB/cy**
							60,638	314	193.1805169
						Σ =	**109,295**		
	Lap Splices (long. Bars)	9	6	3.40	8	309	8,405		
						Σ Bar Wt=	117,700	lb	

FORCES AT THE BOTTOM OF THE STEM

Diversion Face	H	γ	Pbase	**V**	arm	**Mv**
	ft	kcf		K	ft	ft-k
Diversion WSEL	12.44	**0.0624**	0.776256	4.828	4.147	20.0214
Tributary SEL =	26.32	**0.019**	0.50008	6.581	8.773	57.73777
Tributary WSEL =	0.00	**0.0624**	0	0.000	0.000	0
Sum				6.581		57.73777
Net Forces				1.753		37.71637

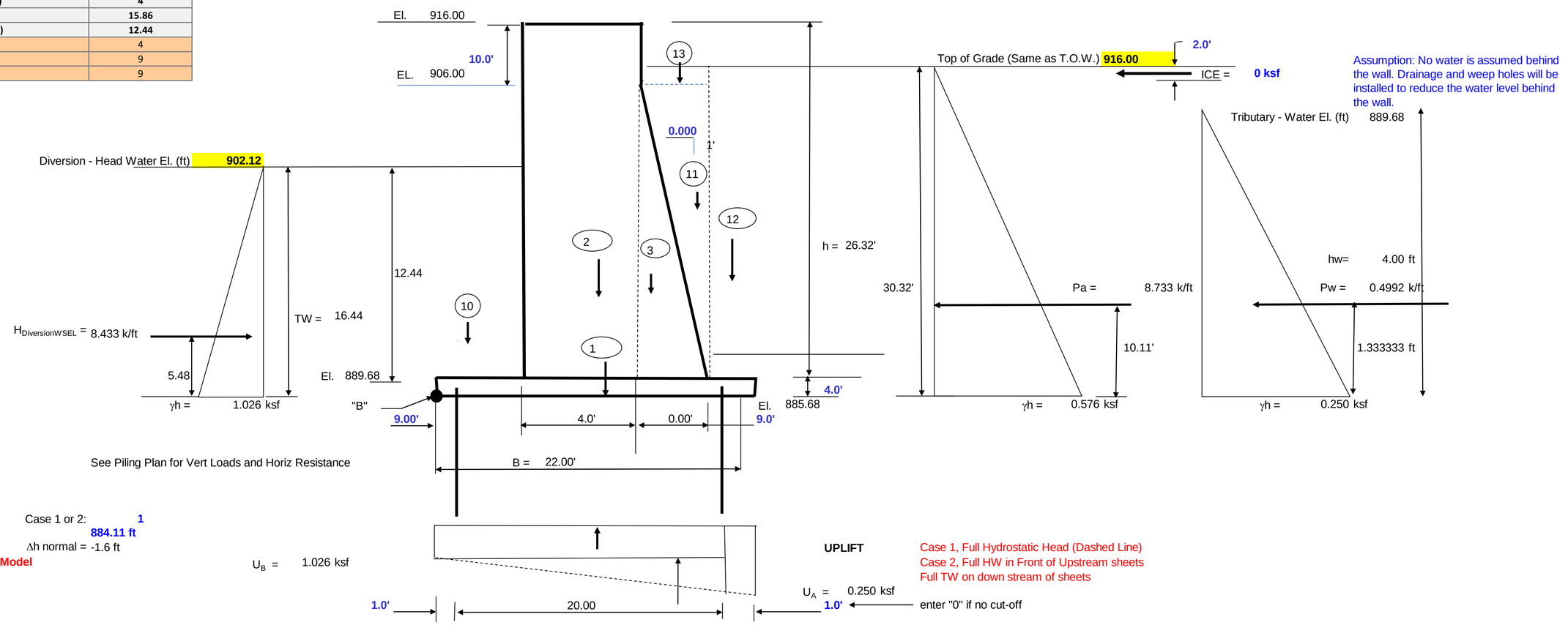
BARR ENGINEERING			DATE	2/11/2011	SHEET NO.
			PROJECT NAME	FARGO – MOORHEAD METRO FLOOD RISK MANAGEMENT PROJECT, FEASIBILITY STUDY, PHASE 4	
COMPUTED	CHECKED	SUBMITTED	PROJECT NUMBER	34091004	
MBI 2/11/11		MBI	SUBJECT	Sheyenne Aquaduct Structure - Retaining Walls Load Cases: Case 2 100 yr. flood + ice Panel C	

ID#	Case 2
Name	100 yr. flood + ice
Load Category	Unusual
Tributary - Water El. (ft)	914.56
Diversion - Head Water El. (ft)	902.12
Diversion - Tail Water El. (ft)	901.91
Tributary - T.O. Wall El. (ft)	916
Tributary - T.O. Deck L.P. El.(ft)	898.7
Tributary - T.O. Deck H.P. El.(ft)	900.7
Diversion - T.O. Mat El. (ft)	889.68
Tributary - Deck Slab thickness @ L.P. (ft)	2
Tributary - Deck Slab thickness @ H.P. (ft)	4
Diversion - Mat Slab thickness (ft)	4
Tibutary - Water height (ft)	15.86
Diversion - Head Water height (ft)	12.44
Wall Thickness (ft)	4
Toe (Ft)	9
Heel (ft)	9

File:

MN State Building Codes
Frost Depth = 5.0 ft provide min frost ftg protection during Dec, Jan, Feb, March
Water El. = 903.24 ft DEC, JAN, FEB Mean Water Elevation

Non-Overflow Section **Length = 80.5 ft**
Stepped Ftg Ls = 2.0 ft overlap distance at stepped ftg



See Piling Plan for Vert Loads and Horiz Resistance

Case 1 or 2: 1
Normal Water Level, El. 884.11 ft
Δh normal = -1.6 ft
See Geotechnical seepage Model

UPLIFT
Case 1, Full Hydrostatic Head (Dashed Line)
Case 2, Full HW in Front of Upstream sheets
Full TW on down stream of sheets
enter "0" if no cut-off

Vertical Loads	Section	L ft	W ft	H ft	γ kcf	shape	V K	arm ft	Mv ft-k
Ftg concrete	1	80.5	22.00	4.00	0.15	rec	1062.6	11.00	11,688.6
Stem	2	80.5	4.00	26.32	0.15	rec	1271.3	11.00	13,983.8
Batter	3	80.5	0.00	16.32	0.15	tri	0.0	13.00	0.0
					D.L. Concrete	ΣVc =	**2333.9**	ΣM_V =	**25,672.4**

← CONSTANT FOR ALL LOAD CASES

T.W on ftg Stem	10	80.5	9.00	12.44	0.0624	rec	562.4	4.50	2,530.8
H.W. on Stem Slope	11	80.5	0.00	16.32	0.12	tri	0.0	13.00	0.0
H.W. Above Slope	13	80.5	0.00	10.00	0.12	rec	0.0	13.00	0.0
Soil on Footing	12s	80.5	9.00	26.32	0.0626	rec	1193.7	17.50	20,889.9
H.W. on Footing	12w	80.5	9.00	0.00	0.0624	rec	0.0	17.50	0.0
					D.L. Water	ΣVw =	**1756.1**	ΣM_V =	**23,420.7**

Uplift Loads		L ft	W ft	Pressure ksf		**U** K	arm ft	**Mu** ft-k
	U_B	80.5	22.00	1.026	rec	-1816.8	11.00	-19,985
	U_A	80.5	22.00	-0.776	tri	687.4	14.67	10,081
					ΣU =	**-1129.4**	ΣM_U =	**-9,903**

Horizontal Loads	L ft	H ft	Pressure ksf	**ICE** K	arm ft	**Mu** ft-k

BARR ENGINEERING			DATE	2/11/2011	SHEET NO.
			PROJECT NAME	FARGO – MOORHEAD METRO FLOOD RISK MANAGEMENT PROJECT, FEASIBILITY STUDY, PHASE 4	
COMPUTED	CHECKED	SUBMITTED	PROJECT NUMBER	34091004	
MBI		MBI	SUBJECT	Sheyenne Aquaduct Structure - Retaining Walls	
2/11/11				Load Cases: Case 2 100 yr. flood + ice	Panel C

ICE	80.5	2.00	0.00	rec	0.0	29.32	0.0	
	L		Force		**H**	arm	**Mw**	
	ft		k/ft		K	ft	ft-k	
SOIL	80.5		-8.733		-703.04	10.11	-7105.36	
Water Loads								
H_{TW}	80.5		8.433	tri	678.82	5.48	3719.93	
H_{HW}	80.5		-0.499	tri	-40.19	1.33	-53.58	
				ΣWater =	**638.63**	ΣM_W =	**-3439.0**	

Overturning Moments	$\Sigma M_{OT} = M_U + M_W + M_{ICE}$ =	-13342	kip-ft
Resisting Moments	$\Sigma M_R = M_V$ =	49093	kip-ft
Sum of Moments	$\Sigma Mnet = M_R + M_{OT}$ =	**35,751**	kip-ft
Sum of Vertical Forces	P = Conc + Water + Uplift =	**2,961**	kips
Sum of Horizontal Forces	H = Σhorizontal	**-64**	kips

Location of Resultant	Xr = ΣM / P =	12.08	ft from Toe
	e = B/2 - Xr =	(1.08)	ft
	B/6 =	3.667	ft

CONCRETE QUANTITIES

			forming	
Ftg conc:	269	cy (includes stepped)	871	sf
Stem Conc:	314	cy	4490	sf
Total =	583			

STEEL REINFORCEMENT: (assumed)

		Bar #	Spacing		Length	# of bars	Total wt		
a) Footing			in	LB /ft	ft	ea	lb		
Top mat	Transverse:	9	6	3.40	21.5	165	12,062		
	Longitudinal:	9	6	3.40	82	44	12,267		
Bot mat	Transverse:	9	6	3.40	21.5	165	12,062		
	Longitudinal:	9	6	3.40	82	44	12,267		
								cy	**LB/cy**
							48,657	269	180.9572727
b) Skin Reinf. On Monolith									
Vert Face	Vertical	9	6	3.40	25.82	161	14,134	28267.736	
	Longitudinal:	9	6	3.40	80	52	14,144	28288	
Top Face	Transverse:	9	6	3.40	3.5	161	1,916		
	Longitudinal:	9	6	3.40	80	8	2,176		
Dowels	Vertical I.F.	9	6	3.40	25.8	161	14,134		
	Vertical O.F.	9	6	3.40	25.8	161	14,134		
								cy	**LB/cy**
							60,638	314	193.1805169
						Σ =	**109,295**		
	Lap Splices (long. Bars)	9		3.40	8	309	8,405		
						Σ Bar Wt=	117,700	lb	

FORCES AT THE BOTTOM OF THE STEM

	H	γ	Pbase	V	arm	Mv
	ft	kcf		K	ft	ft-k
Diversion WSEL	12.44	0.0624	0.776256	4.828	4.147	20.0214
Tributary SEL =	26.32	0.019	0.50008	6.581	8.773	57.73777
Tributary WSEL =	0.00	0.0624	0	0.000	0.000	0
Sum				6.581		57.73777
Net Forces				1.753		37.71637

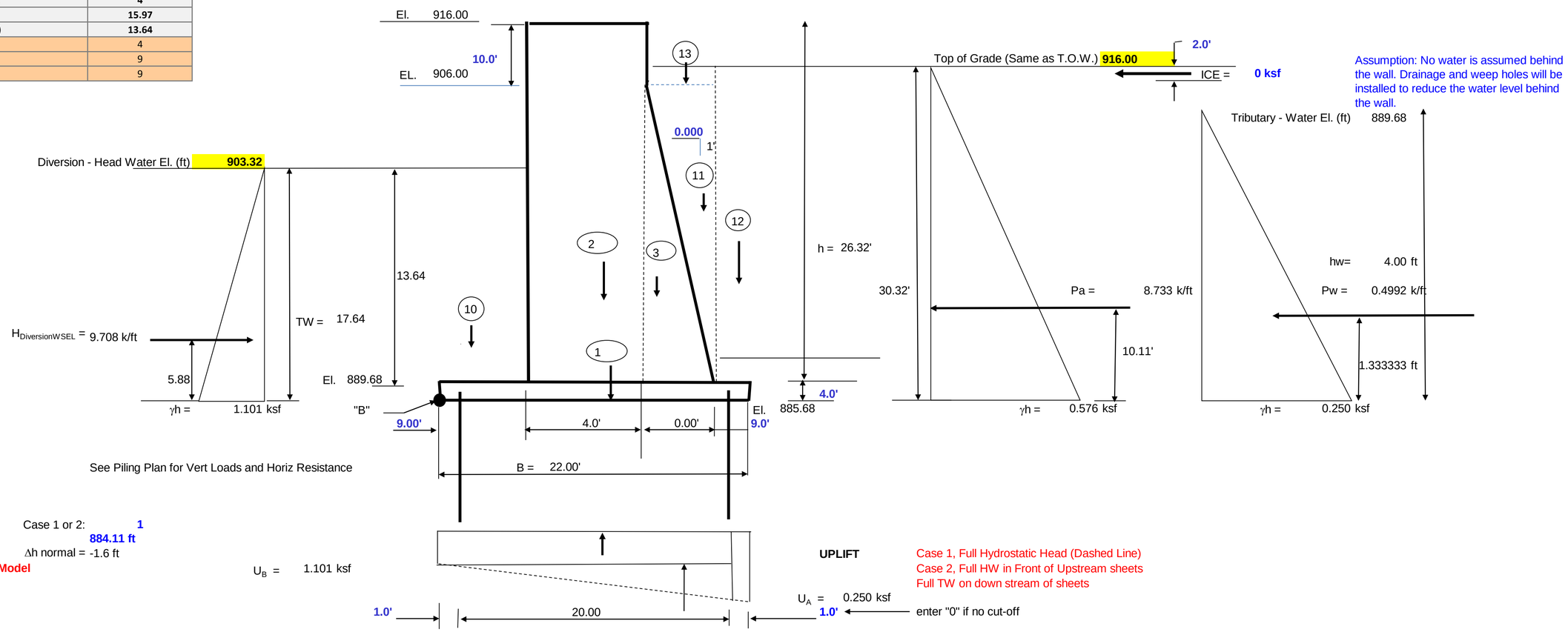
BARR ENGINEERING			DATE	2/11/2011	SHEET NO.
			PROJECT NAME	FARGO – MOORHEAD METRO FLOOD RISK MANAGEMENT PROJECT, FEASIBILITY STUDY, PHASE 4	
COMPUTED	CHECKED	SUBMITTED	PROJECT NUMBER	34091004	
MBI 2/11/11		MBI	SUBJECT	Sheyenne Aquaduct Structure - Retaining Walls Load Cases: Case 3 500 yr. flood Panel C	

ID#	Case 3
Name	500 yr. flood
Load Category	Unusual
Tributary - Water El. (ft)	914.67
Diversion - Head Water El. (ft)	903.32
Diversion - Tail Water El. (ft)	903.06
Tributary - T.O. Wall El. (ft)	916
Tributary - T.O. Deck L.P. El.(ft)	898.7
Tributary - T.O. Deck H.P. El.(ft)	900.7
Diversion - T.O. Mat El. (ft)	889.68
Tributary - Deck Slab thickness @ L.P. (ft)	2
Tributary - Deck Slab thickness @ H.P. (ft)	4
Diversion - Mat Slab thickness (ft)	4
Tibutary - Water height (ft)	15.97
Diversion - Head Water height (ft)	13.64
Wall Thickness (ft)	4
Toe (Ft)	9
Heel (ft)	9

File:

MN State Building Codes
Frost Depth = 5.0 ft provide min frost ftg protection during Dec, Jan, Feb, March
Water El. = 903.24 ft DEC, JAN, FEB Mean Water Elevation

Non-Overflow Section **Length = 80.5 ft**
Stepped Ftg Ls = 2.0 ft overlap distance at stepped ftg



Case 1 or 2: 1
Normal Water Level, El. 884.11 ft
Δh normal = -1.6 ft
See Geotechnical seepage Model

Case 1, Full Hydrostatic Head (Dashed Line)
Case 2, Full HW in Front of Upstream sheets
Full TW on down stream of sheets
enter "0" if no cut-off

Vertical Loads	Section	L ft	W ft	H ft	γ kcf	shape	V K	arm ft	Mv ft-k
Ftg concrete	1	80.5	22.00	4.00	0.15	rec	1062.6	11.00	11,688.6
Stem	2	80.5	4.00	26.32	0.15	rec	1271.3	11.00	13,983.8
Batter	3	80.5	0.00	16.32	0.15	tri	0.0	13.00	0.0
					D.L. Concrete	ΣVc =	**2333.9**	ΣM_V =	**25,672.4**
T.W on ftg Stem	10	80.5	9.00	13.64	0.0624	rec	616.6	4.50	2,774.9
H.W. on Stem Slope	11	80.5	0.00	16.32	0.12	tri	0.0	13.00	0.0
H.W. Above Slope	13	80.5	0.00	10.00	0.12	rec	0.0	13.00	0.0
Soil on Footing	12s	80.5	9.00	26.32	0.0626	rec	1193.7	17.50	20,889.9
H.W. on Footing	12w	80.5	9.00	0.00	0.0624	rec	0.0	17.50	0.0
					D.L. Water	ΣVw =	**1810.4**	ΣM_V =	**23,664.8**

← CONSTANT FOR ALL LOAD CASES

Uplift Loads		L ft	W ft	Pressure ksf		U K	arm ft	Mu ft-k
	U_B	80.5	22.00	1.101	rec	-1949.4	11.00	-21,443
	U_A	80.5	22.00	-0.851	tri	753.7	14.67	11,054
					ΣU =	**-1195.7**	ΣM_U =	**-10,389**

Horizontal Loads	L ft	H ft	Pressure ksf	ICE K	arm ft	Mu ft-k

BARR ENGINEERING			DATE	2/11/2011	SHEET NO.
			PROJECT NAME	FARGO – MOORHEAD METRO FLOOD RISK MANAGEMENT PROJECT, FEASIBILITY STUDY, PHASE 4	
COMPUTED	CHECKED	SUBMITTED	PROJECT NUMBER	34091004	
MBI 2/11/11		MBI	SUBJECT	Sheyenne Aquaduct Structure - Retaining Walls	
				Load Cases: Case 3 500 yr. flood	Panel C

ICE	80.5	2.00	0.00	rec	0.0	29.32	0.0	
	L		Force		**H**	arm	**Mw**	
	ft		k/ft		K	ft	ft-k	
SOIL	80.5		-8.733		-703.04	10.11'	-7105.36	
Water Loads								
H_{TW}	80.5		9.708	tri	781.53	5.88	4595.42	
H_{HW}	80.5		-0.499	tri	-40.19	1.33	-53.58	
				ΣWater =	**741.35**	ΣM_W =	**-2563.5**	

Overturning Moments	$\Sigma M_{OT} = M_U + M_W + M_{ICE}$ =	-12953	kip-ft
Resisting Moments	$\Sigma M_R = M_V$ =	49337	kip-ft
Sum of Moments	$\Sigma Mnet = M_R + M_{OT}$ =	**36,384**	kip-ft
Sum of Vertical Forces	P = Conc + Water + Uplift =	**2,948**	kips
Sum of Horizontal Forces	H = Σhorizontal	**38**	kips

Location of Resultant	Xr = ΣM / P =	12.34	ft from Toe
	e = B/2 - Xr =	(1.34)	ft
	B/6 =	3.667	ft

CONCRETE QUANTITIES

			forming	
Ftg conc:	269	cy (includes stepped)	871	sf
Stem Conc:	314	cy	4490	sf
Total =	583			

STEEL REINFORCEMENT: (assumed)

		Bar #	Spacing in	LB /ft	Length ft	# of bars ea	Total wt lb		
a) Footing									
Top mat	Transverse:	9	6	3.40	21.5	165	12,062		
	Longitudinal:	9	6	3.40	82	44	12,267		
Bot mat	Transverse:	9	6	3.40	21.5	165	12,062		
	Longitudinal:	9	6	3.40	82	44	12,267		
								cy	**LB/cy**
							48,657	269	180.9572727
b) Skin Reinf. On Monolith									
Vert Face	Vertical	9	6	3.40	25.82	161	14,134	28267.736	
	Longitudinal:	9	6	3.40	80	52	14,144	28288	
Top Face	Transverse:	9	6	3.40	3.5	161	1,916		
	Longitudinal:	9	6	3.40	80	8	2,176		
Dowels	Vertical I.F.	9	6	3.40	25.8	161	14,134		
	Vertical O.F.	9	6	3.40	25.8	161	14,134		
								cy	**LB/cy**
							60,638	314	193.1805169
						Σ =	**109,295**		
	Lap Splices (long. Bars)	9		3.40	8	309	8,405		
						Σ Bar Wt=	117,700	lb	

FORCES AT THE BOTTOM OF THE STEM

Diversion Face	H ft	γ kcf	Pbase	**V** K	arm ft	**Mv** ft-k
Diversion WSEL	13.64	0.0624	0.851136	5.805	4.547	26.39225
Tributary SEL =	26.32	0.019	0.50008	6.581	8.773	57.73777
Tributary WSEL =	0.00	0.0624	0	0.000	0.000	0
Sum				6.581		57.73777
Net Forces				0.776		31.34552

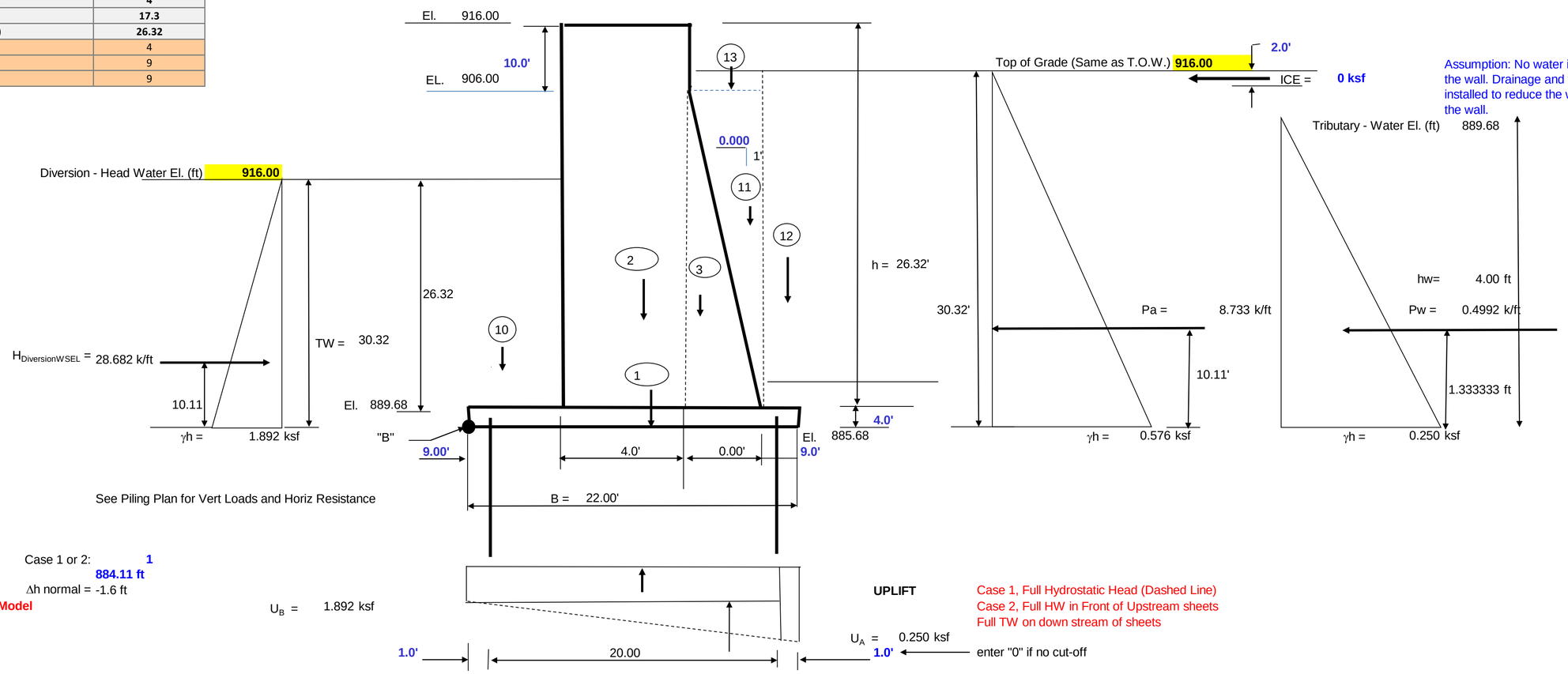
BARR ENGINEERING			DATE	2/11/2011	SHEET NO.
			PROJECT NAME	FARGO – MOORHEAD METRO FLOOD RISK MANAGEMENT PROJECT, FEASIBILITY STUDY, PHASE 4	
COMPUTED	CHECKED	SUBMITTED	PROJECT NUMBER	34091004	
MBI 2/11/11		MBI	SUBJECT	Sheyenne Aquaduct Structure - Retaining Walls Load Cases: Case 4 T.O. Levee Panel C	

ID#	Case 4
Name	T.O. Levee
Load Category	Extreme
Tributary - Water El. (ft)	NA
Diversion - Head Water El. (ft)	916
Diversion - Tail Water El. (ft)	916
Tributary - T.O. Wall El. (ft)	916
Tributary - T.O. Deck L.P. El.(ft)	898.7
Tributary - T.O. Deck H.P. El.(ft)	900.7
Diversion - T.O. Mat El. (ft)	889.68
Tributary - Deck Slab thickness @ L.P. (ft)	2
Tributary - Deck Slab thickness @ H.P. (ft)	4
Diversion - Mat Slab thickness (ft)	4
Tibutary - Water height (ft)	17.3
Diversion - Head Water height (ft)	26.32
Wall Thickness (ft)	4
Toe (Ft)	9
Heel (ft)	9

File:

MN State Building Codes
Frost Depth = **5.0 ft** provide min frost ftg protection during Dec, Jan, Feb, March
Water El. = **903.24 ft** DEC, JAN, FEB Mean Water Elevation

Non-Overflow Section **Length = 80.5 ft**
Stepped Ftg Ls = **2.0 ft** overlap distance at stepped ftg



Case 1 or 2: **1**
Normal Water Level, El. **884.11 ft**
Δh normal = -1.6 ft
See Geotechnical seepage Model

Vertical Loads	Section	L ft	W ft	H ft	γ kcf	shape	V K	arm ft	Mv ft-k
Ftg concrete	1	80.5	22.00	4.00	0.15	rec	1062.6	11.00	11,688.6
Stem	2	80.5	4.00	26.32	0.15	rec	1271.3	11.00	13,983.8
Batter	3	80.5	0.00	16.32	0.15	tri	0.0	13.00	0.0
					D.L. Concrete	ΣVc =	**2333.9**	ΣM_V =	**25,672.4**
T.W on ftg Stem	10	80.5	9.00	26.32	0.0624	rec	1189.9	4.50	5,354.5
H.W. on Stem Slope	11	80.5	0.00	16.32	0.12	tri	0.0	13.00	0.0
H.W. Above Slope	13	80.5	0.00	10.00	0.12	rec	0.0	13.00	0.0
Soil on Footing	12s	80.5	9.00	26.32	0.0626	rec	1193.7	17.50	20,889.9
H.W. on Footing	12w	80.5	9.00	0.00	0.0624	rec	0.0	17.50	0.0
					D.L. Water	ΣVw =	**2383.6**	ΣM_V =	**26,244.4**

← CONSTANT FOR ALL LOAD CASES

Uplift Loads		L ft	W ft	Pressure ksf		U K	arm ft	Mu ft-k
	U_B	80.5	22.00	1.892	rec	-3350.7	11.00	-36,857
	U_A	80.5	22.00	-1.642	tri	1454.3	14.67	21,330
					ΣU =	**-1896.4**	ΣM_U =	**-15,527**

Horizontal Loads		L ft	H ft	Pressure ksf		ICE K	arm ft	Mu ft-k

BARR ENGINEERING			DATE	2/11/2011	SHEET NO.
			PROJECT NAME	FARGO – MOORHEAD METRO FLOOD RISK MANAGEMENT PROJECT, FEASIBILITY STUDY, PHASE 4	
COMPUTED	CHECKED	SUBMITTED	PROJECT NUMBER	34091004	
MBI		MBI	SUBJECT	Sheyenne Aquaduct Structure - Retaining Walls	
2/11/11				Load Cases: Case 4 T.O. Levee Panel C	

ICE	80.5	2.00	0.00	rec	0.0	29.32	0.0	
	L		Force		**H**	arm	**Mw**	
	ft		k/ft		K	ft	ft-k	
SOIL	80.5		-8.733		-703.04	10.11'	-7105.36	
Water Loads								
H_{TW}	80.5		28.682	tri	2308.92	10.11	23335.48	
H_{HW}	80.5		-0.499	tri	-40.19	1.33	-53.58	
				ΣWater =	**2268.73**	ΣM_W =	**16176.5**	

Overturning Moments	$\Sigma M_{OT} = M_U + M_W + M_{ICE}$ =	649	kip-ft
Resisting Moments	$\Sigma M_R = M_V$ =	51917	kip-ft
Sum of Moments	$\Sigma Mnet = M_R + M_{OT}$ =	**52,566**	kip-ft
Sum of Vertical Forces	P = Conc + Water + Uplift =	**2,821**	kips
Sum of Horizontal Forces	H = Σhorizontal	**1,566**	kips

Location of Resultant	Xr = ΣM / P =	18.63	ft from Toe
	e = B/2 - Xr =	(7.63)	ft
	B/6 =	3.667	ft

CONCRETE QUANTITIES

			forming	
Ftg conc:	269	cy (includes stepped)	871	sf
Stem Conc:	314	cy	4490	sf
Total =	583			

STEEL REINFORCEMENT: (assumed)

		Bar #	Spacing		Length	# of bars	Total wt		
a) Footing			in	LB /ft	ft	ea	lb		
Top mat	Transverse:	9	6	3.40	21.5	165	12,062		
	Longitudinal:	9	6	3.40	82	44	12,267		
Bot mat	Transverse:	9	6	3.40	21.5	165	12,062		
	Longitudinal:	9	6	3.40	82	44	12,267		
								cy	**LB/cy**
							48,657	269	180.9572727
b) Skin Reinf. On Monolith									
Vert Face	Vertical	9	6	3.40	25.82	161	14,134	28267.736	
	Longitudinal:	9	6	3.40	80	52	14,144	28288	
Top Face	Transverse:	9	6	3.40	3.5	161	1,916		
	Longitudinal:	9	6	3.40	80	8	2,176		
Dowels	Vertical I.F.	9	6	3.40	25.8	161	14,134		
	Vertical O.F.	9	6	3.40	25.8	161	14,134		
								cy	**LB/cy**
							60,638	314	193.1805169
						Σ =	**109,295**		
	Lap Splices (long. Bars)	9		3.40	8	309	8,405		
						Σ Bar Wt=	117,700	lb	

FORCES AT THE BOTTOM OF THE STEM

Diversion Face	H	γ	Pbase	**V**	arm	**Mv**
	ft	kcf		K	ft	ft-k
Diversion WSEL	26.32	**0.0624**	1.642368	21.614	8.773	189.623
Tributary SEL =	26.32	**0.019**	0.50008	6.581	8.773	57.73777
Tributary WSEL =	0.00	**0.0624**	0	0.000	0.000	0
Sum				6.581		57.73777
Net Forces				-15.033		-131.885

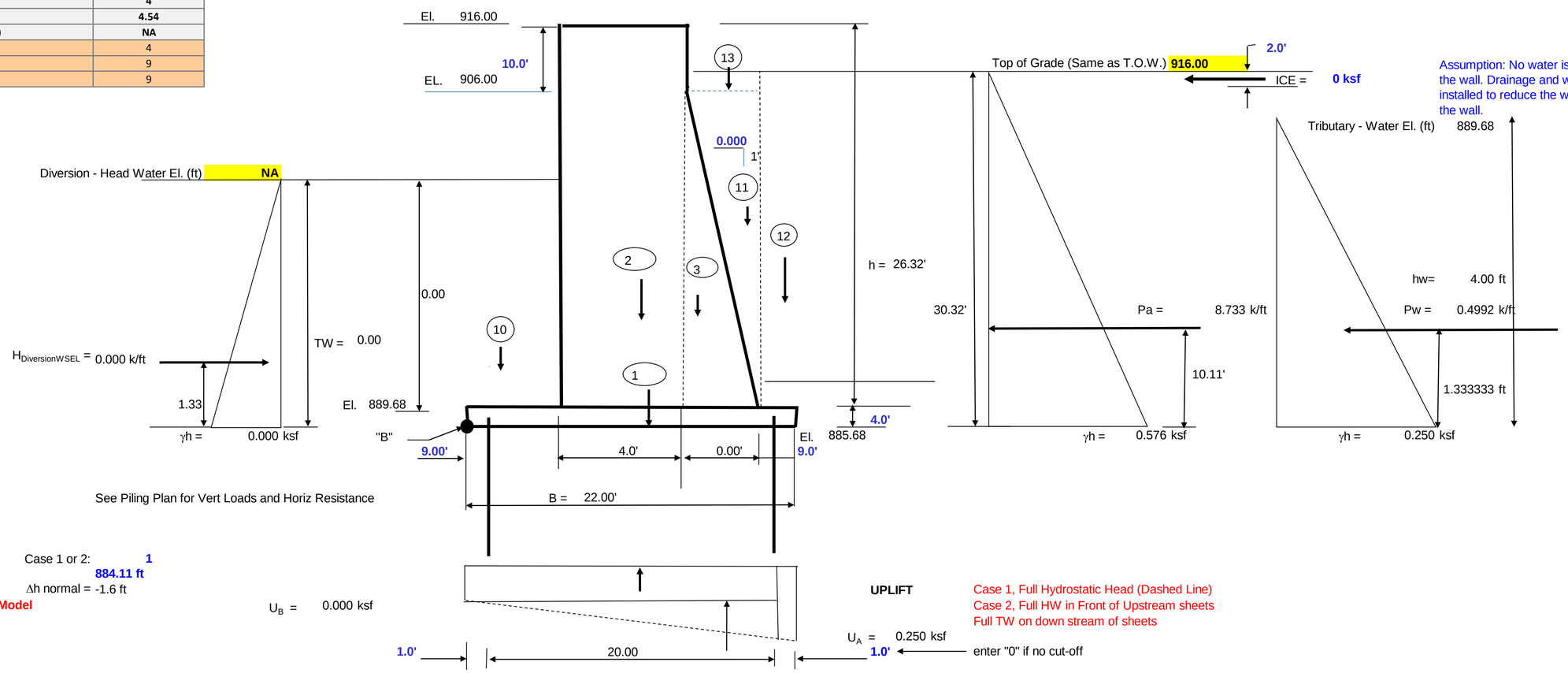
BARR ENGINEERING			DATE	2/11/2011	SHEET NO.
			PROJECT NAME	FARGO – MOORHEAD METRO FLOOD RISK MANAGEMENT PROJECT, FEASIBILITY STUDY, PHASE 4	
COMPUTED	CHECKED	SUBMITTED	PROJECT NUMBER	34091004	
MBI 2/11/11		MBI	SUBJECT	Sheyenne Aquaduct Structure - Retaining Walls Load Cases: Case 5 Normal flow + ice Panel C	

ID#	Case 5
Name	Normal flow + ice
Load Category	Usual
Tributary - Water El. (ft)	903.24
Diversion - Head Water El. (ft)	NA
Diversion - Tail Water El. (ft)	NA
Tributary - T.O. Wall El. (ft)	916
Tributary - T.O. Deck L.P. El.(ft)	898.7
Tributary - T.O. Deck H.P. El.(ft)	900.7
Diversion - T.O. Mat El. (ft)	889.68
Tributary - Deck Slab thickness @ L.P. (ft)	2
Tributary - Deck Slab thickness @ H.P. (ft)	4
Diversion - Mat Slab thickness (ft)	4
Tibutary - Water height (ft)	4.54
Diversion - Head Water height (ft)	NA
Wall Thickness (ft)	4
Toe (Ft)	9
Heel (ft)	9

File:

MN State Building Codes
Frost Depth = 5.0 ft provide min frost ftg protection during Dec, Jan, Feb, March
Water El. = 903.24 ft DEC, JAN, FEB Mean Water Elevation

Non-Overflow Section **Length = 80.5 ft**
Stepped Ftg Ls = 2.0 ft overlap distance at stepped ftg



See Piling Plan for Vert Loads and Horiz Resistance

Case 1 or 2: 1
Normal Water Level, El. 884.11 ft
Δh normal = -1.6 ft
See Geotechnical seepage Model

U_B = 0.000 ksf

U_A = 0.250 ksf

UPLIFT
Case 1, Full Hydrostatic Head (Dashed Line)
Case 2, Full HW in Front of Upstream sheets
Full TW on down stream of sheets
enter "0" if no cut-off

Vertical Loads	Section	L ft	W ft	H ft	γ kcf	shape	V K	arm ft	Mv ft-k
Ftg concrete	1	80.5	22.00	4.00	0.15	rec	1062.6	11.00	11,688.6
Stem	2	80.5	4.00	26.32	0.15	rec	1271.3	11.00	13,983.8
Batter	3	80.5	0.00	16.32	0.15	tri	0.0	13.00	0.0
					D.L. Concrete	ΣVc =	**2333.9**	ΣM_V =	**25,672.4**

← CONSTANT FOR ALL LOAD CASES

T.W on ftg Stem	10	80.5	9.00	0.00	0.0624	rec	0.0	4.50	0.0
H.W. on Stem Slope	11	80.5	0.00	16.32	0.12	tri	0.0	13.00	0.0
H.W. Above Slope	13	80.5	0.00	10.00	0.12	rec	0.0	13.00	0.0
Soil on Footing	12s	80.5	9.00	26.32	0.0626	rec	1193.7	17.50	20,889.9
H.W. on Footing	12w	80.5	9.00	0.00	0.0624	rec	0.0	17.50	0.0
					D.L. Water	ΣVw =	**1193.7**	ΣM_V =	**20,889.9**

Uplift Loads		L ft	W ft	Pressure ksf		U K	arm ft	Mu ft-k
	U_B	80.5	22.00	0.000	rec	0.0	11.00	0
	U_A	80.5	22.00	0.250	tri	-221.0	14.67	-3,242
					ΣU =	**-221.0**	ΣM_U =	**-3,242**

Horizontal Loads	L ft	H ft	Pressure ksf	ICE K	arm ft	Mu ft-k

BARR ENGINEERING			DATE	2/11/2011	SHEET NO.
			PROJECT NAME	FARGO – MOORHEAD METRO FLOOD RISK MANAGEMENT PROJECT, FEASIBILITY STUDY, PHASE 4	
COMPUTED	CHECKED	SUBMITTED	PROJECT NUMBER	34091004	
MBI		MBI	SUBJECT	Sheyenne Aquaduct Structure - Retaining Walls	
2/11/11				Load Cases: Case 5 Normal flow + ice Panel C	

ICE	80.5	2.00	0.00	rec	0.0	29.32	0.0	
	L		Force		**H**	arm	**Mw**	
	ft		k/ft		K	ft	ft-k	
SOIL	80.5		-8.733		-703.04	10.11'	-7105.36	
Water Loads								
H_{TW}	80.5		0.000	tri	0.00	1.33	0.00	
H_{HW}	80.5		-0.499	tri	-40.19	0.00	0.00	
				ΣWater =	**-40.19**	ΣM_W =	**-7105.4**	

Overturning Moments	$\Sigma M_{OT} = M_U + M_W + M_{ICE}$ =	-10347	kip-ft
Resisting Moments	$\Sigma M_R = M_V$ =	46562	kip-ft
Sum of Moments	$\Sigma Mnet = M_R + M_{OT}$ =	**36,215**	kip-ft
Sum of Vertical Forces	P = Conc + Water + Uplift =	**3,307**	kips
Sum of Horizontal Forces	H = Σhorizontal	**-743**	kips

Location of Resultant	Xr = ΣM / P =	10.95	ft from Toe
	e = B/2 - Xr =	0.05	ft
	B/6 =	3.667	ft

CONCRETE QUANTITIES

			forming	
Ftg conc:	269	cy (includes stepped)	871	sf
Stem Conc:	314	cy	4490	sf
Total =	583			

STEEL REINFORCEMENT: (assumed)

		Bar #	Spacing		Length	# of bars	Total wt		
a) Footing			in	LB /ft	ft	ea	lb		
Top mat	Transverse:	9	6	3.40	21.5	165	12,062		
	Longitudinal:	9	6	3.40	82	44	12,267		
Bot mat	Transverse:	9	6	3.40	21.5	165	12,062		
	Longitudinal:	9	6	3.40	82	44	12,267		
								cy	**LB/cy**
							48,657	269	180.9572727
b) Skin Reinf. On Monolith									
Vert Face	Vertical	9	6	3.40	25.82	161	14,134	28267.736	
	Longitudinal:	9	6	3.40	80	52	14,144	28288	
Top Face	Transverse:	9	6	3.40	3.5	161	1,916		
	Longitudinal:	9	6	3.40	80	8	2,176		
Dowels	Vertical I.F.	9	6	3.40	25.8	161	14,134		
	Vertical O.F.	9	6	3.40	25.8	161	14,134		
								cy	**LB/cy**
							60,638	314	193.1805169
						Σ =	**109,295**		
	Lap Splices (long. Bars)	9		3.40	8	309	8,405		
						Σ Bar Wt=	117,700	lb	

FORCES AT THE BOTTOM OF THE STEM

Diversion Face	H	γ	Pbase	V	arm	Mv
	ft	kcf		K	ft	ft-k
Diversion WSEL	0.00	0.0624	0	0.000	0.000	0
Tributary SEL =	26.32	0.019	0.50008	6.581	8.773	57.73777
Tributary WSEL =	0.00	0.0624	0	0.000	0.000	0
Sum				6.581		57.73777
Net Forces				6.581		57.73777

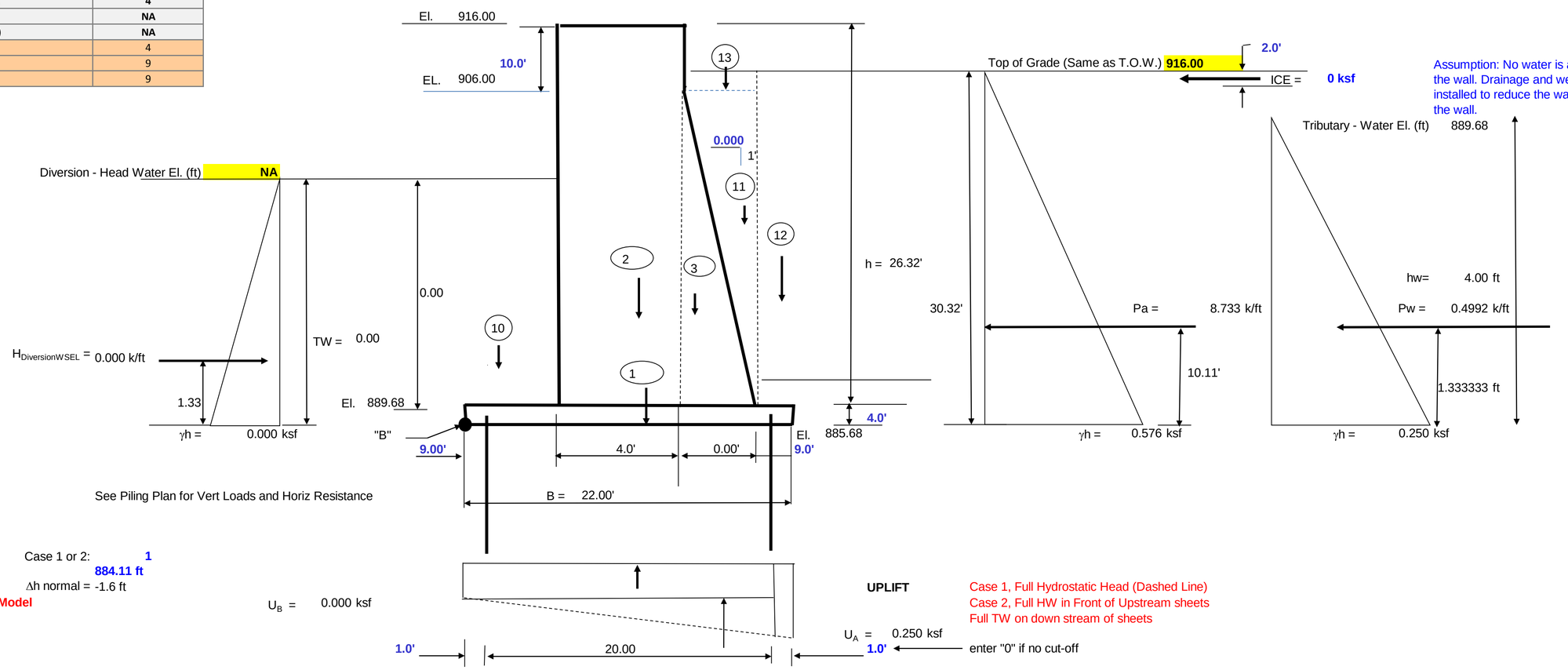
BARR ENGINEERING			DATE	2/11/2011	SHEET NO.
			PROJECT NAME	FARGO – MOORHEAD METRO FLOOD RISK MANAGEMENT PROJECT, FEASIBILITY STUDY, PHASE 4	
COMPUTED	CHECKED	SUBMITTED	PROJECT NUMBER	34091004	
MBI 2/11/11		MBI	SUBJECT	Sheyenne Aquaduct Structure - Retaining Walls Load Cases: Case 6 Construction Panel C	

ID#	Case 6
Name	Construction
Load Category	Unusual
Tributary - Water El. (ft)	NA
Diversion - Head Water El. (ft)	NA
Diversion - Tail Water El. (ft)	NA
Tributary - T.O. Wall El. (ft)	916
Tributary - T.O. Deck L.P. El.(ft)	898.7
Tributary - T.O. Deck H.P. El.(ft)	900.7
Diversion - T.O. Mat El. (ft)	889.68
Tributary - Deck Slab thickness @ L.P. (ft)	2
Tributary - Deck Slab thickness @ H.P. (ft)	4
Diversion - Mat Slab thickness (ft)	4
Tibutary - Water height (ft)	NA
Diversion - Head Water height (ft)	NA
Wall Thickness (ft)	4
Toe (Ft)	9
Heel (ft)	9

File:

MN State Building Codes
Frost Depth = **5.0 ft** provide min frost ftg protection during Dec, Jan, Feb, March
Water El. = **903.24 ft** DEC, JAN, FEB Mean Water Elevation

Non-Overflow Section **Length = 80.5 ft**
Stepped Ftg Ls = **2.0 ft** overlap distance at stepped ftg



Case 1 or 2: **1**
Normal Water Level, El. **884.11 ft**
Δh normal = -1.6 ft
See Geotechnical seepage Model

Vertical Loads	Section	L ft	W ft	H ft	γ kcf	shape	V K	arm ft	Mv ft-k
Ftg concrete	1	80.5	22.00	4.00	0.15	rec	1062.6	11.00	11,688.6
Stem	2	80.5	4.00	26.32	0.15	rec	1271.3	11.00	13,983.8
Batter	3	80.5	0.00	16.32	0.15	tri	0.0	13.00	0.0
					D.L. Concrete	ΣVc =	**2333.9**	ΣM_V =	**25,672.4**
T.W on ftg Stem	10	80.5	9.00	0.00	0.0624	rec	0.0	4.50	0.0
H.W. on Stem Slope	11	80.5	0.00	16.32	0.12	tri	0.0	13.00	0.0
H.W. Above Slope	13	80.5	0.00	10.00	0.12	rec	0.0	13.00	0.0
Soil on Footing	12s	80.5	9.00	26.32	0.0626	rec	1193.7	17.50	20,889.9
H.W. on Footing	12w	80.5	9.00	0.00	0.0624	rec	0.0	17.50	0.0
					D.L. Water	ΣVw =	**1193.7**	ΣM_V =	**20,889.9**

← CONSTANT FOR ALL LOAD CASES

Uplift Loads		L ft	W ft	Pressure ksf		U K	arm ft	Mu ft-k
	U_B	80.5	22.00	0.000	rec	0.0	11.00	0
	U_A	80.5	22.00	0.250	tri	-221.0	14.67	-3,242
					ΣU =	**-221.0**	ΣM_U =	**-3,242**

Horizontal Loads	L ft	H ft	Pressure ksf	ICE K	arm ft	Mu ft-k

BARR ENGINEERING			DATE	2/11/2011	SHEET NO.
			PROJECT NAME	FARGO – MOORHEAD METRO FLOOD RISK MANAGEMENT PROJECT, FEASIBILITY STUDY, PHASE 4	
COMPUTED	CHECKED	SUBMITTED	PROJECT NUMBER	34091004	
MBI		MBI	SUBJECT	Sheyenne Aquaduct Structure - Retaining Walls	
2/11/11				Load Cases: Case 6 Construction Panel C	

ICE	80.5	2.00	0.00	rec	0.0	29.32	0.0	
	L		Force		**H**	arm	**Mw**	
	ft		k/ft		K	ft	ft-k	
SOIL	80.5		-8.733		-703.04	10.11'	-7105.36	
Water Loads								
H_{TW}	80.5		0.000	tri	0.00	1.33	0.00	
H_{HW}	80.5		-0.499	tri	-40.19	1.33	-53.58	
				ΣWater =	**-40.19**	ΣM_W =	**-7158.9**	

Overturning Moments	$\Sigma M_{OT} = M_U + M_W + M_{ICE}$ =	-10401	kip-ft
Resisting Moments	$\Sigma M_R = M_V$ =	46562	kip-ft
Sum of Moments	$\Sigma Mnet = M_R + M_{OT}$ =	**36,162**	kip-ft
Sum of Vertical Forces	P = Conc + Water + Uplift =	**3,307**	kips
Sum of Horizontal Forces	H = Σhorizontal	**-743**	kips

Location of Resultant	Xr = ΣM / P =	10.94	ft from Toe
	e = B/2 - Xr =	0.06	ft
	B/6 =	3.667	ft

CONCRETE QUANTITIES

			forming	
Ftg conc:	269	cy (includes stepped)	871	sf
Stem Conc:	314	cy	4490	sf
Total =	583			

STEEL REINFORCEMENT: (assumed)

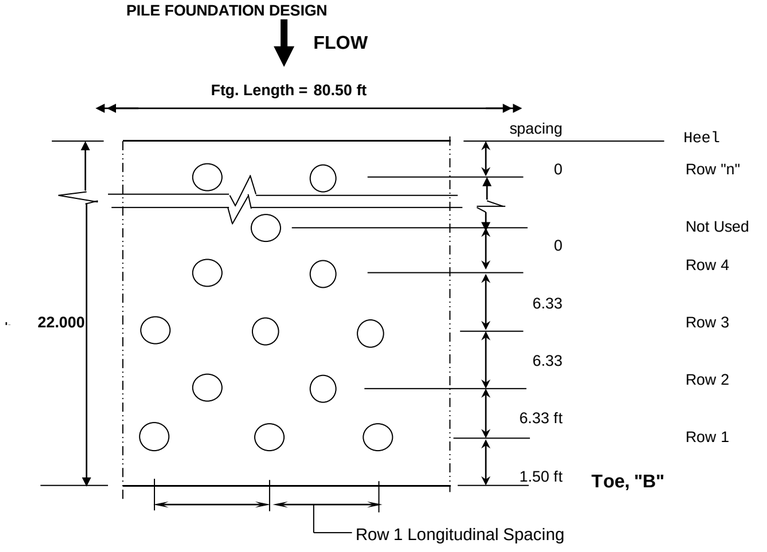
		Bar #	Spacing		Length	# of bars	Total wt		
a) Footing			in	LB /ft	ft	ea	lb		
Top mat	Transverse:	9	6	3.40	21.5	165	12,062		
	Longitudinal:	9	6	3.40	82	44	12,267		
Bot mat	Transverse:	9	6	3.40	21.5	165	12,062		
	Longitudinal:	9	6	3.40	82	44	12,267		
								cy	**LB/cy**
							48,657	269	180.9572727
b) Skin Reinf. On Monolith									
Vert Face	Vertical	9	6	3.40	25.82	161	14,134	28267.736	
	Longitudinal:	9	6	3.40	80	52	14,144	28288	
Top Face	Transverse:	9	6	3.40	3.5	161	1,916		
	Longitudinal:	9	6	3.40	80	8	2,176		
Dowels	Vertical I.F.	9	6	3.40	25.8	161	14,134		
	Vertical O.F.	9	6	3.40	25.8	161	14,134		
								cy	**LB/cy**
							60,638	314	193.1805169
						Σ =	**109,295**		
	Lap Splices (long. Bars)	9		3.40	8	309	8,405		
						Σ Bar Wt=	117,700	lb	

FORCES AT THE BOTTOM OF THE STEM

Diversion Face	H	γ	Pbase	V	arm	Mv
	ft	kcf		K	ft	ft-k
Diversion WSEL	0.00	0.0624	0	0.000	0.000	0
Tributary SEL =	26.32	0.019	0.50008	6.581	8.773	57.73777
Tributary WSEL =	0.00	0.0624	0	0.000	0.000	0
Sum				6.581		57.73777
Net Forces				6.581		57.73777

BARR ENGINEERING			DATE	2/11/2011	SHEET NO.
			PROJECT NAME	FARGO – MOORHEAD METRO FLOOD RISK MANAGEMENT PROJECT, FEASIBILITY STUDY, PHASE 4	
COMPUTED	CHECKED	SUBMITTED	PROJECT NUMBER	34091004	
MBI 2/11/11		MBI	SUBJECT	Sheyenne Aquaduct Structure - Retaining Walls	
				Panel C	

PILE FOUNDATION DESIGN



L = 80.50 ft

PILE PATTERN GEOMETRY

Transverse Spacing		Distance to Toe, d_{toe}	Longitudinal Spacing	Batter	Piles per Row (**N**)	Edge Dist (ft)		Trial N
Row 1 to Toe	**1.50 ft**	1.5 ft	**2.50 ft**	**0** "/12"	**12**	26.50	1	33
Row 1 to Row 2	**6.33 ft**	7.8 ft	**5.00 ft**	**0** "/12"	**12**	12.75	2	17
Row 2 to Row 3	**6.33 ft**	14.2 ft	**5.00 ft**	**0** "/12"	**12**	12.75	3	17
Row 3 to Row 4	**6.33 ft**	20.5 ft	**5.00 ft**	**0** "/12"	**12**	12.75	4	17
Row 4 to Row 5	**0.00 ft**	0.0 ft	**0.00 ft**	**0** "/12"	**0**	40.25	0	0
Row 5 to Row 6	**0.00 ft**	0.0 ft	**0.00 ft**	**0** "/12"	**0**	40.25	0	0
Row 6 to Row 7	**0.00 ft**	0.0 ft	**0.00 ft**	**0** "/12"	**0**	40.25	0	0
Row 7 to Row 8	**0.00 ft**	0.0 ft	**0.00 ft**	**0** "/12"	**0**	40.25	0	0
Row 8 to Row 9	**0.00 ft**	0.0 ft	**0.00 ft**	**0** "/12"	**0**	40.25	0	0
Row 9 to Row 10	**0.00 ft**	0.0 ft	**0.00 ft**	**0** "/12"	**0**	40.25	0	0
Row 10 to Row 11	**0.00 ft**	0.0 ft	**0.00 ft**	**0** "/12"	**0**	40.25	0	0
Row 11 to Row 12	**0.00 ft**	0.0 ft	**0.00 ft**	**0** "/12"	**0**	40.25	0	0
Row 12 to Row 13	**0.00 ft**	0.0 ft	**0.00 ft**	**0** "/12"	**0**	40.25	0	0
Row 13 to Row 14	**0.00 ft**	0.0 ft	**0.00 ft**	**0** "/12"	**0**	40.25	0	0
Row 14 to Row 15	**0.00 ft**	0.0 ft	**0.00 ft**	**0** "/12"	**0**	40.25	0	0
Last Row to Heel	1.51 ft							
	22.00 ft				**ΣN =**	**48**		84

Note: Enter 0 for Longitudinal Spacing for Rows Not Used)

Pile Properties: Pile Type: **HP** (C.I.P or HP) Pile Length = **44.0 ft**
HP Nominal Depth, h = **14.0 in**
Wt. per ft, plf **73**

Ftg EL. 885.68
Pile Tip El. 842.68
Pile Cap Embed = **1.00 ft**

Total pile Length = 2,112 LF

Pile Group Properties

N.A. of Pile Group to Toe
$X_{NA} = (\Sigma N * d_{toe}) / \Sigma N =$ **11.00 ft**

	Dist. From N.A. to Pile Row	d	N	$I = N * d^2$
1	Dist. To Row 1	9.50 ft	12	1081.9
2	Dist. To Row 2	3.17 ft	12	120.2
3	Dist. Row 3	-3.17 ft	12	120.2
4	Dist. Row 4	-9.50 ft	12	1081.9
0	Row 5 (not used)	0.00 ft	0	0.0
0	Row 6 (not used)	0.00 ft	0	0.0
0	Row 7 (not used)	0.00 ft	0	0.0
0	Row 8 (not used)	0.00 ft	0	0.0
0	Row 9 (not used)	0.00 ft	0	0.0
0	Row 10 (not used)	0.00 ft	0	0.0
0	Row 11 (not used)	0.00 ft	0	0.0
0	Row 12 (not used)	0.00 ft	0	0.0
0	Row 13 (not used)	0.00 ft	0	0.0
0	Row 14 (not used)	0.00 ft	0	0.0
0	Row 15 (not used)	0.00 ft	0	0.0
			48	$\Sigma I =$ **2404.1**

ALLOWABLE LOADS (from Geotechnical)

	Service	Allowable Pile Loads					
	ID#	Case 1	Case 2	Case 3	Case 4	Case 5	Case 6
	Name	100 yr. flood	100 yr. flood + ice	500 yr. flood	T.O. Levee	Normal flow + ice	Construction
	Load Category	Usual	Unusual	Unusual	Extreme	Usual	Unusual
Allwable Lateral Capacity (tons)		18.0 tons	20.5 tons	20.5 tons	24.0 tons	11.5 tons	20.5 tons
Allowable Pile Capacity (tons) - Axial		62.0 tons	82.6 tons	82.6 tons	107.7 tons	36.5 tons	82.6 tons
Safety Factors		2.00	1.50	1.50	1.15	2.00	1.50

w/o Group effects

Summary Pile Reactions

Load Combinations	Allowable Pile Capacity (tons) - Axial	Pile Loads (tons/pile) 1	2	3	4	5	6	7	8	9	10	11	12	Max. Vertical Load (Tons)	Horiz Pile Group Capacity (k)	Check
Case 1	**62.0 tons**	24.5	28.7	32.9	37.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	37.2	1,728	**OK**
Case 2	**82.6 tons**	24.5	28.7	32.9	37.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	37.2	1,968	**OK**
Case 3	**82.6 tons**	22.9	28.1	33.3	38.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	38.5	1,968	**OK**
Case 4	**107.7 tons**	-13.2	15.2	43.6	71.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	71.9	2,304	**OK**
Case 5	**36.5 tons**	34.7	34.5	34.4	34.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	34.7	1,104	**OK**
Case 6	**82.6 tons**	34.8	34.6	34.3	34.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	34.8	1,104	**OK**

Max Service : P = **71.9**

Using solid mechanics equations adapted for discrete elements, the forces in the pile rows for different load combinations are determined.
The force in each pile row is found using:

$$\text{Pile Load} = P / N + M_{NA} / I$$

First, the moment about the toe must be translated to get the moment about the neutral axis of the pile group.

$$e_{toe} = M_{toe} / P$$

Then the eccentricity about the neutral axis of the pile group is

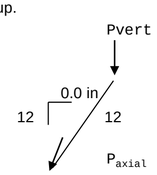
$$e_{NA} = X_{NA} - e_{toe}$$

The moment about the neutral axis of the pile group becomes

$$M_{NA} = P * e_{NA}$$

For battered pile, the Vertical pile load needs to be transformed to the axial load along the pile axis

Paxial = 1.000 Pvert



FORCE RESULTANT (see Stability Analysis)

CASE	Event		Vertical Load P (kips)	Horizontal	ΣM toe (kip-	$e_{toe} = M_{toe} / P$	$e_{NA} = X_{NA} - e_{toe}$	$M_{NA} = P * e_{NA}$

BARR ENGINEERING			DATE	2/11/2011	SHEET NO.
			PROJECT NAME	FARGO – MOORHEAD METRO FLOOD RISK MANAGEMENT PROJECT, FEASIBILITY STUDY, PHASE 4	
COMPUTED	CHECKED	SUBMITTED	PROJECT NUMBER	34091004	
MBI		MBI	SUBJECT	Sheyenne Aquaduct Structure - Retaining Walls	
2/11/11				Panel C	

Case 1	**100 yr. flood**	**Usual**	2,961	64	35,751	12.08	-1.08	-3200
Case 2	**100 yr. flood + ice**	**Unusual**	2,961	64	35,751	12.08	-1.08	-3200
Case 3	**500 yr. flood**	**Unusual**	2,948	-38	36,384	12.34	-1.34	-3966
Case 4	**T.O. Levee**	**Extreme**	2,821	-1,566	52,566	18.63	-7.64	-21548
Case 5	**Normal flow + ice**	**Usual**	3,307	743	36,215	10.95	0.04	140
Case 6	**Construction**	**Unusual**	3,307	743	36,162	10.94	0.06	194

SERVICE

Case **Case 1**
Flood Event **100 yr. flood**
Usual

Vertical Load, P = 2961 kips
Horizontal Load, H = 64 kips
M_{NA} = -3200 kip-ft

48

	Vertical Pile Loading	P / N	+	M_{NA}* d / Σ I	= Pile Loads		**Axial Pile Load**
1	Row 1	61.7		-12.6	49.0 kips/pile	24.5 tons/pile	24.5 tons/pile
2	Row 2	61.7		-4.2	57.5 kips/pile	28.7 tons/pile	28.7 tons/pile
3	Row 3	61.7		4.2	65.9 kips/pile	32.9 tons/pile	32.9 tons/pile
4	Row 4	61.7		12.6	74.3 kips/pile	37.2 tons/pile	37.2 tons/pile
5	Row 5	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
6	Row 6	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
7	Row 7	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
8	Row 8	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
9	Row 9	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
10	Row 10	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
11	Row 11	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
12	Row 12	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
13	Row 13	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
14	Row 14	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
15	Row 15	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
					max:	**37.2 tons/pile**	**max: 37.2 tons/pile**

Assumed lateral Capacity: 36.0 kips/pile

	Horizontal Pile Capacity	**Batter "/ft**	**N**	Resistance due to Batter, kips	Resitance due to Bending, kips	Group Efficiency	Lateral Resitance
1	Row 1	0	12	0.0	432	1.000	432 kips
2	Row 2	0	12	0.0	432	1.000	432 kips
3	Row 3	0	12	0.0	432	1.000	432 kips
4	Row 4	0	12	0.0	432	1.000	432 kips
5	Row 5	0	0	0.0	0	1.000	0 kips
6	Row 6	0	0	0.0	0	1.000	0 kips
7	Row 7	0	0	0.0	0	1.000	0 kips
8	Row 8	0	0	0.0	0	1.000	0 kips
9	Row 9	0	0	0.0	0	1.000	0 kips
10	Row 10	0	0	0.0	0	1.000	0 kips
11	Row 11	0	0	0.0	0	1.000	0 kips
12	Row 12	0	0	0.0	0	1.000	0 kips
13	Row 13	0	0	0.0	0	1.000	0 kips
14	Row 14	0	0	0.0	0	1.000	0 kips
15	Row 15	0	0	0.0	0	1.000	0 kips
			48		1728		**1728 kips**

OK

Case **Case 2**
Flood Event **100 yr. flood + ice**
Unusual

Vertical Load, P = 2961 kips
Horizontal Load, H = 64 kips
M_{NA} = -3200 kip-ft

48

	Vertical Pile Loading	P / N	+	M_{NA}* d / Σ I	= Pile Loads		**Axial Pile Load**
1	Row 1	61.7		-12.6	49.0 kips/pile	24.5 tons/pile	24.5 tons/pile
2	Row 2	61.7		-4.2	57.5 kips/pile	28.7 tons/pile	28.7 tons/pile
3	Row 3	61.7		4.2	65.9 kips/pile	32.9 tons/pile	32.9 tons/pile
4	Row 4	61.7		12.6	74.3 kips/pile	37.2 tons/pile	37.2 tons/pile
5	Row 5	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
6	Row 6	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
7	Row 7	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
8	Row 8	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
9	Row 9	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
10	Row 10	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
11	Row 11	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
12	Row 12	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
13	Row 13	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
14	Row 14	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
15	Row 15	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
					max:	**37.2 tons/pile**	**max: 37.2 tons/pile**

Assumed lateral Capacity: 41.0 kips/pile

	Horizontal Pile Capacity	**Batter "/ft**	**N**	Resistance due to Batter, kips	Resitance due to Bending, kips	Group Efficiency	Lateral Resitance
1	Row 1	0	12	0.0	492	1.000	492 kips
2	Row 2	0	12	0.0	492	1.000	492 kips
3	Row 3	0	12	0.0	492	1.000	492 kips

4	Row 4	0	12	0.0	492	1.000	492 kips	
5	Row 5	0	0	0.0	0	1.000	0 kips	
6	Row 6	0	0	0.0	0	1.000	0 kips	
7	Row 7	0	0	0.0	0	1.000	0 kips	
8	Row 8	0	0	0.0	0	1.000	0 kips	
9	Row 9	0	0	0.0	0	1.000	0 kips	
10	Row 10	0	0	0.0	0	1.000	0 kips	
11	Row 11	0	0	0.0	0	1.000	0 kips	
12	Row 12	0	0	0.0	0	1.000	0 kips	
13	Row 13	0	0	0.0	0	1.000	0 kips	
14	Row 14	0	0	0.0	0	1.000	0 kips	
15	Row 15	0	0	0.0	0	1.000	0 kips	
			48		1968		**1968 kips**	**OK**

Case **Case 3**
Flood Event **500 yr. flood**
Unusual

Vertical Load, P = 2948 kips
Horizontal Load, H = -38 kips
M_{NA} = -3966 kip-ft

	Vertical Pile Loading	P / N	+	M_{NA}* d / Σ I	= Pile Loads		**Axial Pile Load**
1	Row 1	61.4		-15.7	45.8 kips/pile	22.9 tons/pile	22.9 tons/pile
2	Row 2	61.4		-5.2	56.2 kips/pile	28.1 tons/pile	28.1 tons/pile
3	Row 3	61.4		5.2	66.6 kips/pile	33.3 tons/pile	33.3 tons/pile
4	Row 4	61.4		15.7	77.1 kips/pile	38.5 tons/pile	38.5 tons/pile
5	Row 5	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
6	Row 6	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
7	Row 7	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
8	Row 8	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
9	Row 9	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
10	Row 10	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
11	Row 11	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
12	Row 12	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
13	Row 13	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
14	Row 14	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
15	Row 15	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
						max: **38.5 tons/pile**	**max:** **38.5 tons/pile**

Assumed lateral Capacity: 41.0 kips/pile

	Horizontal Pile Capacity	**Batter "/ft**	**N**	Resistance due to Batter, kips	Resitance due to Bending, kips	Group Efficiency	Lateral Resitance	
1	Row 1	0	12	0.0	492	1.000	492 kips	
2	Row 2	0	12	0.0	492	1.000	492 kips	
3	Row 3	0	12	0.0	492	1.000	492 kips	
4	Row 4	0	12	0.0	492	1.000	492 kips	
5	Row 5	0	0	0.0	0	1.000	0 kips	
6	Row 6	0	0	0.0	0	1.000	0 kips	
7	Row 7	0	0	0.0	0	1.000	0 kips	
8	Row 8	0	0	0.0	0	1.000	0 kips	
9	Row 9	0	0	0.0	0	1.000	0 kips	
10	Row 10	0	0	0.0	0	1.000	0 kips	
11	Row 11	0	0	0.0	0	1.000	0 kips	
12	Row 12	0	0	0.0	0	1.000	0 kips	
13	Row 13	0	0	0.0	0	1.000	0 kips	
14	Row 14	0	0	0.0	0	1.000	0 kips	
15	Row 15	0	0	0.0	0	1.000	0 kips	
			48		1968		**1968 kips**	**OK**

Case **Case 4**
Flood Event **T.O. Levee**
Extreme

Vertical Load, P = 2821 kips
Horizontal Load, H = -1566 kips
M_{NA} = -21548 kip-ft

	Vertical Pile Loading	P / N	+	M_{NA}* d / Σ I	= Pile Loads		**Axial Pile Load**
1	Row 1	58.8		-85.1	-26.3 kips/pile	-13.2 tons/pile	-13.2 tons/pile
2	Row 2	58.8		-28.4	30.4 kips/pile	15.2 tons/pile	15.2 tons/pile
3	Row 3	58.8		28.4	87.1 kips/pile	43.6 tons/pile	43.6 tons/pile
4	Row 4	58.8		85.1	143.9 kips/pile	71.9 tons/pile	71.9 tons/pile
5	Row 5	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
6	Row 6	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
7	Row 7	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
8	Row 8	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
9	Row 9	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
10	Row 10	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
11	Row 11	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
12	Row 12	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
13	Row 13	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
14	Row 14	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
15	Row 15	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
						max: **71.9 tons/pile**	**max:** **71.9 tons/pile**

Assumed lateral Capacity: 48.0 kips/pile

BARR ENGINEERING			DATE	2/11/2011	SHEET NO.
			PROJECT NAME	FARGO – MOORHEAD METRO FLOOD RISK MANAGEMENT PROJECT, FEASIBILITY STUDY, PHASE 4	
COMPUTED	CHECKED	SUBMITTED	PROJECT NUMBER	34091004	
MBI		MBI	SUBJECT	Sheyenne Aquaduct Structure - Retaining Walls	
2/11/11				**Panel C**	

	Horizontal Pile Capacity	**Batter "/ft**	**N**	Resistance due to Batter, kips	Resitance due to Bending, kips	Group Efficiency	Lateral Resitance	
1	Row 1	0	12	0.0	576	1.000	576 kips	
2	Row 2	0	12	0.0	576	1.000	576 kips	
3	Row 3	0	12	0.0	576	1.000	576 kips	
4	Row 4	0	12	0.0	576	1.000	576 kips	
5	Row 5	0	0	0.0	0	1.000	0 kips	
6	Row 6	0	0	0.0	0	1.000	0 kips	
7	Row 7	0	0	0.0	0	1.000	0 kips	
8	Row 8	0	0	0.0	0	1.000	0 kips	
9	Row 9	0	0	0.0	0	1.000	0 kips	
10	Row 10	0	0	0.0	0	1.000	0 kips	
11	Row 11	0	0	0.0	0	1.000	0 kips	
12	Row 12	0	0	0.0	0	1.000	0 kips	
13	Row 13	0	0	0.0	0	1.000	0 kips	
14	Row 14	0	0	0.0	0	1.000	0 kips	
15	Row 15	0	0	0.0	0	1.000	0 kips	
			48		2304		**2304 kips**	**OK**

Case **Case 5**
Flood Event **Normal flow + ice**
Usual

Vertical Load, P = 3307 kips
Horizontal Load, H = 743 kips
M_{NA} = 140 kip-ft

	Vertical Pile Loading	P / N	+	M_{NA}* d / Σ I	= Pile Loads		**Axial Pile Load**
1	Row 1	68.9		0.6	69.4 kips/pile	34.7 tons/pile	34.7 tons/pile
2	Row 2	68.9		0.2	69.1 kips/pile	34.5 tons/pile	34.5 tons/pile
3	Row 3	68.9		-0.2	68.7 kips/pile	34.4 tons/pile	34.4 tons/pile
4	Row 4	68.9		-0.6	68.3 kips/pile	34.2 tons/pile	34.2 tons/pile
5	Row 5	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
6	Row 6	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
7	Row 7	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
8	Row 8	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
9	Row 9	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
10	Row 10	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
11	Row 11	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
12	Row 12	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
13	Row 13	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
14	Row 14	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
15	Row 15	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
					max:	**34.7 tons/pile**	**max: 34.7 tons/pile**

Assumed lateral Capacity: 23.0 kips/pile

	Horizontal Pile Capacity	**Batter "/ft**	**N**	Resistance due to Batter, kips	Resitance due to Bending, kips	Group Efficiency	Lateral Resitance	
1	Row 1	0	12	0.0	276	1.000	276 kips	
2	Row 2	0	12	0.0	276	1.000	276 kips	
3	Row 3	0	12	0.0	276	1.000	276 kips	
4	Row 4	0	12	0.0	276	1.000	276 kips	
5	Row 5	0	0	0.0	0	1.000	0 kips	
6	Row 6	0	0	0.0	0	1.000	0 kips	
7	Row 7	0	0	0.0	0	1.000	0 kips	
8	Row 8	0	0	0.0	0	1.000	0 kips	
9	Row 9	0	0	0.0	0	1.000	0 kips	
10	Row 10	0	0	0.0	0	1.000	0 kips	
11	Row 11	0	0	0.0	0	1.000	0 kips	
12	Row 12	0	0	0.0	0	1.000	0 kips	
13	Row 13	0	0	0.0	0	1.000	0 kips	
14	Row 14	0	0	0.0	0	1.000	0 kips	
15	Row 15	0	0	0.0	0	1.000	0 kips	
			48		1104		**1104 kips**	**OK**

Case **Case 6**
Flood Event **Construction**
Unusual

Vertical Load, P = 3307 kips
Horizontal Load, H = 743 kips
M_{NA} = 194 kip-ft

	Vertical Pile Loading	P / N	+	M_{NA}* d / Σ I	= Pile Loads		**Axial Pile Load**
1	Row 1	68.9		0.8	69.7 kips/pile	34.8 tons/pile	34.8 tons/pile
2	Row 2	68.9		0.3	69.1 kips/pile	34.6 tons/pile	34.6 tons/pile
3	Row 3	68.9		-0.3	68.6 kips/pile	34.3 tons/pile	34.3 tons/pile
4	Row 4	68.9		-0.8	68.1 kips/pile	34.1 tons/pile	34.1 tons/pile
5	Row 5	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
6	Row 6	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
7	Row 7	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
8	Row 8	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
9	Row 9	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile
10	Row 10	0.0		0.0	0.0 kips/pile	0.0 tons/pile	0.0 tons/pile

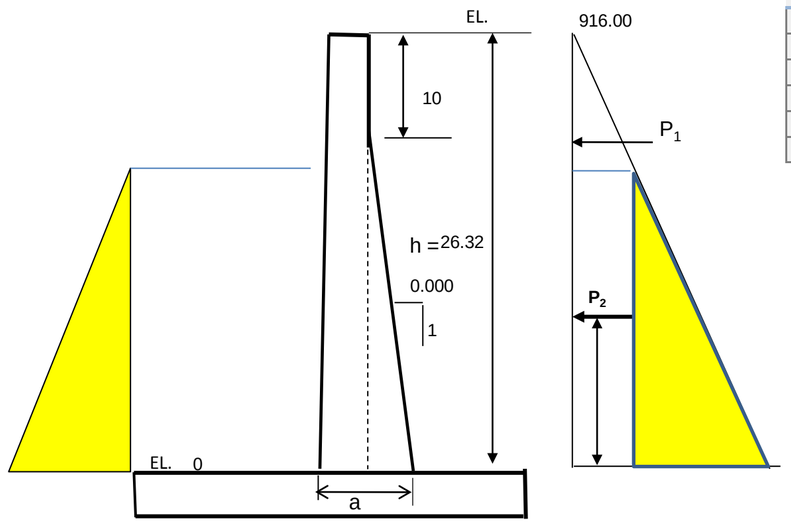
BARR ENGINEERING			DATE	2/11/2011	SHEET NO.
			PROJECT NAME	FARGO – MOORHEAD METRO FLOOD RISK MANAGEMENT PROJECT, FEASIBILITY STUDY, PHASE 4	
COMPUTED	CHECKED	SUBMITTED	PROJECT NUMBER	34091004	
MBI 2/11/11		MBI	SUBJECT	Sheyenne Aquaduct Structure - Retaining Walls Panel C	

11	Row 11	0.0	0.0	0.0 kips/pile		0.0 tons/pile		0.0 tons/pile	
12	Row 12	0.0	0.0	0.0 kips/pile		0.0 tons/pile		0.0 tons/pile	
13	Row 13	0.0	0.0	0.0 kips/pile		0.0 tons/pile		0.0 tons/pile	
14	Row 14	0.0	0.0	0.0 kips/pile		0.0 tons/pile		0.0 tons/pile	
15	Row 15	0.0	0.0	0.0 kips/pile		0.0 tons/pile		0.0 tons/pile	
					max:	**34.8 tons/pile**	**max:**	**34.8 tons/pile**	

Assumed lateral Capacity: 41.0 kips/pile

	Horizontal Pile Capacity	**Batter "/ft**	**N**	Resistance due to Batter, kips	Resitance due to Bending, kips	Group Efficiency	Lateral Resitance	
1	Row 1	0	12	0.0	276	1.000	276 kips	
2	Row 2	0	12	0.0	276	1.000	276 kips	
3	Row 3	0	12	0.0	276	1.000	276 kips	
4	Row 4	0	12	0.0	276	1.000	276 kips	
5	Row 5	0	0	0.0	0	1.000	0 kips	
6	Row 6	0	0	0.0	0	1.000	0 kips	
7	Row 7	0	0	0.0	0	1.000	0 kips	
8	Row 8	0	0	0.0	0	1.000	0 kips	
9	Row 9	0	0	0.0	0	1.000	0 kips	
10	Row 10	0	0	0.0	0	1.000	0 kips	
11	Row 11	0	0	0.0	0	1.000	0 kips	
12	Row 12	0	0	0.0	0	1.000	0 kips	
13	Row 13	0	0	0.0	0	1.000	0 kips	
14	Row 14	0	0	0.0	0	1.000	0 kips	
15	Row 15	0	0	0.0	0	1.000	0 kips	
			48		1104		**1104 kips**	**OK**

BARR ENGINEERING			DATE	2/11/2011	SHEET NO.
			PROJECT NAME	FARGO – MOORHEAD METRO FLOOD RISK MANAGEMENT PROJECT, FEASIBILITY STUDY, PHASE 4	
COMPUTED	CHECKED	SUBMITTED	PROJECT NUMBER	34091004	
MBI 2/11/11		MBI	SUBJECT	Sheyenne Aquaduct Structure - Retaining Walls Panel C 0	



CASE	Event		HW	TW	Dh	TW -ftg
Case 1	100 yr. flood	Usual	902.12	901.91	0.21	901.91
Case 2	100 yr. flood + ice	Unusual	902.12	901.91	0.21	901.91
Case 3	500 yr. flood	Unusual	914.670	903.06	11.61	903.06
Case 4	T.O. Levee	Extreme	916.000	916.00	0.00	916.00
Case 5	Normal flow + ice	Usual	0.000	0.000	0.00	0.00
Case 6	Construction	Unusual	0.000	0.000	0.00	0.00

LOAD FACTORS

Hf =	1.30	hydraulic Factor
LF =	1.70	
Unsual & Extreme =	0.75	
TOP THICK =	4.0 ft	48.0 in
Batter at Base =	0.00 ft	0.0 in
a =	4.00 ft	48.0 in

Load Factors - Hydraulic Structures	
live load, LL =	1.7
dead load, DL =	1.4
flood level , FL =	1
Fluid, F =	1.7
hydraulic, Hf =	1.3
direct tension hydraulic, Hf =	1.65
ICE =	1.7

WALL DESIGN:

Horizontal Load Components and Moments about Bottom of Stem (Service)

CASE	Event	Condition	Load Factor	H (kips/ft)	Moment (kip-ft/ ft)	Vu (kips/ft)	Mu (kip-ft/ ft)
Case 1	100 yr. flood	Usual	1	1.75	37.716	3.87	83.35
Case 2	100 yr. flood + ice	Unusual	0.75	1.75	37.716	2.91	62.51
Case 3	500 yr. flood	Unusual	0.75	0.78	31.346	1.29	51.96
Case 4	T.O. Levee	Extreme	0.75	-15.03	-131.885	24.92	218.60
Case 5	Normal flow + ice	Usual	1	6.58	57.738	14.54	127.60
Case 6	Construction	Unusual	0.75	6.58	57.738	10.91	95.70

STEM DESIGN VALUES

MU, k-ft/ft	218.60	k-ft/ft
VU, k/ft	24.92	k/ft

BARR ENGINEERING			DATE	2/11/2011	SHEET NO.
			PROJECT NAME	FARGO – MOORHEAD METRO FLOOD RISK MANAGEMENT PROJECT, FEASIBILITY STUDY, PHASE 4	
COMPUTED	CHECKED	SUBMITTED	PROJECT NUMBER	34091004	
MBI 2/11/11		MBI	SUBJECT	Sheyenne Aquaduct Structure - Retaining Walls Panel C 0	

ACI 318-05 w/ Modifications per EM 1110-2-2104 ref. EM 110-2-2104

9.3 - Design Strength

ϕ = **0.9** 9.3.2.1 - Tension Controlled sections

0.75 9.3.2.3 - Shear and torsion

FLEXURAL STEEL FOR RECTANGULAR CONCRETE SECTIONS

fy=	60	ksi	
Fc'=	4	ksi	
B1=	0.85		
Muh =	219	k-ft /ft	Includes: hf = 1.3
Vuh=	24.92	k / ft	
bw=	12	in.	
h=	48	in	
cover=	4	in (include correct stirrup bar dia.)	
d=	43.50	in	
pb=	0.0285		pb=0.85*B1*Fc'/ fy*(87 / (87+fy))
.75*pb=	0.0214		
m=fy / 0.85*Fc'=	17.647		

TRIAL

Ru=Mn/bd^2 = 128.360

REQ'D p= 0.0022 **O.K.**

p= 0.0029

As (REQ'D)= 1.52 in^2

ACI 10.5.1

p(min)= 3*SQRT(Fc')/fy 0.00316

200* / fy 0.00333

ACI 10.5.3

4/3*p 0.0029

EM 110-2-2104 2-8 c. (not less than Temp & Shrinkage, half in each face)

p(min)= 0.0028 /2 ▶ As =0.5*$p_{T\&S}$bh = 0.8064 in^2

As = #9 @ 12 = 1.00 in^2

SELECT STEEL

bar #=	9		
spacing, s=	6	in	
# OF BAR=	1	(ENTER 1 IF PER FT, b=12")	a
As=	1.999	in^2	
d=	43.4375	in	
p = As/bd =	0.0038	**O.K. < 0.375pb**	**EM 110-2-2104**
p =	**0.135**	**pb**	**MAXIMUM TENSILE REINFORCEMENT**
T= As*fy =	119.9	k	a) For singly reinforced flexural members
C= B1*Fc' *b*a =	743.2	**a**	1) p = **0.25** pb Recommended limit
a= T/C =	0.161	in	2) p = **0.375** pb Max. permitted upper limit not requiring special study
Mn= T(d - a/2)/12 =	433.3	ft-k	3) p = **0.5** pb Max. permitted upper limit when excessive deflections are not predicted In ACI 318
ϕ Mn=	389.9	ft-k	4) p = >**0.5** pb but ≤ 0.375 pb permitted only if detailed serviceability analysis incl. deflect. Calc.
			b) Use of compression reinf. shall be per ACI 318
			> Mu O.K.

CHECK SHEAR REINFORCEMENT (ACI 11.3 & EM 110-2-2104 3-3a)

Vuh =	24.9	k		NO SHEAR REINF. REQUIRED
Vn = Vuh / ϕ =	33.2	k		
Vc = 2*sqrt(Fc') bw * d =	65.9	k		11.3.1.1
Vs =Vuh / f - 1.3Vc =	No Shear Reinf. Req.	k	NG	Vs(max) ≤ 8*sqrt(fc')bd = 263.7 k

Trial Stirrup Sizes:

# of stirrup legs =	2	(single stirrup = 2, Dbl stirrup = 4……..)
Stirrup bar size =	4	
Av=	0.393	in^2
s=	0.000	in s = Av * fy * d / (Vu / f - Vc)

11.5.5 - Spacing limits for shear reinforcement

s = d/2 =	21.719	in	OR 24	in
s(max)=	10.859	in		
4*sqrt(Fc')*bw*d=	131.9	k	< Vs Reduce Spacing	
USE s=	**0.00**	in		
Vs = (Av * Fy * d) / s =	#DIV/0!	k		

11.5.6 - MINIMUM SHEAR REINFORCEMENT

A minimum area of shear reinforcement, Av,min shall be provided in all reinforced concrete flexural members where **Vu** exceeds **0.5 f Vc**

NOT REQUIRED IF:

a) SLAB OR FOOTING, vc>vn **O.K.**

b) CONCRETE JOIST ACI 8.11

c) BEAMS W/ h <= 10"

h <= 2.5*Bf

h <= 0.5*tw

d) WALLS (SEE ACI 11.10.1); vc>vn **O.K.**

11.5.6.3

Av,min = 0.75 sqrt(fc') bw*s/fy = 0.55 * s

but not less than 50bw*s/ fy = 18.33333333 * s

s max = Av fy / 0.75 sqrt(fc') bw = 0.00 in

s max = Av fy /50 bw = 0.00 in

11.5.5.3

Where Vs exceeds 4*sqrt(Fc')*bw*d maximum spacings shall be reduced by one-half