

# **APPENDIX J**



## **LEVEL II ROSGEN WORKSHEETS**

**Worksheet 2-1.** Gage station and field data (Rosgen and Silvey, 2007).

Summary.... <b>USGS GAGE STATION</b> Data/Records for <b>STREAM CHANNEL CLASSIFICATION</b>					
Station NAME:	Buffalo River-1-1.19			Station Number:	N/A
LOCATION:	Buffalo River-1-1.19				
Period of RECORD:	N/A	yrs	Mean Annual DISCHARGE:	N/A	cfs
Drainage AREA:	636224	acres	994.1	mi <sup>2</sup>	Drainage Area Mn ELEV: 848.05 ft
Reference REACH SLOPE:		ft/ft	Valley Type:	X	
Stream Type:	E6		HUC:	-- -- -- -- -- -- -- -- -- -- -- -- -- -- -- --	
"BANKFULL" CHARACTERISTICS					
Determined from FIELD MEASUREMENT			Determined from GAGE DATA Analysis		
Bankfull WIDTH ( $W_{bkf}$ )	73.1	ft	Bankfull WIDTH ( $W_{bkf}$ )		ft
Bankfull Mean DEPTH ( $d_{bkf}$ )	6.3	ft	Bankfull MEAN DEPTH ( $d_{bkf}$ )		ft
Bankfull Xsec AREA ( $A_{bkf}$ )	462.7	ft <sup>2</sup>	Bankfull Xsec AREA ( $A_{bkf}$ )		ft <sup>2</sup>
Wetted PERIMETER ( $W_p$ )	76.6	ft	Wetted PERIMETER ( $W_p$ )		ft
Bankfull STAGE (Gage Ht)		ft	Bankfull STAGE (Gage Ht)		ft
Est. Mean VELOCITY ( $u$ )	0.9	ft/sec	Mean VELOCITY ( $u$ )		ft/sec
Est. Bkf. DISCHARGE ( $Q_{bkf}$ )	420.0	cfs	Bankfull DISCHARGE ( $Q_{bkf}$ )		cfs
Bankfull DISCHARGE associated with "field-determined" Bankfull STAGE				420.0	cfs
Recurrence Interval ( Log-Pearson ) associated with "field-determined" Bankfull Discharge				1.04	yrs
From the Annual Peak Flow Frequency Analysis data for the Gage Station, determine:					
1.5 Year R.I. Discharge..... =	N/A	cfs	10 Year R.I. Discharge..... =	N/A	cfs
2.0 Year R.I. Discharge..... =	N/A	cfs	25 Year R.I. Discharge..... =	N/A	cfs
5.0 Year R.I. Discharge..... =	N/A	cfs	50 Year R.I. Discharge..... =	N/A	cfs
MEANDER GEOMETRY					
Meander Length ( $L_m$ )	681	ft	Radius of Curvature ( $R_C$ )	94.0	ft
Belt Width ( $W_{blt}$ )	953	ft	Meander Width Ratio ( $W_{blt}/W_{bkf}$ )	13.0	ft/ft
HYDRAULIC GEOMETRY					
Based on USGS Discharge Summary Notes data ( Form 9-207 ) and regression analyses of measured discharge ( $Q$ ) with the hydraulic parameters of Width ( $W$ ), Area ( $A$ ), Mean Depth ( $d$ ) & Mean Velocity ( $u$ ), determine the <i>intercept coefficient</i> ( $a$ ) and the <i>slope exponent</i> ( $b$ ) values for a power function of the form $Y = aX^b$ , when $Y$ is one of the selected hydraulic parameters and $X$ is a given discharge value ( $Q$ ).					
	Width ( $W$ )	Depth ( $d$ )	Area ( $A$ )	Velocity ( $u$ )	
Intercept Coefficient: ( $a$ )					
Slope Exponent: ( $b$ )					
Hydraulic Radius: $R = A / W_p$		ft	Manning's "n" at Bankfull Stage	0.035	Coeff.
$"n" = 1.4865 [ ( Area ) ( Hydraulic Radius^{2/3} ) ( Slope^{1/2} ) ] / Q_{bkf}$					

**Worksheet 2-2.** Computations of velocity and bankfull discharge using various methods (Rosgen, 2006b; Rosgen and Silvey, 2007).

Bankfull VELOCITY / DISCHARGE Estimates									
Site	Buffalo River-1-1.19			Location	Buffalo River-1-1.19				
Date	9/27/2011	Stream Type	E6	Valley Type	X				
Observers	KD, JB			HUC	-- -- -- -- -- -- -- -- -- --				
INPUT VARIABLES				OUTPUT VARIABLES					
Bankfull Cross-sectional	462.7	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Mean DEPTH	6.3	$D_{bkf}$ (ft)				
Bankfull WIDTH	73.1	$W_{bkf}$ (ft)	Wetted PERIMETER $\sim 2 * d_{bkf} + W_{bkf}$	85.7	$W_p$ (ft)				
$D_{84}$ @ Riffle	0.022	Dia. (mm)	$D_{84}$ mm / 304.8 =	0.0001	$D_{84}$ (ft)				
Bankfull SLOPE	0.00004	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	5.4	R (ft)				
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R (ft) / $D_{84}$ (ft)	74759					
Drainage AREA	994.1	DA (mi <sup>2</sup> )	Shear Velocity $u^* = \sqrt{gRS}$	0.08	$u^*$ (ft / sec)				
ESTIMATION METHODS				Bankfull VELOCITY		Bankfull DISCHARGE			
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 \text{Log}\{ R / D_{84} \} ] u^*$				2.4	ft / sec	1126	cfs		
2. Roughness Coefficient: a) Manning's 'n' from friction factor / relative roughness (Figs. 2-18, 19) $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text"/>				0.8	ft / sec	367	cfs		
2. Roughness Coefficient: b) Manning's 'n' from Jarrett ( USGS ): $n = 0.39S^{-.38R^{-.16}}$ n = <input type="text"/>				4.5	ft / sec	2087	cfs		
Note: This equation is for applications involving steep, step-pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for stream types A1, A2, A3, B1, B2, B3, C2 and E3.									
2. Roughness Coefficient: c) Manning's 'n' from Stream Type $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text" value="0.035"/>				0.8	ft / sec	367	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.) HEC-RAS				0.9	ft / sec	420	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.) <input type="text"/>					ft / sec		cfs		
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge $Q = 1.46$ Yr. $u = Q / A$					ft / sec		cfs		
4. Continuity Equations: b) USGS Gage Data $u = Q / A$					ft / sec		cfs		
Options for using the $D_{84}$ term in the relative roughness relation ( $R/D_{84}$ ), when using estimation method 1.									
Option 1. For sand-bed channels: Measure the "protrusion height" ( $h_{sd}$ ) of sand dunes above channel bed elevations. Substitute an average sand dune protrusion height ( $h_{sd}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 2. For boulder-dominated channels: Measure several "protrusion heights" ( $h_{bo}$ ) of boulders above channel bed elevations. Substitute an ave. boulder protrusion height ( $h_{bo}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 3. For bedrock-dominated channels: Measure several "protrusion heights" ( $h_{br}$ ) of rock separations/steps/joints/uplifted surfaces above channel bed elevations. Substitute an average bedrock protrusion height ( $h_{br}$ in feet) for the $D_{84}$ term in estimation method 1.									

**Worksheet 2-3.** Field form for Level II stream classification (Rosgen, 1996; Rosgen , 2006b).

Stream: <b>Buffalo River-1-1.19</b>	
Basin: <b>Red River Basin</b>	Drainage Area: <b>636224</b> acres <b>994.1</b> mi <sup>2</sup>
Location: <b>Buffalo River-1-1.19</b>	
Twp.&Rge: - Sec.&Qtr.: -	
Cross-Section Monuments (Lat./Long.): - Date: <b>9/27/2011</b>	
Observers: <b>KD, JB</b> Valley Type: <b>X</b>	

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>73.1</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>6.3</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>462.7</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>11.5</b>	ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>9.0</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>196.0</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>2.7</b>	ft/ft
<b>Channel Materials (Particle Size Index ) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>0.0015</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.000037</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).	<b>2.2</b>	

<b>Stream Type</b>	<b>E6</b>	<b>See Classification Key (Figure 2-21)</b>
--------------------	-----------	---

**Worksheet 2-4.** Morphological relations, including dimensionless ratios of river reach sites (Rosgen, 2006b; Rosgen and Silvey 2007).

Stream: <b>Buffalo River-1-1.19</b>		Location: <b>Buffalo River-1-1.19</b>								
Observers: <b>KD, JB</b>		Date: <b>9/27/2011</b>		Valley Type: <b>X</b>		Stream Type: <b>E6</b>				
<b>River Reach Summary Data</b>										
<b>Channel Dimension</b>	Mean Riffle Depth ( $d_{bkt}$ )	<b>6.3</b>	ft	Riffle Width ( $W_{bkt}$ )	<b>73.1</b>	ft	Riffle Area ( $A_{bkt}$ )	<b>462.7</b>	ft <sup>2</sup>	
	Mean Pool Depth ( $d_{bkfp}$ )		ft	Pool Width ( $W_{bkfp}$ )		ft	Pool Area ( $A_{bkfp}$ )		ft <sup>2</sup>	
	Mean Pool Depth/Mean Riffle Depth		$\frac{d_{bkfp}}{d_{bkt}}$	Pool Width/Riffle Width		$\frac{W_{bkfp}}{W_{bkt}}$	Pool Area / Riffle Area		$\frac{A_{bkfp}}{A_{bkt}}$	
	Max Riffle Depth ( $d_{maxrif}$ )	<b>9.01</b>	ft	Max Pool Depth ( $d_{maxp}$ )		ft	Max Riffle Depth/Mean Riffle Depth	<b>1.4</b>		
	Max Pool Depth/Mean Riffle Depth			Point Bar Slope		ft/ft	Inner Berm Width ( $W_{ib}$ )		ft	
	Inner Berm Depth ( $d_{ib}$ )		ft	Inner Berm Width/Depth Ratio			$W_{ib}/d_{ib}$	Inner Berm Area ( $A_{ib}$ )		ft <sup>2</sup>
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )				<b>0.9</b>	ft/s	Estimation Method		<b>HEC-RAS</b>	
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )				<b>420</b>	cfs	Drainage Area		<b>994.1</b>	mi <sup>2</sup>

<b>Channel Pattern</b>	Geometry			Dimensionless Geometry Ratios			
	Mean	Min	Max	Mean	Min	Max	
	Meander Wavelength ( $L_m$ )	<b>681</b>			ft	Meander Length Ratio ( $L_m/W_{bkt}$ )	<b>9.3</b>
	Radius of Curvature ( $R_c$ )	<b>94</b>			ft	Radius of Curvature/Riffle Width ( $R_c/W_{bkt}$ )	<b>1.3</b>
	Belt Width ( $W_{bt}$ )	<b>953</b>			ft	Meander Width Ratio ( $W_{bt}/W_{bkt}$ )	<b>13.0</b>
	Individual Pool Length				ft	Pool Length/Riffle Width	
	Pool to Pool Spacing				ft	Pool to Pool Spacing/Riffle Width	
Riffle Length				ft	Riffle Length/Riffle Width		

<b>Channel Profile</b>	Valley Slope (VS)		ft/ft	Average Water Surface Slope (S)		ft/ft	Sinuosity (VS/S)		
	Stream Length (SL)	<b>17491</b>	ft	Valley Length (VL)	<b>8114</b>	ft	Sinuosity (SL/VL)	<b>2.2</b>	
	Low Bank Height (LBH)	start	ft	Max Riffle Depth	start	ft	Bank-Height Ratio (BHR) (LBH/Max Riffle Depth)	start	
		end	ft		end	ft		end	
	Facet Slopes			Dimensionless Slope Ratios			Mean	Min	Max
	Riffle Slope ( $S_{rif}$ )	<b>0.0</b>		ft/ft	Riffle Slope/Average Water Surface Slope ( $S_{rif} / S$ )	<b>1.0</b>			
	Run Slope ( $S_{run}$ )			ft/ft	Run Slope/Average Water Surface Slope ( $S_{run} / S$ )				
	Pool Slope ( $S_p$ )			ft/ft	Pool Slope/Average Water Surface Slope ( $S_p / S$ )				
	Glide Slope ( $S_g$ )			ft/ft	Glide Slope/Average Water Surface Slope ( $S_g / S$ )				
	Feature Midpoint <sup>a</sup>			Dimensionless Depth Ratios			Mean	Min	Max
	Max Riffle Depth ( $d_{maxrif}$ )	<b>9.0</b>		ft	Max Riffle Depth/Mean Riffle Depth ( $d_{maxrif} / d_{bkt}$ )	<b>1.4</b>			
	Max Run Depth ( $d_{maxrun}$ )			ft	Max Run Depth/Mean Riffle Depth ( $d_{maxrun} / d_{bkt}$ )				
	Max Pool Depth ( $d_{maxp}$ )			ft	Max Pool Depth/Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )				
Max Glide Depth ( $d_{maxg}$ )			ft	Max Glide Depth/Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )					

<b>Channel Materials</b>	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Protrusion Height <sup>d</sup>	
	% Silt/Clay	<b>98</b>			$D_{16}$	<b>&lt;.001</b>		mm
	% Sand	<b>2</b>			$D_{35}$	<b>&lt;.001</b>		mm
	% Gravel	<b>0</b>			$D_{50}$	<b>0.0015</b>		mm
	% Cobble	<b>0</b>			$D_{84}$	<b>0.022</b>		mm
	% Boulder	<b>0</b>			$D_{95}$	<b>0.063</b>		mm
	% Bedrock	<b>0</b>			$D_{100}$	<b>4.75</b>		mm

<sup>a</sup> Min, max, mean depths are ave. mid-point values except pools: taken at deepest part of pool.

<sup>b</sup> Composite sample of riffles and pools within the designated reach.

<sup>c</sup> Active bed of a riffle.

<sup>d</sup> Height of roughness feature above bed.

**Worksheet 2-1.** Gage station and field data (Rosgen and Silvey, 2007).

Summary.... <b>USGS GAGE STATION</b> Data/Records for <b>STREAM CHANNEL CLASSIFICATION</b>							
Station NAME:	Wolverton Creek - 1 - 0.64				Station Number:	N/A	
LOCATION:	Wolverton Creek - 1 - 0.64						
Period of RECORD:	N/A		yrs	Mean Annual DISCHARGE:	N/A		cfs
Drainage AREA:	65920	acres	103	mi <sup>2</sup>	Drainage Area Mn ELEV:	885.63	ft
Reference REACH SLOPE:				ft/ft	Valley Type:	X	
Stream Type:	B6c		HUC: _____				
"BANKFULL" CHARACTERISTICS							
Determined from FIELD MEASUREMENT				Determined from GAGE DATA Analysis			
Bankfull WIDTH ( $W_{bkf}$ )	25.4	ft		Bankfull WIDTH ( $W_{bkf}$ )		ft	
Bankfull Mean DEPTH ( $d_{bkf}$ )	2.1	ft		Bankfull MEAN DEPTH ( $d_{bkf}$ )		ft	
Bankfull Xsec AREA ( $A_{bkf}$ )	53.7	ft <sup>2</sup>		Bankfull Xsec AREA ( $A_{bkf}$ )		ft <sup>2</sup>	
Wetted PERIMETER ( $W_p$ )	26.9	ft		Wetted PERIMETER ( $W_p$ )		ft	
Bankfull STAGE (Gage Ht)		ft		Bankfull STAGE (Gage Ht)		ft	
Est. Mean VELOCITY ( $u$ )	2.5	ft/sec		Mean VELOCITY ( $u$ )		ft/sec	
Est. Bkf. DISCHARGE ( $Q_{bkf}$ )	130.0	cfs		Bankfull DISCHARGE ( $Q_{bkf}$ )		cfs	
Bankfull DISCHARGE associated with "field-determined" Bankfull STAGE					130.0	cfs	
Recurrence Interval ( Log-Pearson ) associated with "field-determined" Bankfull Discharge					1.1	yrs	
From the Annual Peak Flow Frequency Analysis data for the Gage Station, determine:							
1.5 Year R.I. Discharge..... =	N/A	cfs		10 Year R.I. Discharge..... =	N/A	cfs	
2.0 Year R.I. Discharge..... =	N/A	cfs		25 Year R.I. Discharge..... =	N/A	cfs	
5.0 Year R.I. Discharge..... =	N/A	cfs		50 Year R.I. Discharge..... =	N/A	cfs	
MEANDER GEOMETRY							
Meander Length ( $L_m$ )	314	ft		Radius of Curvature ( $R_C$ )	57.0	ft	
Belt Width ( $W_{blt}$ )	656	ft		Meander Width Ratio ( $W_{blt}/W_{bkf}$ )	25.8	ft/ft	
HYDRAULIC GEOMETRY							
Based on USGS Discharge Summary Notes data ( Form 9-207 ) and regression analyses of measured discharge ( $Q$ ) with the hydraulic parameters of Width ( $W$ ), Area ( $A$ ), Mean Depth ( $d$ ) & Mean Velocity ( $u$ ), determine the <i>intercept coefficient</i> ( $a$ ) and the <i>slope exponent</i> ( $b$ ) values for a power function of the form $Y = aX^b$ , when $Y$ is one of the selected hydraulic parameters and $X$ is a given discharge value ( $Q$ ).							
		Width ( $W$ )	Depth ( $d$ )	Area ( $A$ )	Velocity ( $u$ )		
Intercept Coefficient:	( $a$ )						
Slope Exponent:	( $b$ )						
Hydraulic Radius: $R = A / W_p$			ft	Manning's "n" at Bankfull Stage		0.045	Coeff.
$"n" = 1.4865 [ ( Area ) ( Hydraulic Radius^{2/3} ) ( Slope^{1/2} ) ] / Q_{bkf}$							

**Worksheet 2-2.** Computations of velocity and bankfull discharge using various methods (Rosgen, 2006b; Rosgen and Silvey, 2007).

Bankfull VELOCITY / DISCHARGE Estimates									
Site	Wolverton Creek - 1 - 0.64			Location	Wolverton Creek - 1 - 0.64				
Date	9/28/2011	Stream Type	B6c	Valley Type	X				
Observers	KP, AL			HUC	-- -- -- -- -- -- -- -- -- --				
INPUT VARIABLES				OUTPUT VARIABLES					
Bankfull Cross-sectional	53.7	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Mean DEPTH	2.1	$D_{bkf}$ (ft)				
Bankfull WIDTH	25.4	$W_{bkf}$ (ft)	Wetted PERIMETER $\sim 2 * d_{bkf} + W_{bkf}$	29.6	$W_p$ (ft)				
$D_{84}$ @ Riffle	0.01	Dia. (mm)	$D_{84}$ mm / 304.8 =	0.00	$D_{84}$ (ft)				
Bankfull SLOPE	0.0012	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	1.8	R (ft)				
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R (ft) / $D_{84}$ (ft)	55337					
Drainage AREA	103.0	DA (mi <sup>2</sup> )	Shear Velocity $u^* = \sqrt{gRS}$	0.3	$u^*$ (ft / sec)				
ESTIMATION METHODS				Bankfull VELOCITY		Bankfull DISCHARGE			
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 \text{Log}\{ R / D_{84} \} ] u^*$				8.0	ft / sec	429	cfs		
2. Roughness Coefficient: a) Manning's 'n' from friction factor / relative roughness (Figs. 2-18, 19) $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text"/>				1.7	ft / sec	93	cfs		
2. Roughness Coefficient: $u = 1.4865 * R^{2/3} * S^{1/2} / n$ b) Manning's 'n' from Jarrett ( USGS ): $n = 0.39S^{-.38R^{-.16}}$ n = <input type="text"/>				2.8	ft / sec	150	cfs		
Note: This equation is for applications involving steep, step-pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for stream types A1, A2, A3, B1, B2, B3, C2 and E3.									
2. Roughness Coefficient: c) Manning's 'n' from Stream Type $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text" value="0.045"/>				1.7	ft / sec	93	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.) HEC-RAS				2.5	ft / sec	130	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.)					ft / sec		cfs		
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge Q = <input type="text" value="1.46"/> Yr. $u = Q / A$					ft / sec		cfs		
4. Continuity Equations: b) USGS Gage Data $u = Q / A$					ft / sec		cfs		
Options for using the $D_{84}$ term in the relative roughness relation ( $R/D_{84}$ ), when using estimation method 1.									
Option 1. For sand-bed channels: Measure the "protrusion height" ( $h_{sd}$ ) of sand dunes above channel bed elevations. Substitute an average sand dune protrusion height ( $h_{sd}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 2. For boulder-dominated channels: Measure several "protrusion heights" ( $h_{bo}$ ) of boulders above channel bed elevations. Substitute an ave. boulder protrusion height ( $h_{bo}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 3. For bedrock-dominated channels: Measure several "protrusion heights" ( $h_{br}$ ) of rock separations/steps/joints/uplifted surfaces above channel bed elevations. Substitute an average bedrock protrusion height ( $h_{br}$ in feet) for the $D_{84}$ term in estimation method 1.									

**Worksheet 2-3.** Field form for Level II stream classification (Rosgen, 1996; Rosgen, 2006b).

Stream: <b>Wolverton Creek - 1 - 0.64</b>	
Basin: <b>Red River Basin</b>	Drainage Area: <b>65920</b> acres <b>103</b> mi <sup>2</sup>
Location: <b>Wolverton Creek - 1 - 0.64</b>	
Twp.&Rge: - Sec.&Qtr.: -	
Cross-Section Monuments (Lat./Long.): - Date: <b>9/28/2011</b>	
Observers: <b>KP, AL</b> Valley Type: <b>X</b>	

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>25.4</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>2.1</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>53.7</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>12.2</b>	ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>3.3</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>47.5</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>1.9</b>	ft/ft
<b>Channel Materials (Particle Size Index) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>&lt;0.001</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.0012</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).	<b>1.7</b>	

<b>Stream Type</b>	<b>B6c</b>	<b>See Classification Key (Figure 2-21)</b>
--------------------	------------	---

**Worksheet 2-4.** Morphological relations, including dimensionless ratios of river reach sites (Rosgen, 2006b; Rosgen and Silvey 2007).

Stream: <b>Wolverton Creek - 1 - 0.64</b>		Location: <b>Wolverton Creek - 1 - 0.64</b>								
Observers: <b>KP, AL</b>		Date: <b>9/28/2011</b>		Valley Type: <b>X</b>		Stream Type: <b>B6c</b>				
<b>River Reach Summary Data</b>										
<b>Channel Dimension</b>	Mean Riffle Depth ( $d_{bkt}$ )	<b>2.09</b>	ft	Riffle Width ( $W_{bkt}$ )	<b>25.4</b>	ft	Riffle Area ( $A_{bkt}$ )	<b>53.7</b>	ft <sup>2</sup>	
	Mean Pool Depth ( $d_{bkfp}$ )		ft	Pool Width ( $W_{bkfp}$ )		ft	Pool Area ( $A_{bkfp}$ )		ft <sup>2</sup>	
	Mean Pool Depth/Mean Riffle Depth		$d_{bkfp}/d_{bkt}$	Pool Width/Riffle Width		$W_{bkfp}/W_{bkt}$	Pool Area / Riffle Area		$A_{bkfp}/A_{bkt}$	
	Max Riffle Depth ( $d_{maxrif}$ )	<b>3.3</b>	ft	Max Pool Depth ( $d_{maxp}$ )		ft	Max Riffle Depth/Mean Riffle Depth	<b>1.6</b>		
	Max Pool Depth/Mean Riffle Depth			Point Bar Slope		ft/ft	Inner Berm Width ( $W_{ib}$ )		ft	
	Inner Berm Depth ( $d_{ib}$ )		ft	Inner Berm Width/Depth Ratio			$W_{ib}/d_{ib}$	Inner Berm Area ( $A_{ib}$ )		ft <sup>2</sup>
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )			<b>2.5</b>	ft/s	Estimation Method	<b>HEC-RAS</b>			
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )			<b>130</b>	cfs	Drainage Area	<b>103</b>	mi <sup>2</sup>		

<b>Channel Pattern</b>	Geometry			Dimensionless Geometry Ratios			
	Mean	Min	Max	Mean	Min	Max	
	Meander Wavelength ( $L_m$ )	<b>314</b>			ft	Meander Length Ratio ( $L_m/W_{bkt}$ )	<b>12.4</b>
	Radius of Curvature ( $R_c$ )	<b>57</b>			ft	Radius of Curvature/Riffle Width ( $R_c/W_{bkt}$ )	<b>2.2</b>
	Belt Width ( $W_{bit}$ )	<b>656</b>			ft	Meander Width Ratio ( $W_{bit}/W_{bkt}$ )	<b>25.8</b>
	Individual Pool Length				ft	Pool Length/Riffle Width	
	Pool to Pool Spacing				ft	Pool to Pool Spacing/Riffle Width	
Riffle Length				ft	Riffle Length/Riffle Width		

<b>Channel Profile</b>	Valley Slope (VS)		ft/ft	Average Water Surface Slope (S)		ft/ft	Sinuosity (VS/S)		
	Stream Length (SL)	<b>8458</b>	ft	Valley Length (VL)	<b>4883</b>	ft	Sinuosity (SL/VL)	<b>1.7</b>	
	Low Bank Height (LBH)	start	ft	Max Riffle Depth	start	ft	Bank-Height Ratio (BHR)	start	
		end	ft		end	ft	(LBH/Max Riffle Depth)	end	
	Facet Slopes			Dimensionless Slope Ratios			Mean	Min	Max
	Riffle Slope ( $S_{rif}$ )	<b>0.0</b>		ft/ft	Riffle Slope/Average Water Surface Slope ( $S_{rif}/S$ )	<b>1.0</b>			
	Run Slope ( $S_{run}$ )			ft/ft	Run Slope/Average Water Surface Slope ( $S_{run}/S$ )				
	Pool Slope ( $S_p$ )			ft/ft	Pool Slope/Average Water Surface Slope ( $S_p/S$ )				
	Glide Slope ( $S_g$ )			ft/ft	Glide Slope/Average Water Surface Slope ( $S_g/S$ )				
	Feature Midpoint <sup>a</sup>			Dimensionless Depth Ratios			Mean	Min	Max
	Max Riffle Depth ( $d_{maxrif}$ )	<b>3.3</b>		ft	Max Riffle Depth/Mean Riffle Depth ( $d_{maxrif}/d_{bkt}$ )	<b>1.6</b>			
	Max Run Depth ( $d_{maxrun}$ )			ft	Max Run Depth/Mean Riffle Depth ( $d_{maxrun}/d_{bkt}$ )				
	Max Pool Depth ( $d_{maxp}$ )			ft	Max Pool Depth/Mean Riffle Depth ( $d_{maxp}/d_{bkt}$ )				
Max Glide Depth ( $d_{maxg}$ )			ft	Max Glide Depth/Mean Riffle Depth ( $d_{maxg}/d_{bkt}$ )					

<b>Channel Materials</b>	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Protrusion Height <sup>d</sup>	
	% Silt/Clay	<b>92</b>			$D_{16}$	<b>&lt;.001</b>		mm
	% Sand	<b>8</b>			$D_{35}$	<b>&lt;.001</b>		mm
	% Gravel	<b>0</b>			$D_{50}$	<b>&lt;.001</b>		mm
	% Cobble	<b>0</b>			$D_{84}$	<b>0.01</b>		mm
	% Boulder	<b>0</b>			$D_{95}$	<b>0.25</b>		mm
	% Bedrock	<b>0</b>			$D_{100}$	<b>1</b>		mm

<sup>a</sup> Min, max, mean depths are ave. mid-point values except pools: taken at deepest part of pool.

<sup>b</sup> Composite sample of riffles and pools within the designated reach.

<sup>c</sup> Active bed of a riffle.

<sup>d</sup> Height of roughness feature above bed.

**Worksheet 2-1.** Gage station and field data (Rosgen and Silvey, 2007).

Summary.... <b>USGS GAGE STATION</b> Data/Records for <b>STREAM CHANNEL CLASSIFICATION</b>					
Station NAME:	Wild Rice River-6-42.36			Station Number:	N/A
LOCATION:	Wild Rice River-6-42.36				
Period of RECORD:	N/A yrs		Mean Annual DISCHARGE:	N/A cfs	
Drainage AREA:	1182080 acres	1847 mi <sup>2</sup>	Drainage Area Mn ELEV:	904.68 ft	
Reference REACH SLOPE:	ft/ft		Valley Type:	X	
Stream Type:	E6		HUC:	-- -- -- -- --	
"BANKFULL" CHARACTERISTICS					
Determined from FIELD MEASUREMENT			Determined from GAGE DATA Analysis		
Bankfull WIDTH ( $W_{bkf}$ )	76.2	ft	Bankfull WIDTH ( $W_{bkf}$ )		ft
Bankfull Mean DEPTH ( $d_{bkf}$ )	6.1	ft	Bankfull MEAN DEPTH ( $d_{bkf}$ )		ft
Bankfull Xsec AREA ( $A_{bkf}$ )	462.2	ft <sup>2</sup>	Bankfull Xsec AREA ( $A_{bkf}$ )		ft <sup>2</sup>
Wetted PERIMETER ( $W_p$ )	80.1	ft	Wetted PERIMETER ( $W_p$ )		ft
Bankfull STAGE (Gage Ht)		ft	Bankfull STAGE (Gage Ht)		ft
Est. Mean VELOCITY ( $u$ )	1.1	ft/sec	Mean VELOCITY ( $u$ )		ft/sec
Est. Bkf. DISCHARGE ( $Q_{bkf}$ )	517.0	cfs	Bankfull DISCHARGE ( $Q_{bkf}$ )		cfs
Bankfull DISCHARGE associated with "field-determined" Bankfull STAGE				517.0	cfs
Recurrence Interval ( Log-Pearson ) associated with "field-determined" Bankfull Discharge				1.3	yrs
From the Annual Peak Flow Frequency Analysis data for the Gage Station, determine:					
1.5 Year R.I. Discharge..... =	N/A	cfs	10 Year R.I. Discharge..... =	N/A	cfs
2.0 Year R.I. Discharge..... =	N/A	cfs	20 Year R.I. Discharge..... =	N/A	cfs
5.0 Year R.I. Discharge..... =	N/A	cfs	50 Year R.I. Discharge..... =	N/A	cfs
MEANDER GEOMETRY					
Meander Length ( $L_m$ )	1353	ft	Radius of Curvature ( $R_C$ )	328.0	ft
Belt Width ( $W_{blt}$ )	2214	ft	Meander Width Ratio ( $W_{blt}/W_{bkf}$ )	29.1	ft/ft
HYDRAULIC GEOMETRY					
Based on USGS Discharge Summary Notes data ( Form 9-207 ) and regression analyses of measured discharge ( $Q$ ) with the hydraulic parameters of Width ( $W$ ), Area ( $A$ ), Mean Depth ( $d$ ) & Mean Velocity ( $u$ ), determine the <i>intercept coefficient</i> ( $a$ ) and the <i>slope exponent</i> ( $b$ ) values for a power function of the form $Y = aX^b$ , when $Y$ is one of the selected hydraulic parameters and $X$ is a given discharge value ( $Q$ ).					
	Width ( $W$ )	Depth ( $d$ )	Area ( $A$ )	Velocity ( $u$ )	
Intercept Coefficient: ( $a$ )					
Slope Exponent: ( $b$ )					
Hydraulic Radius: $R = A / W_p$		ft	Manning's "n" at Bankfull Stage	0.043	Coeff.
$"n" = 1.4865 [ ( Area ) ( Hydraulic Radius^{2/3} ) ( Slope^{1/2} ) ] / Q_{bkf}$					

**Worksheet 2-2.** Computations of velocity and bankfull discharge using various methods (Rosgen, 2006b; Rosgen and Silvey, 2007).

Bankfull VELOCITY / DISCHARGE Estimates									
Site	Wild Rice River-6-42.36			Location	Wild Rice River-6-42.36				
Date	10/1/2011	Stream Type	E6	Valley Type	X				
Observers	KD, JB			HUC	-- -- -- -- --				
INPUT VARIABLES				OUTPUT VARIABLES					
Bankfull Cross-sectional	462.2	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Mean DEPTH	6.1	$D_{bkf}$ (ft)				
Bankfull WIDTH	76.2	$W_{bkf}$ (ft)	Wetted PERIMETER ~ 2 * $d_{bkf}$ + $W_{bkf}$	88.3	$W_p$ (ft)				
$D_{84}$ @ Riffle	0.073	Dia. (mm)	$D_{84}$ mm / 304.8 =	0.00	$D_{84}$ (ft)				
Bankfull SLOPE	0.0001	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	5.2	R (ft)				
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R (ft) / $D_{84}$ (ft)	21845					
Drainage AREA	1847.0	DA (mi <sup>2</sup> )	Shear Velocity $u^* = \sqrt{gRS}$	0.1	$u^*$ (ft / sec)				
ESTIMATION METHODS				Bankfull VELOCITY		Bankfull DISCHARGE			
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 \text{Log}\{ R / D_{84} \} ] u^*$				3.3	ft / sec	1545	cfs		
2. Roughness Coefficient: a) Manning's 'n' from friction factor / relative roughness (Figs. 2-18, 19) $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text"/>				1.0	ft / sec	453	cfs		
2. Roughness Coefficient: $u = 1.4865 * R^{2/3} * S^{1/2} / n$ b) Manning's 'n' from Jarrett ( USGS ): $n = 0.39S^{-.38}R^{-.16}$ n = <input type="text"/>				4.9	ft / sec	2258	cfs		
Note: This equation is for applications involving steep, step-pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for stream types A1, A2, A3, B1, B2, B3, C2 and E3.									
2. Roughness Coefficient: c) Manning's 'n' from Stream Type $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text" value="0.043"/>				1.0	ft / sec	453	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.) HEC-RAS				1.1	ft / sec	517	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.)					ft / sec		cfs		
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge $Q = 1.46$ Yr. $u = Q / A$					ft / sec		cfs		
4. Continuity Equations: b) USGS Gage Data $u = Q / A$					ft / sec		cfs		
Options for using the $D_{84}$ term in the relative roughness relation ( $R/D_{84}$ ), when using estimation method 1.									
Option 1. For sand-bed channels: Measure the "protrusion height" ( $h_{sd}$ ) of sand dunes above channel bed elevations. Substitute an average sand dune protrusion height ( $h_{sd}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 2. For boulder-dominated channels: Measure several "protrusion heights" ( $h_{bo}$ ) of boulders above channel bed elevations. Substitute an ave. boulder protrusion height ( $h_{bo}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 3. For bedrock-dominated channels: Measure several "protrusion heights" ( $h_{br}$ ) of rock separations/steps/joints/uplifted surfaces above channel bed elevations. Substitute an average bedrock protrusion height ( $h_{br}$ in feet) for the $D_{84}$ term in estimation method 1.									

**Worksheet 2-3.** Field form for Level II stream classification (Rosgen, 1996; Rosgen , 2006b).

Stream: <b>Wild Rice River-6-42.36</b>	
Basin: <b>Red River Basin</b>	Drainage Area: <b>1E+06</b> acres <b>1847</b> mi <sup>2</sup>
Location: <b>Wild Rice River-6-42.36</b>	
Twp.&Rge: - Sec.&Qtr.: -	
Cross-Section Monuments (Lat./Long.): - Date: <b>10/1/2011</b>	
Observers: <b>KD, JB</b> Valley Type: <b>X</b>	

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>76.2</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>6.1</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>462.2</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>12.6</b>	ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>8.4</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>157.7</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>2.1</b>	ft/ft
<b>Channel Materials (Particle Size Index ) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>0.0027</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.000088</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).	<b>2.7</b>	

<b>Stream Type</b>	<b>E6</b>	<b>See Classification Key (Figure 2-21)</b>
--------------------	-----------	---

**Worksheet 2-4.** Morphological relations, including dimensionless ratios of river reach sites (Rosgen, 2006b; Rosgen and Silvey 2007).

Stream: <b>Wild Rice River-6-42.36</b>		Location: <b>Wild Rice River-6-42.36</b>								
Observers: <b>KD, JB</b>		Date: <b>10/1/2011</b>		Valley Type: <b>X</b>		Stream Type: <b>E6</b>				
River Reach Summary Data										
Channel Dimension	Mean Riffle Depth ( $d_{bkt}$ )	<b>6.1</b>	ft	Riffle Width ( $W_{bkt}$ )	<b>76.2</b>	ft	Riffle Area ( $A_{bkt}$ )	<b>462.2</b>	ft <sup>2</sup>	
	Mean Pool Depth ( $d_{bkfp}$ )		ft	Pool Width ( $W_{bkfp}$ )		ft	Pool Area ( $A_{bkfp}$ )		ft <sup>2</sup>	
	Mean Pool Depth/Mean Riffle Depth		$d_{bkfp}/d_{bkt}$	Pool Width/Riffle Width		$W_{bkfp}/W_{bkt}$	Pool Area / Riffle Area		$A_{bkfp}/A_{bkt}$	
	Max Riffle Depth ( $d_{maxrif}$ )	<b>8.4</b>	ft	Max Pool Depth ( $d_{maxp}$ )		ft	Max Riffle Depth/Mean Riffle Depth	<b>1.4</b>		
	Max Pool Depth/Mean Riffle Depth			Point Bar Slope		ft/ft	Inner Berm Width ( $W_{ib}$ )		ft	
	Inner Berm Depth ( $d_{ib}$ )		ft	Inner Berm Width/Depth Ratio			$W_{ib}/d_{ib}$	Inner Berm Area ( $A_{ib}$ )		ft <sup>2</sup>
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )				<b>1.1</b>	ft/s	Estimation Method		<b>HEC-RAS</b>	
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )				<b>517</b>	cfs	Drainage Area		<b>1847</b>	mi <sup>2</sup>

Channel Pattern	Geometry	Mean	Min	Max	Dimensionless Geometry Ratios	Mean	Min	Max	
	Meander Wavelength ( $L_m$ )	<b>1353</b>			ft	Meander Length Ratio ( $L_m/W_{bkt}$ )	<b>17.8</b>		
	Radius of Curvature ( $R_c$ )	<b>328</b>			ft	Radius of Curvature/Riffle Width ( $R_c/W_{bkt}$ )	<b>4.3</b>		
	Belt Width ( $W_{bit}$ )	<b>2214</b>			ft	Meander Width Ratio ( $W_{bit}/W_{bkt}$ )	<b>29.1</b>		
	Individual Pool Length				ft	Pool Length/Riffle Width			
	Pool to Pool Spacing				ft	Pool to Pool Spacing/Riffle Width			
	Riffle Length				ft	Riffle Length/Riffle Width			

Channel Profile	Valley Slope (VS)			ft/ft	Average Water Surface Slope (S)			ft/ft	Sinuosity (VS/S)	
	Stream Length (SL)	<b>14371</b>		ft	Valley Length (VL)	<b>5318</b>		ft	Sinuosity (SL/VL)	<b>2.7</b>
	Low Bank Height (LBH)	start		ft	Max Riffle Depth	start		ft	Bank-Height Ratio (BHR) (LBH/Max Riffle Depth)	start
		end		ft		end		ft		end
	Facet Slopes	Mean	Min	Max	Dimensionless Slope Ratios	Mean	Min	Max		
	Riffle Slope ( $S_{rif}$ )	<b>0.0</b>			ft/ft	Riffle Slope/Average Water Surface Slope ( $S_{rif}/S$ )	<b>1.0</b>			
	Run Slope ( $S_{run}$ )				ft/ft	Run Slope/Average Water Surface Slope ( $S_{run}/S$ )				
	Pool Slope ( $S_p$ )				ft/ft	Pool Slope/Average Water Surface Slope ( $S_p/S$ )				
	Glide Slope ( $S_g$ )				ft/ft	Glide Slope/Average Water Surface Slope ( $S_g/S$ )				
	Feature Midpoint <sup>a</sup>	Mean	Min	Max	Dimensionless Depth Ratios	Mean	Min	Max		
	Max Riffle Depth ( $d_{maxrif}$ )	<b>8.4</b>			ft	Max Riffle Depth/Mean Riffle Depth ( $d_{maxrif}/d_{bkt}$ )	<b>1.4</b>			
	Max Run Depth ( $d_{maxrun}$ )				ft	Max Run Depth/Mean Riffle Depth ( $d_{maxrun}/d_{bkt}$ )				
	Max Pool Depth ( $d_{maxp}$ )				ft	Max Pool Depth/Mean Riffle Depth ( $d_{maxp}/d_{bkt}$ )				
	Max Glide Depth ( $d_{maxg}$ )				ft	Max Glide Depth/Mean Riffle Depth ( $d_{maxg}/d_{bkt}$ )				

Channel Materials	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Protrusion Height <sup>d</sup>
	% Silt/Clay	<b>84</b>			$D_{16}$	<b>&lt;.001</b>	mm
	% Sand	<b>16</b>			$D_{35}$	<b>&lt;.001</b>	mm
	% Gravel	<b>0</b>			$D_{50}$	<b>0.0027</b>	mm
	% Cobble	<b>0</b>			$D_{84}$	<b>0.073</b>	mm
	% Boulder	<b>0</b>			$D_{95}$	<b>1.6</b>	mm
	% Bedrock	<b>0</b>			$D_{100}$	<b>4.75</b>	mm

<sup>a</sup> Min, max, mean depths are ave. mid-point values except pools: taken at deepest part of pool.

<sup>b</sup> Composite sample of riffles and pools within the designated reach.

<sup>c</sup> Active bed of a riffle.

<sup>d</sup> Height of roughness feature above bed.

**Worksheet 2-1.** Gage station and field data (Rosgen and Silvey, 2007).

Summary.... <b>USGS GAGE STATION</b> Data/Records for <b>STREAM CHANNEL CLASSIFICATION</b>					
Station NAME:	Wild Rice River-5-38.49			Station Number:	N/A
LOCATION:	Wild Rice River-5-38.49				
Period of RECORD:	N/A	yrs	Mean Annual DISCHARGE:	N/A	cfs
Drainage AREA:	1191680	acres	1862	mi <sup>2</sup>	Drainage Area Mn ELEV: 901.37 ft
Reference REACH SLOPE:		ft/ft	Valley Type:	X	
Stream Type:	E6		HUC:	_ _ _ _ _	
"BANKFULL" CHARACTERISTICS					
Determined from FIELD MEASUREMENT			Determined from GAGE DATA Analysis		
Bankfull WIDTH ( $W_{bkf}$ )	74.1	ft	Bankfull WIDTH ( $W_{bkf}$ )		ft
Bankfull Mean DEPTH ( $d_{bkf}$ )	7.0	ft	Bankfull MEAN DEPTH ( $d_{bkf}$ )		ft
Bankfull Xsec AREA ( $A_{bkf}$ )	516.1	ft <sup>2</sup>	Bankfull Xsec AREA ( $A_{bkf}$ )		ft <sup>2</sup>
Wetted PERIMETER ( $W_p$ )	79.0	ft	Wetted PERIMETER ( $W_p$ )		ft
Bankfull STAGE (Gage Ht)		ft	Bankfull STAGE (Gage Ht)		ft
Est. Mean VELOCITY ( $u$ )	1.0	ft/sec	Mean VELOCITY ( $u$ )		ft/sec
Est. Bkf. DISCHARGE ( $Q_{bkf}$ )	517.0	cfs	Bankfull DISCHARGE ( $Q_{bkf}$ )		cfs
Bankfull DISCHARGE associated with "field-determined" Bankfull STAGE				517.0	cfs
Recurrence Interval ( Log-Pearson ) associated with "field-determined" Bankfull Discharge				1.3	yrs
From the Annual Peak Flow Frequency Analysis data for the Gage Station, determine:					
1.5 Year R.I. Discharge..... =	N/A	cfs	10 Year R.I. Discharge..... =	N/A	cfs
2.0 Year R.I. Discharge.....=	N/A	cfs	25 Year R.I. Discharge.....=	N/A	cfs
5.0 Year R.I. Discharge.....=	N/A	cfs	50 Year R.I. Discharge..... =	N/A	cfs
MEANDER GEOMETRY					
Meander Length ( $L_m$ )	1709	ft	Radius of Curvature ( $R_C$ )	352.0	ft
Belt Width ( $W_{blt}$ )	2019	ft	Meander Width Ratio ( $W_{blt}/W_{bkf}$ )	27.2	ft/ft
HYDRAULIC GEOMETRY					
Based on USGS Discharge Summary Notes data ( Form 9-207 ) and regression analyses of measured discharge ( $Q$ ) with the hydraulic parameters of Width ( $W$ ), Area ( $A$ ), Mean Depth ( $d$ ) & Mean Velocity ( $u$ ), determine the <i>intercept coefficient</i> ( $a$ ) and the <i>slope exponent</i> ( $b$ ) values for a power function of the form $Y = aX^b$ , when $Y$ is one of the selected hydraulic parameters and $X$ is a given discharge value ( $Q$ ).					
	Width ( $W$ )	Depth ( $d$ )	Area ( $A$ )	Velocity ( $u$ )	
Intercept Coefficient: ( $a$ )					
Slope Exponent: ( $b$ )					
Hydraulic Radius: $R = A / W_p$		ft	Manning's "n" at Bankfull Stage	0.043	Coeff.
$"n" = 1.4865 [ ( Area ) ( Hydraulic Radius^{2/3} ) ( Slope^{1/2} ) ] / Q_{bkf}$					

**Worksheet 2-2.** Computations of velocity and bankfull discharge using various methods (Rosgen, 2006b; Rosgen and Silvey, 2007).

Bankfull VELOCITY / DISCHARGE Estimates									
Site	Wild Rice River-5-38.49			Location	Wild Rice River-5-38.49				
Date	10/2/2011	Stream Type	E6	Valley Type	X				
Observers	KD, JB			HUC	-- -- -- -- -- -- -- -- -- --				
INPUT VARIABLES				OUTPUT VARIABLES					
Bankfull Cross-sectional	516.1	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Mean DEPTH	7.0	$D_{bkf}$ (ft)				
Bankfull WIDTH	74.1	$W_{bkf}$ (ft)	Wetted PERIMETER $\sim 2 * d_{bkf} + W_{bkf}$	88.1	$W_p$ (ft)				
$D_{84}$ @ Riffle	0.013	Dia. (mm)	$D_{84}$ mm / 304.8 =	0.00	$D_{84}$ (ft)				
Bankfull SLOPE	0.0001	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	5.9	R (ft)				
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R (ft) / $D_{84}$ (ft)	142927					
Drainage AREA	1862.0	DA (mi <sup>2</sup> )	Shear Velocity $u^* = \sqrt{gRS}$	0.1	$u^*$ (ft / sec)				
ESTIMATION METHODS				Bankfull VELOCITY		Bankfull DISCHARGE			
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 \text{Log}\{ R / D_{84} \} ] u^*$				3.9	ft / sec	2037	cfs		
2. Roughness Coefficient: a) Manning's 'n' from friction factor / relative roughness (Figs. 2-18, 19) $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text"/>				1.0	ft / sec	520	cfs		
2. Roughness Coefficient: $u = 1.4865 * R^{2/3} * S^{1/2} / n$ b) Manning's 'n' from Jarrett ( USGS ): $n = 0.39S^{-.38}R^{-.16}$ n = <input type="text"/>				5.3	ft / sec	2738	cfs		
Note: This equation is for applications involving steep, step-pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for stream types A1, A2, A3, B1, B2, B3, C2 and E3.									
2. Roughness Coefficient: c) Manning's 'n' from Stream Type $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text" value="0.043"/>				1.0	ft / sec	520	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.) HEC-RAS				1.0	ft / sec	517	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.)					ft / sec		cfs		
4. Continuity Equations: a) Regional Curves $u = Q / A$ Return Period for Bankfull Discharge Q = <input type="text" value="1.46"/> Yr.					ft / sec		cfs		
4. Continuity Equations: b) USGS Gage Data $u = Q / A$					ft / sec		cfs		
Options for using the $D_{84}$ term in the relative roughness relation (R/ $D_{84}$ ), when using estimation method 1.									
Option 1. For sand-bed channels: Measure the "protrusion height" ( $h_{sd}$ ) of sand dunes above channel bed elevations. Substitute an average sand dune protrusion height ( $h_{sd}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 2. For boulder-dominated channels: Measure several "protrusion heights" ( $h_{bo}$ ) of boulders above channel bed elevations. Substitute an ave. boulder protrusion height ( $h_{bo}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 3. For bedrock-dominated channels: Measure several "protrusion heights" ( $h_{br}$ ) of rock separations/steps/joints/uplifted surfaces above channel bed elevations. Substitute an average bedrock protrusion height ( $h_{br}$ in feet) for the $D_{84}$ term in estimation method 1.									

**Worksheet 2-3.** Field form for Level II stream classification (Rosgen, 1996; Rosgen, 2006b).

Stream: <b>Wild Rice River-5-38.49</b>	
Basin: <b>Red River Basin</b>	Drainage Area: <b>1E+06</b> acres <b>1862</b> mi <sup>2</sup>
Location: <b>Wild Rice River-5-38.49</b>	
Twp.&Rge: - Sec.&Qtr.: -	
Cross-Section Monuments (Lat./Long.): - Date: <b>10/2/2011</b>	
Observers: <b>KD, JB</b> Valley Type: <b>X</b>	

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>74.1</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>7.0</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>516.1</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>10.6</b>	ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>9.6</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>236.0</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>3.2</b>	ft/ft
<b>Channel Materials (Particle Size Index) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>0.0025</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.000081</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).	<b>1.9</b>	

<div style="border: 1px solid black; padding: 5px; display: inline-block;"> <b>Stream Type</b> </div>	<div style="border: 1px solid black; padding: 5px; display: inline-block; background-color: yellow;"> <b>E6</b> </div>	<div style="border: 1px solid black; padding: 5px; display: inline-block;"> <b>See Classification Key (Figure 2-21)</b> </div>
---	--	--

**Worksheet 2-4.** Morphological relations, including dimensionless ratios of river reach sites (Rosgen, 2006b; Rosgen and Silvey 2007).

Stream: <b>Wild Rice River-5-38.49</b>		Location: <b>Wild Rice River-5-38.49</b>								
Observers: <b>KD, JB</b>		Date: <b>10/2/2011</b>		Valley Type: <b>X</b>		Stream Type: <b>E6</b>				
<b>River Reach Summary Data</b>										
<b>Channel Dimension</b>	Mean Riffle Depth ( $d_{bkt}$ )	<b>7.0</b>	ft	Riffle Width ( $W_{bkt}$ )	<b>74.1</b>	ft	Riffle Area ( $A_{bkt}$ )	<b>516.1</b>	ft <sup>2</sup>	
	Mean Pool Depth ( $d_{bkfp}$ )		ft	Pool Width ( $W_{bkfp}$ )		ft	Pool Area ( $A_{bkfp}$ )		ft <sup>2</sup>	
	Mean Pool Depth/Mean Riffle Depth		$d_{bkfp}/d_{bkt}$	Pool Width/Riffle Width		$W_{bkfp}/W_{bkt}$	Pool Area / Riffle Area		$A_{bkfp}/A_{bkt}$	
	Max Riffle Depth ( $d_{maxrif}$ )	<b>9.6</b>	ft	Max Pool Depth ( $d_{maxp}$ )		ft	Max Riffle Depth/Mean Riffle Depth	<b>1.4</b>		
	Max Pool Depth/Mean Riffle Depth			Point Bar Slope		ft/ft	Inner Berm Width ( $W_{ib}$ )		ft	
	Inner Berm Depth ( $d_{ib}$ )		ft	Inner Berm Width/Depth Ratio			$W_{ib}/d_{ib}$	Inner Berm Area ( $A_{ib}$ )		ft <sup>2</sup>
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )				<b>1.0</b>	ft/s	Estimation Method		<b>HEC-RAS</b>	
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )				<b>517</b>	cfs	Drainage Area		<b>1862</b>	mi <sup>2</sup>

<b>Channel Pattern</b>	Geometry			Dimensionless Geometry Ratios			
	Mean	Min	Max	Mean	Min	Max	
	Meander Wavelength ( $L_m$ )	<b>1709</b>			ft	Meander Length Ratio ( $L_m/W_{bkt}$ )	<b>23.1</b>
	Radius of Curvature ( $R_c$ )	<b>352</b>			ft	Radius of Curvature/Riffle Width ( $R_c/W_{bkt}$ )	<b>4.8</b>
	Belt Width ( $W_{bit}$ )	<b>2019</b>			ft	Meander Width Ratio ( $W_{bit}/W_{bkt}$ )	<b>27.2</b>
	Individual Pool Length				ft	Pool Length/Riffle Width	
	Pool to Pool Spacing				ft	Pool to Pool Spacing/Riffle Width	
Riffle Length				ft	Riffle Length/Riffle Width		

<b>Channel Profile</b>	Valley Slope (VS)		ft/ft	Average Water Surface Slope (S)		ft/ft	Sinuosity (VS/S)		
	Stream Length (SL)	<b>42195</b>	ft	Valley Length (VL)	<b>21767</b>	ft	Sinuosity (SL/VL)	<b>1.9</b>	
	Low Bank Height (LBH)	start	ft	Max Riffle Depth	start	ft	Bank-Height Ratio (BHR)	start	
		end	ft		end	ft	(LBH/Max Riffle Depth)	end	
	Facet Slopes			Dimensionless Slope Ratios			Mean	Min	Max
	Riffle Slope ( $S_{rif}$ )	<b>0.0</b>		ft/ft	Riffle Slope/Average Water Surface Slope ( $S_{rif}/S$ )	<b>1.0</b>			
	Run Slope ( $S_{run}$ )			ft/ft	Run Slope/Average Water Surface Slope ( $S_{run}/S$ )				
	Pool Slope ( $S_p$ )			ft/ft	Pool Slope/Average Water Surface Slope ( $S_p/S$ )				
	Glide Slope ( $S_g$ )			ft/ft	Glide Slope/Average Water Surface Slope ( $S_g/S$ )				
	Feature Midpoint <sup>a</sup>			Dimensionless Depth Ratios			Mean	Min	Max
	Max Riffle Depth ( $d_{maxrif}$ )	<b>9.6</b>		ft	Max Riffle Depth/Mean Riffle Depth ( $d_{maxrif}/d_{bkt}$ )	<b>1.4</b>			
	Max Run Depth ( $d_{maxrun}$ )			ft	Max Run Depth/Mean Riffle Depth ( $d_{maxrun}/d_{bkt}$ )				
	Max Pool Depth ( $d_{maxp}$ )			ft	Max Pool Depth/Mean Riffle Depth ( $d_{maxp}/d_{bkt}$ )				
Max Glide Depth ( $d_{maxg}$ )			ft	Max Glide Depth/Mean Riffle Depth ( $d_{maxg}/d_{bkt}$ )					

<b>Channel Materials</b>	Reach <sup>b</sup>		Riffle <sup>c</sup>	Bar	Reach <sup>b</sup>		Riffle <sup>c</sup>	Bar	Protrusion Height <sup>d</sup>	
	% Silt/Clay	<b>94</b>			$D_{16}$	<b>&lt;.001</b>				mm
	% Sand	<b>6</b>			$D_{35}$	<b>&lt;.001</b>				mm
	% Gravel	<b>0</b>			$D_{50}$	<b>0.0025</b>				mm
	% Cobble	<b>0</b>			$D_{84}$	<b>0.0125</b>				mm
	% Boulder	<b>0</b>			$D_{95}$	<b>0.13</b>				mm
	% Bedrock	<b>0</b>			$D_{100}$	<b>4.75</b>				mm

<sup>a</sup> Min, max, mean depths are ave. mid-point values except pools: taken at deepest part of pool.

<sup>b</sup> Composite sample of riffles and pools within the designated reach.

<sup>c</sup> Active bed of a riffle.

<sup>d</sup> Height of roughness feature above bed.

**Worksheet 2-1.** Gage station and field data (Rosgen and Silvey, 2007).

Summary.... <b>USGS GAGE STATION</b> Data/Records for <b>STREAM CHANNEL CLASSIFICATION</b>					
Station NAME:	Wild Rice River-4-22.94			Station Number:	N/A
LOCATION:	Wild Rice River-4-22.94				
Period of RECORD:	N/A yrs		Mean Annual DISCHARGE:	N/A cfs	
Drainage AREA:	1219200 acres	1905 mi <sup>2</sup>	Drainage Area Mn ELEV:	892.85 ft	
Reference REACH SLOPE:	ft/ft		Valley Type:	X	
Stream Type:	B6c		HUC:	-----	
"BANKFULL" CHARACTERISTICS					
Determined from FIELD MEASUREMENT			Determined from GAGE DATA Analysis		
Bankfull WIDTH ( $W_{bkf}$ )	75.5	ft	Bankfull WIDTH ( $W_{bkf}$ )		ft
Bankfull Mean DEPTH ( $d_{bkf}$ )	5.6	ft	Bankfull MEAN DEPTH ( $d_{bkf}$ )		ft
Bankfull Xsec AREA ( $A_{bkf}$ )	424.6	ft <sup>2</sup>	Bankfull Xsec AREA ( $A_{bkf}$ )		ft <sup>2</sup>
Wetted PERIMETER ( $W_p$ )	78.8	ft	Wetted PERIMETER ( $W_p$ )		ft
Bankfull STAGE (Gage Ht)		ft	Bankfull STAGE (Gage Ht)		ft
Est. Mean VELOCITY ( $u$ )	1.2	ft/sec	Mean VELOCITY ( $u$ )		ft/sec
Est. Bkf. DISCHARGE ( $Q_{bkf}$ )	517.0	cfs	Bankfull DISCHARGE ( $Q_{bkf}$ )		cfs
Bankfull DISCHARGE associated with "field-determined" Bankfull STAGE				517.0	cfs
Recurrence Interval ( Log-Pearson ) associated with "field-determined" Bankfull Discharge				1.3	yrs
From the Annual Peak Flow Frequency Analysis data for the Gage Station, determine:					
1.5 Year R.I. Discharge..... =	N/A	cfs	10 Year R.I. Discharge..... =	N/A	cfs
2.0 Year R.I. Discharge..... =	N/A	cfs	25 Year R.I. Discharge..... =	N/A	cfs
5.0 Year R.I. Discharge..... =	N/A	cfs	50 Year R.I. Discharge..... =	N/A	cfs
MEANDER GEOMETRY					
Meander Length ( $L_m$ )	1514	ft	Radius of Curvature ( $R_C$ )	613.0	ft
Belt Width ( $W_{blt}$ )	2633	ft	Meander Width Ratio ( $W_{blt}/W_{bkf}$ )	34.9	ft/ft
HYDRAULIC GEOMETRY					
Based on USGS Discharge Summary Notes data ( Form 9-207 ) and regression analyses of measured discharge ( $Q$ ) with the hydraulic parameters of Width ( $W$ ), Area ( $A$ ), Mean Depth ( $d$ ) & Mean Velocity ( $u$ ), determine the <i>intercept coefficient</i> ( $a$ ) and the <i>slope exponent</i> ( $b$ ) values for a power function of the form $Y = aX^b$ , when $Y$ is one of the selected hydraulic parameters and $X$ is a given discharge value ( $Q$ ).					
	Width ( $W$ )	Depth ( $d$ )	Area ( $A$ )	Velocity ( $u$ )	
Intercept Coefficient: ( $a$ )					
Slope Exponent: ( $b$ )					
Hydraulic Radius: $R = A / W_p$		ft	Manning's "n" at Bankfull Stage	0.043	Coeff.
$"n" = 1.4865 [ ( Area ) ( Hydraulic Radius^{2/3} ) ( Slope^{1/2} ) ] / Q_{bkf}$					

**Worksheet 2-2.** Computations of velocity and bankfull discharge using various methods (Rosgen, 2006b; Rosgen and Silvey, 2007).

Bankfull VELOCITY / DISCHARGE Estimates									
Site	Wild Rice River-4-22.94			Location	Wild Rice River-4-22.94				
Date	10/3/2011	Stream Type	B6c	Valley Type	X				
Observers	KD, JB			HUC	-- -- -- -- -- -- -- -- -- --				
INPUT VARIABLES				OUTPUT VARIABLES					
Bankfull Cross-sectional	424.6	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Mean DEPTH	5.6	$D_{bkf}$ (ft)				
Bankfull WIDTH	75.5	$W_{bkf}$ (ft)	Wetted PERIMETER $\sim 2 * d_{bkf} + W_{bkf}$	86.7	$W_p$ (ft)				
$D_{84}$ @ Riffle	0.012	Dia. (mm)	$D_{84}$ mm / 304.8 =	0.00	$D_{84}$ (ft)				
Bankfull SLOPE	0.0001	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	4.9	R (ft)				
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R (ft) / $D_{84}$ (ft)	124350					
Drainage AREA	1905.0	DA (mi <sup>2</sup> )	Shear Velocity $u^* = \sqrt{gRS}$	0.1	$u^*$ (ft / sec)				
ESTIMATION METHODS				Bankfull VELOCITY		Bankfull DISCHARGE			
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 \text{Log}\{ R / D_{84} \} ] u^*$				4.6	ft / sec	1963	cfs		
2. Roughness Coefficient: a) Manning's 'n' from friction factor / relative roughness (Figs. 2-18, 19) $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text"/>				1.2	ft / sec	492	cfs		
2. Roughness Coefficient: b) Manning's 'n' from Jarrett ( USGS ): $n = 0.39S^{-.38}R^{-.16}$ n = <input type="text"/>				4.9	ft / sec	2065	cfs		
Note: This equation is for applications involving steep, step-pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for stream types A1, A2, A3, B1, B2, B3, C2 and E3.									
2. Roughness Coefficient: c) Manning's 'n' from Stream Type $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text" value="0.043"/>				1.2	ft / sec	492	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.) HEC-RAS				1.2	ft / sec	517	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.)					ft / sec		cfs		
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge $Q = 1.46$ Yr. $u = Q / A$					ft / sec		cfs		
4. Continuity Equations: b) USGS Gage Data $u = Q / A$					ft / sec		cfs		
Options for using the $D_{84}$ term in the relative roughness relation ( $R/D_{84}$ ), when using estimation method 1.									
Option 1. For sand-bed channels: Measure the "protrusion height" ( $h_{sd}$ ) of sand dunes above channel bed elevations. Substitute an average sand dune protrusion height ( $h_{sd}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 2. For boulder-dominated channels: Measure several "protrusion heights" ( $h_{bo}$ ) of boulders above channel bed elevations. Substitute an ave. boulder protrusion height ( $h_{bo}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 3. For bedrock-dominated channels: Measure several "protrusion heights" ( $h_{br}$ ) of rock separations/steps/joints/uplifted surfaces above channel bed elevations. Substitute an average bedrock protrusion height ( $h_{br}$ in feet) for the $D_{84}$ term in estimation method 1.									

**Worksheet 2-3.** Field form for Level II stream classification (Rosgen, 1996; Rosgen, 2006b).

Stream: <b>Wild Rice River-4-22.94</b>	
Basin: <b>Red River Basin</b>	Drainage Area: <b>1E+06</b> acres <b>1905</b> mi <sup>2</sup>
Location: <b>Wild Rice River-4-22.94</b>	
Twp.&Rge: - Sec.&Qtr.: -	
Cross-Section Monuments (Lat./Long.): - Date: <b>10/3/2011</b>	
Observers: <b>KD, JB</b> Valley Type: <b>X</b>	

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>75.5</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>5.6</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>424.6</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>13.4</b>	ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>8.2</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>144.3</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>1.9</b>	ft/ft
<b>Channel Materials (Particle Size Index) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>0.0032</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.00014</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).	<b>1.8</b>	

<b>Stream Type</b>	<b>B6c</b>	<b>See Classification Key (Figure 2-21)</b>
--------------------	------------	---

**Worksheet 2-4.** Morphological relations, including dimensionless ratios of river reach sites (Rosgen, 2006b; Rosgen and Silvey 2007).

Stream: <b>Wild Rice River-4-22.94</b>		Location: <b>Wild Rice River-4-22.94</b>								
Observers: <b>KD, JB</b>		Date: <b>10/3/2011</b>		Valley Type: <b>X</b>		Stream Type: <b>B6c</b>				
<b>River Reach Summary Data</b>										
<b>Channel Dimension</b>	Mean Riffle Depth ( $d_{bkt}$ )	<b>5.6</b>	ft	Riffle Width ( $W_{bkt}$ )	<b>75.5</b>	ft	Riffle Area ( $A_{bkt}$ )	<b>424.6</b>	ft <sup>2</sup>	
	Mean Pool Depth ( $d_{bkfp}$ )		ft	Pool Width ( $W_{bkfp}$ )		ft	Pool Area ( $A_{bkfp}$ )		ft <sup>2</sup>	
	Mean Pool Depth/Mean Riffle Depth		$d_{bkfp}/d_{bkt}$	Pool Width/Riffle Width		$W_{bkfp}/W_{bkt}$	Pool Area / Riffle Area		$A_{bkfp}/A_{bkt}$	
	Max Riffle Depth ( $d_{maxrif}$ )	<b>8.2</b>	ft	Max Pool Depth ( $d_{maxp}$ )		ft	Max Riffle Depth/Mean Riffle Depth	<b>1.5</b>		
	Max Pool Depth/Mean Riffle Depth			Point Bar Slope		ft/ft	Inner Berm Width ( $W_{ib}$ )		ft	
	Inner Berm Depth ( $d_{ib}$ )		ft	Inner Berm Width/Depth Ratio			$W_{ib}/d_{ib}$	Inner Berm Area ( $A_{ib}$ )		ft <sup>2</sup>
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )				<b>1.2</b>	ft/s	Estimation Method		<b>HEC-RAS</b>	
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )				<b>517</b>	cfs	Drainage Area		<b>1905</b>	mi <sup>2</sup>

<b>Channel Pattern</b>	Geometry			Dimensionless Geometry Ratios			
	Mean	Min	Max	Mean	Min	Max	
	Meander Wavelength ( $L_m$ )	<b>1514</b>			ft	Meander Length Ratio ( $L_m/W_{bkt}$ )	<b>20.1</b>
	Radius of Curvature ( $R_c$ )	<b>613</b>			ft	Radius of Curvature/Riffle Width ( $R_c/W_{bkt}$ )	<b>8.1</b>
	Belt Width ( $W_{bit}$ )	<b>2633</b>			ft	Meander Width Ratio ( $W_{bit}/W_{bkt}$ )	<b>34.9</b>
	Individual Pool Length				ft	Pool Length/Riffle Width	
	Pool to Pool Spacing				ft	Pool to Pool Spacing/Riffle Width	
Riffle Length				ft	Riffle Length/Riffle Width		

<b>Channel Profile</b>	Valley Slope (VS)		ft/ft	Average Water Surface Slope (S)		ft/ft	Sinuosity (VS/S)		
	Stream Length (SL)	<b>63892</b>	ft	Valley Length (VL)	<b>36411</b>	ft	Sinuosity (SL/VL)	<b>1.8</b>	
	Low Bank Height (LBH)	start	ft	Max Riffle Depth	start	ft	Bank-Height Ratio (BHR)	start	
		end	ft		end	ft	(LBH/Max Riffle Depth)	end	
	Facet Slopes			Dimensionless Slope Ratios			Mean	Min	Max
	Riffle Slope ( $S_{rif}$ )	<b>0.0</b>		ft/ft	Riffle Slope/Average Water Surface Slope ( $S_{rif} / S$ )	<b>1.0</b>			
	Run Slope ( $S_{run}$ )			ft/ft	Run Slope/Average Water Surface Slope ( $S_{run} / S$ )				
	Pool Slope ( $S_p$ )			ft/ft	Pool Slope/Average Water Surface Slope ( $S_p / S$ )				
	Glide Slope ( $S_g$ )			ft/ft	Glide Slope/Average Water Surface Slope ( $S_g / S$ )				
	Feature Midpoint <sup>a</sup>			Dimensionless Depth Ratios			Mean	Min	Max
	Max Riffle Depth ( $d_{maxrif}$ )	<b>8.2</b>		ft	Max Riffle Depth/Mean Riffle Depth ( $d_{maxrif} / d_{bkt}$ )	<b>1.5</b>			
	Max Run Depth ( $d_{maxrun}$ )			ft	Max Run Depth/Mean Riffle Depth ( $d_{maxrun} / d_{bkt}$ )				
	Max Pool Depth ( $d_{maxp}$ )			ft	Max Pool Depth/Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )				
	Max Glide Depth ( $d_{maxg}$ )			ft	Max Glide Depth/Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )				

<b>Channel Materials</b>	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Protrusion Height <sup>d</sup>	
	% Silt/Clay	<b>99</b>			$D_{16}$	<b>&lt;.001</b>		mm
	% Sand	<b>1</b>			$D_{35}$	<b>&lt;.001</b>		mm
	% Gravel	<b>0</b>			$D_{50}$	<b>0.0032</b>		mm
	% Cobble	<b>0</b>			$D_{84}$	<b>0.012</b>		mm
	% Boulder	<b>0</b>			$D_{95}$	<b>0.045</b>		mm
	% Bedrock	<b>0</b>			$D_{100}$	<b>0.85</b>		mm

<sup>a</sup> Min, max, mean depths are ave. mid-point values except pools: taken at deepest part of pool.

<sup>b</sup> Composite sample of riffles and pools within the designated reach.

<sup>c</sup> Active bed of a riffle.

<sup>d</sup> Height of roughness feature above bed.

**Worksheet 2-1.** Gage station and field data (Rosgen and Silvey, 2007).

Summary.... <b>USGS GAGE STATION</b> Data/Records for <b>STREAM CHANNEL CLASSIFICATION</b>					
Station NAME:	Wild Rice River-3-17.52			Station Number:	N/A
LOCATION:	Wild Rice River-3-17.52				
Period of RECORD:	N/A	yrs	Mean Annual DISCHARGE:	N/A	cfs
Drainage AREA:	1260800	acres	1970	mi <sup>2</sup>	Drainage Area Mn ELEV: 888.52 ft
Reference REACH SLOPE:		ft/ft	Valley Type:	X	
Stream Type:	E6		HUC:	_ _ _ _ _	
"BANKFULL" CHARACTERISTICS					
Determined from FIELD MEASUREMENT			Determined from GAGE DATA Analysis		
Bankfull WIDTH ( $W_{bkf}$ )	73.8	ft	Bankfull WIDTH ( $W_{bkf}$ )		ft
Bankfull Mean DEPTH ( $d_{bkf}$ )	6.1	ft	Bankfull MEAN DEPTH ( $d_{bkf}$ )		ft
Bankfull Xsec AREA ( $A_{bkf}$ )	450.7	ft <sup>2</sup>	Bankfull Xsec AREA ( $A_{bkf}$ )		ft <sup>2</sup>
Wetted PERIMETER ( $W_p$ )	77.1	ft	Wetted PERIMETER ( $W_p$ )		ft
Bankfull STAGE (Gage Ht)		ft	Bankfull STAGE (Gage Ht)		ft
Est. Mean VELOCITY ( $u$ )	1.2	ft/sec	Mean VELOCITY ( $u$ )		ft/sec
Est. Bkf. DISCHARGE ( $Q_{bkf}$ )	517.0	cfs	Bankfull DISCHARGE ( $Q_{bkf}$ )		cfs
Bankfull DISCHARGE associated with "field-determined" Bankfull STAGE				517.0	cfs
Recurrence Interval ( Log-Pearson ) associated with "field-determined" Bankfull Discharge				1.3	yrs
From the Annual Peak Flow Frequency Analysis data for the Gage Station, determine:					
1.5 Year R.I. Discharge..... =	N/A	cfs	10 Year R.I. Discharge..... =	N/A	cfs
2.0 Year R.I. Discharge.....=	N/A	cfs	25 Year R.I. Discharge.....=	N/A	cfs
5.0 Year R.I. Discharge.....=	N/A	cfs	50 Year R.I. Discharge..... =	N/A	cfs
MEANDER GEOMETRY					
Meander Length ( $L_m$ )	1346	ft	Radius of Curvature ( $R_C$ )	283.0	ft
Belt Width ( $W_{blt}$ )	1344	ft	Meander Width Ratio ( $W_{blt}/W_{bkf}$ )	18.2	ft/ft
HYDRAULIC GEOMETRY					
Based on <i>USGS Discharge Summary Notes</i> data ( Form 9-207 ) and regression analyses of measured discharge ( $Q$ ) with the hydraulic parameters of Width ( $W$ ), Area ( $A$ ), Mean Depth ( $d$ ) & Mean Velocity ( $u$ ), determine the <i>intercept coefficient</i> ( $a$ ) and the <i>slope exponent</i> ( $b$ ) values for a power function of the form $Y = aX^b$ , when $Y$ is one of the selected hydraulic parameters and $X$ is a given discharge value ( $Q$ ).					
	Width ( $W$ )	Depth ( $d$ )	Area ( $A$ )	Velocity ( $u$ )	
Intercept Coefficient: ( $a$ )					
Slope Exponent: ( $b$ )					
Hydraulic Radius: $R = A / W_p$		ft	Manning's "n" at Bankfull Stage	0.03	Coeff.
$"n" = 1.4865 [ ( Area ) ( Hydraulic Radius^{2/3} ) ( Slope^{1/2} ) ] / Q_{bkf}$					

**Worksheet 2-2.** Computations of velocity and bankfull discharge using various methods (Rosgen, 2006b; Rosgen and Silvey, 2007).

Bankfull VELOCITY / DISCHARGE Estimates									
Site	Wild Rice River-3-17.52			Location	Wild Rice River-3-17.52				
Date	10/4/2011	Stream Type	E6	Valley Type	X				
Observers	KD, JB			HUC	-- -- -- -- -- -- -- -- -- --				
INPUT VARIABLES				OUTPUT VARIABLES					
Bankfull Cross-sectional	450.7	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Mean DEPTH	6.1	$D_{bkf}$ (ft)				
Bankfull WIDTH	73.8	$W_{bkf}$ (ft)	Wetted PERIMETER $\sim 2 * d_{bkf} + W_{bkf}$	86.0	$W_p$ (ft)				
$D_{84}$ @ Riffle	0.0046	Dia. (mm)	$D_{84}$ mm / 304.8 =	0.00	$D_{84}$ (ft)				
Bankfull SLOPE	0.0001	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	5.2	R (ft)				
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R (ft) / $D_{84}$ (ft)	347177					
Drainage AREA	1970.0	DA (mi <sup>2</sup> )	Shear Velocity $u^* = \sqrt{gRS}$	0.1	$u^*$ (ft / sec)				
ESTIMATION METHODS				Bankfull VELOCITY		Bankfull DISCHARGE			
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 \text{Log}\{ R / D_{84} \} ] u^*$				3.8	ft / sec	1709	cfs		
2. Roughness Coefficient: a) Manning's 'n' from friction factor / relative roughness (Figs. 2-18, 19) $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text"/>				1.3	ft / sec	575	cfs		
2. Roughness Coefficient: $u = 1.4865 * R^{2/3} * S^{1/2} / n$ b) Manning's 'n' from Jarrett ( USGS ): $n = 0.39S^{-.38}R^{-.16}$ n = <input type="text"/>				4.8	ft / sec	2153	cfs		
Note: This equation is for applications involving steep, step-pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for stream types A1, A2, A3, B1, B2, B3, C2 and E3.									
2. Roughness Coefficient: c) Manning's 'n' from Stream Type $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text" value="0.03"/>				1.3	ft / sec	575	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.) HEC-RAS				1.2	ft / sec	517	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.)					ft / sec		cfs		
4. Continuity Equations: a) Regional Curves $u = Q / A$ Return Period for Bankfull Discharge Q = <input type="text" value="1.46"/> Yr.					ft / sec		cfs		
4. Continuity Equations: b) USGS Gage Data $u = Q / A$					ft / sec		cfs		
Options for using the $D_{84}$ term in the relative roughness relation (R/ $D_{84}$ ), when using estimation method 1.									
Option 1. For sand-bed channels: Measure the "protrusion height" ( $h_{sd}$ ) of sand dunes above channel bed elevations. Substitute an average sand dune protrusion height ( $h_{sd}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 2. For boulder-dominated channels: Measure several "protrusion heights" ( $h_{bo}$ ) of boulders above channel bed elevations. Substitute an ave. boulder protrusion height ( $h_{bo}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 3. For bedrock-dominated channels: Measure several "protrusion heights" ( $h_{br}$ ) of rock separations/steps/joints/ uplifted surfaces above channel bed elevations. Substitute an average bedrock protrusion height ( $h_{br}$ in feet) for the $D_{84}$ term in estimation method 1.									

**Worksheet 2-3.** Field form for Level II stream classification (Rosgen, 1996; Rosgen , 2006b).

Stream: <b>Wild Rice River-3-17.52</b>	
Basin: <b>Red River Basin</b>	Drainage Area: <b>1E+06</b> acres <b>1970</b> mi <sup>2</sup>
Location: <b>Wild Rice River-3-17.52</b>	
Twp.&Rge: - Sec.&Qtr.: -	
Cross-Section Monuments (Lat./Long.): - Date: <b>10/4/2011</b>	
Observers: <b>KD, JB</b> Valley Type: <b>X</b>	

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>73.8</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>6.1</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>450.7</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>12.1</b>	ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>8.7</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>150.7</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>2.0</b>	ft/ft
<b>Channel Materials (Particle Size Index ) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>0.001</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.000073</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).	<b>1.5</b>	

<div style="border: 1px solid black; padding: 5px; display: inline-block;"> <b>Stream Type</b> </div>	<div style="border: 1px solid black; padding: 5px; display: inline-block; background-color: yellow;"> <b>E6</b> </div>	<div style="border: 1px solid black; padding: 5px; display: inline-block;"> <b>See Classification Key (Figure 2-21)</b> </div>
---	--	--

**Worksheet 2-4.** Morphological relations, including dimensionless ratios of river reach sites (Rosgen, 2006b; Rosgen and Silvey 2007).

Stream: <b>Wild Rice River-3-17.52</b>		Location: <b>Wild Rice River-3-17.52</b>								
Observers: <b>KD, JB</b>		Date: <b>10/4/2011</b>		Valley Type: <b>X</b>		Stream Type: <b>E6</b>				
<b>River Reach Summary Data</b>										
<b>Channel Dimension</b>	Mean Riffle Depth ( $d_{bkt}$ )	<b>6.1</b>	ft	Riffle Width ( $W_{bkt}$ )	<b>73.8</b>	ft	Riffle Area ( $A_{bkt}$ )	<b>450.7</b>	ft <sup>2</sup>	
	Mean Pool Depth ( $d_{bkfp}$ )		ft	Pool Width ( $W_{bkfp}$ )		ft	Pool Area ( $A_{bkfp}$ )		ft <sup>2</sup>	
	Mean Pool Depth/Mean Riffle Depth		$d_{bkfp}/d_{bkt}$	Pool Width/Riffle Width		$W_{bkfp}/W_{bkt}$	Pool Area / Riffle Area		$A_{bkfp}/A_{bkt}$	
	Max Riffle Depth ( $d_{maxrif}$ )	<b>8.7</b>	ft	Max Pool Depth ( $d_{maxp}$ )		ft	Max Riffle Depth/Mean Riffle Depth	<b>1.4</b>		
	Max Pool Depth/Mean Riffle Depth			Point Bar Slope		ft/ft	Inner Berm Width ( $W_{ib}$ )		ft	
	Inner Berm Depth ( $d_{ib}$ )		ft	Inner Berm Width/Depth Ratio			$W_{ib}/d_{ib}$	Inner Berm Area ( $A_{ib}$ )		ft <sup>2</sup>
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )				<b>1.2</b>	ft/s	Estimation Method		<b>HEC-RAS</b>	
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )				<b>517</b>	cfs	Drainage Area		<b>1970</b>	mi <sup>2</sup>

<b>Channel Pattern</b>	Geometry			Dimensionless Geometry Ratios			
	Mean	Min	Max	Mean	Min	Max	
	Meander Wavelength ( $L_m$ )	<b>1346</b>			ft	Meander Length Ratio ( $L_m/W_{bkt}$ )	<b>18.2</b>
	Radius of Curvature ( $R_c$ )	<b>283</b>			ft	Radius of Curvature/Riffle Width ( $R_c/W_{bkt}$ )	<b>3.8</b>
	Belt Width ( $W_{bit}$ )	<b>1344</b>			ft	Meander Width Ratio ( $W_{bit}/W_{bkt}$ )	<b>18.2</b>
	Individual Pool Length				ft	Pool Length/Riffle Width	
	Pool to Pool Spacing				ft	Pool to Pool Spacing/Riffle Width	
Riffle Length				ft	Riffle Length/Riffle Width		

<b>Channel Profile</b>	Valley Slope (VS)		ft/ft	Average Water Surface Slope (S)		ft/ft	Sinuosity (VS/S)		
	Stream Length (SL)	<b>32534</b>	ft	Valley Length (VL)	<b>21177</b>	ft	Sinuosity (SL/VL)	<b>1.5</b>	
	Low Bank Height (LBH)	start	ft	Max Riffle Depth	start	ft	Bank-Height Ratio (BHR) (LBH/Max Riffle Depth)	start	
		end	ft		end	ft		end	
	Facet Slopes			Dimensionless Slope Ratios			Mean Min Max		
	Riffle Slope ( $S_{rif}$ )	<b>0.0</b>		ft/ft	Riffle Slope/Average Water Surface Slope ( $S_{rif} / S$ )	<b>1.0</b>			
	Run Slope ( $S_{run}$ )			ft/ft	Run Slope/Average Water Surface Slope ( $S_{run} / S$ )				
	Pool Slope ( $S_p$ )			ft/ft	Pool Slope/Average Water Surface Slope ( $S_p / S$ )				
	Glide Slope ( $S_g$ )			ft/ft	Glide Slope/Average Water Surface Slope ( $S_g / S$ )				
	Feature Midpoint <sup>a</sup>			Dimensionless Depth Ratios			Mean Min Max		
	Max Riffle Depth ( $d_{maxrif}$ )	<b>8.7</b>		ft	Max Riffle Depth/Mean Riffle Depth ( $d_{maxrif} / d_{bkt}$ )	<b>1.4</b>			
	Max Run Depth ( $d_{maxrun}$ )			ft	Max Run Depth/Mean Riffle Depth ( $d_{maxrun} / d_{bkt}$ )				
	Max Pool Depth ( $d_{maxp}$ )			ft	Max Pool Depth/Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )				
Max Glide Depth ( $d_{maxg}$ )			ft	Max Glide Depth/Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )					

<b>Channel Materials</b>	Reach <sup>b</sup>			Riffle <sup>c</sup>			Bar			Protrusion Height <sup>d</sup>		
	% Silt/Clay	<b>95</b>			$D_{16}$	<b>&lt;.001</b>						mm
	% Sand	<b>5</b>			$D_{35}$	<b>&lt;.001</b>					mm	
	% Gravel	<b>0</b>			$D_{50}$	<b>0.001</b>					mm	
	% Cobble	<b>0</b>			$D_{84}$	<b>0.0046</b>					mm	
	% Boulder	<b>0</b>			$D_{95}$	<b>0.071</b>					mm	
	% Bedrock	<b>0</b>			$D_{100}$	<b>4.75</b>					mm	

<sup>a</sup> Min, max, mean depths are ave. mid-point values except pools: taken at deepest part of pool.

<sup>b</sup> Composite sample of riffles and pools within the designated reach.

<sup>c</sup> Active bed of a riffle.

<sup>d</sup> Height of roughness feature above bed.

**Worksheet 2-1.** Gage station and field data (Rosgen and Silvey, 2007).

Summary.... <b>USGS GAGE STATION</b> Data/Records for <b>STREAM CHANNEL CLASSIFICATION</b>					
Station NAME:	Wild Rice River-2-4.23			Station Number:	N/A
LOCATION:	Wild Rice River-2-4.23				
Period of RECORD:	N/A	yrs	Mean Annual DISCHARGE:	N/A	cfs
Drainage AREA:	1287040	acres	2011	mi <sup>2</sup>	Drainage Area Mn ELEV: 880.59 ft
Reference REACH SLOPE:		ft/ft	Valley Type:	X	
Stream Type:	E6		HUC:	-- -- -- -- -- -- -- -- -- -- -- -- -- -- -- --	
"BANKFULL" CHARACTERISTICS					
Determined from FIELD MEASUREMENT			Determined from GAGE DATA Analysis		
Bankfull WIDTH ( $W_{bkf}$ )	84.3	ft	Bankfull WIDTH ( $W_{bkf}$ )		ft
Bankfull Mean DEPTH ( $d_{bkf}$ )	6.2	ft	Bankfull MEAN DEPTH ( $d_{bkf}$ )		ft
Bankfull Xsec AREA ( $A_{bkf}$ )	525.3	ft <sup>2</sup>	Bankfull Xsec AREA ( $A_{bkf}$ )		ft <sup>2</sup>
Wetted PERIMETER ( $W_p$ )	87.5	ft	Wetted PERIMETER ( $W_p$ )		ft
Bankfull STAGE (Gage Ht)		ft	Bankfull STAGE (Gage Ht)		ft
Est. Mean VELOCITY ( $u$ )	1.1	ft/sec	Mean VELOCITY ( $u$ )		ft/sec
Est. Bkf. DISCHARGE ( $Q_{bkf}$ )	600.0	cfs	Bankfull DISCHARGE ( $Q_{bkf}$ )		cfs
Bankfull DISCHARGE associated with "field-determined" Bankfull STAGE				600.0	cfs
Recurrence Interval ( Log-Pearson ) associated with "field-determined" Bankfull Discharge				1.3	yrs
From the Annual Peak Flow Frequency Analysis data for the Gage Station, determine:					
1.5 Year R.I. Discharge..... =	N/A	cfs	10 Year R.I. Discharge..... =	N/A	cfs
2.0 Year R.I. Discharge.....=	N/A	cfs	25 Year R.I. Discharge.....=	N/A	cfs
5.0 Year R.I. Discharge.....=	N/A	cfs	50 Year R.I. Discharge..... =	N/A	cfs
MEANDER GEOMETRY					
Meander Length ( $L_m$ )	745	ft	Radius of Curvature ( $R_C$ )	153.0	ft
Belt Width ( $W_{blt}$ )	1608	ft	Meander Width Ratio ( $W_{blt}/W_{bkf}$ )	19.1	ft/ft
HYDRAULIC GEOMETRY					
Based on <i>USGS Discharge Summary Notes</i> data ( Form 9-207 ) and regression analyses of measured discharge ( $Q$ ) with the hydraulic parameters of Width ( $W$ ), Area ( $A$ ), Mean Depth ( $d$ ) & Mean Velocity ( $u$ ), determine the <i>intercept coefficient</i> ( $a$ ) and the <i>slope exponent</i> ( $b$ ) values for a power function of the form $Y = aX^b$ , when $Y$ is one of the selected hydraulic parameters and $X$ is a given discharge value ( $Q$ ).					
	Width ( $W$ )	Depth ( $d$ )	Area ( $A$ )	Velocity ( $u$ )	
Intercept Coefficient: ( $a$ )					
Slope Exponent: ( $b$ )					
Hydraulic Radius: $R = A / W_p$		ft	Manning's "n" at Bankfull Stage	0.045	Coeff.
$"n" = 1.4865 [ ( Area ) ( Hydraulic Radius^{2/3} ) ( Slope^{1/2} ) ] / Q_{bkf}$					

**Worksheet 2-2.** Computations of velocity and bankfull discharge using various methods (Rosgen, 2006b; Rosgen and Silvey, 2007).

Bankfull VELOCITY / DISCHARGE Estimates									
Site	Wild Rice River-2-4.23			Location	Wild Rice River-2-4.23				
Date	10/4/2011	Stream Type	E6	Valley Type	X				
Observers	KP, AL			HUC	-- -- -- -- -- -- -- -- -- --				
INPUT VARIABLES				OUTPUT VARIABLES					
Bankfull Cross-sectional	525.3	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Mean DEPTH	6.2	$D_{bkf}$ (ft)				
Bankfull WIDTH	84.3	$W_{bkf}$ (ft)	Wetted PERIMETER $\sim 2 * d_{bkf} + W_{bkf}$	96.8	$W_p$ (ft)				
$D_{84}$ @ Riffle	0.05	Dia. (mm)	$D_{84}$ mm / 304.8 =	0.00	$D_{84}$ (ft)				
Bankfull SLOPE	0.0001	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	5.4	R (ft)				
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R (ft) / $D_{84}$ (ft)	33090					
Drainage AREA	2011.0	DA (mi <sup>2</sup> )	Shear Velocity $u^* = \sqrt{gRS}$	0.1	$u^*$ (ft / sec)				
ESTIMATION METHODS				Bankfull VELOCITY		Bankfull DISCHARGE			
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 \text{Log}\{ R / D_{84} \} ] u^*$				3.5	ft / sec	1853	cfs		
2. Roughness Coefficient: a) Manning's 'n' from friction factor / relative roughness (Figs. 2-18, 19) $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text"/>				1.0	ft / sec	503	cfs		
2. Roughness Coefficient: $u = 1.4865 * R^{2/3} * S^{1/2} / n$ b) Manning's 'n' from Jarrett ( USGS ): $n = 0.39S^{-.38}R^{-.16}$ n = <input type="text"/>				5.0	ft / sec	2644	cfs		
Note: This equation is for applications involving steep, step-pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for stream types A1, A2, A3, B1, B2, B3, C2 and E3.									
2. Roughness Coefficient: c) Manning's 'n' from Stream Type $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text" value="0.045"/>				1.0	ft / sec	503	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.) HEC-RAS				1.1	ft / sec	600	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.)					ft / sec		cfs		
4. Continuity Equations: a) Regional Curves $u = Q / A$ Return Period for Bankfull Discharge Q = <input type="text" value="1.46"/> Yr.					ft / sec		cfs		
4. Continuity Equations: b) USGS Gage Data $u = Q / A$					ft / sec		cfs		
Options for using the $D_{84}$ term in the relative roughness relation ( $R/D_{84}$ ), when using estimation method 1.									
Option 1. For sand-bed channels: Measure the "protrusion height" ( $h_{sd}$ ) of sand dunes above channel bed elevations. Substitute an average sand dune protrusion height ( $h_{sd}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 2. For boulder-dominated channels: Measure several "protrusion heights" ( $h_{bo}$ ) of boulders above channel bed elevations. Substitute an ave. boulder protrusion height ( $h_{bo}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 3. For bedrock-dominated channels: Measure several "protrusion heights" ( $h_{br}$ ) of rock separations/steps/joints/uplifted surfaces above channel bed elevations. Substitute an average bedrock protrusion height ( $h_{br}$ in feet) for the $D_{84}$ term in estimation method 1.									

**Worksheet 2-3.** Field form for Level II stream classification (Rosgen, 1996; Rosgen , 2006b).

Stream: <b>Wild Rice River-2-4.23</b>	
Basin: <b>Red River Basin</b>	Drainage Area: <b>1E+06</b> acres <b>2011</b> mi <sup>2</sup>
Location: <b>Wild Rice River-2-4.23</b>	
Twp.&Rge: - Sec.&Qtr.: -	
Cross-Section Monuments (Lat./Long.): - Date: <b>10/4/2011</b>	
Observers: <b>KP, AL</b> Valley Type: <b>X</b>	

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>84.3</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>6.2</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>525.3</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>13.5</b>	ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>8.5</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>283.7</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>3.4</b>	ft/ft
<b>Channel Materials (Particle Size Index ) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>0.0029</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.000088</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).	<b>2.3</b>	

<b>Stream Type</b>	<b>E6</b>	<b>See Classification Key (Figure 2-21)</b>
--------------------	-----------	---

**Worksheet 2-4.** Morphological relations, including dimensionless ratios of river reach sites (Rosgen, 2006b; Rosgen and Silvey 2007).

Stream: <b>Wild Rice River-2-4.23</b>		Location: <b>Wild Rice River-2-4.23</b>								
Observers: <b>KP, AL</b>		Date: <b>10/4/2011</b>		Valley Type: <b>X</b>		Stream Type: <b>E6</b>				
<b>River Reach Summary Data</b>										
<b>Channel Dimension</b>	Mean Riffle Depth ( $d_{bkt}$ )	<b>6.2</b>	ft	Riffle Width ( $W_{bkt}$ )	<b>84.3</b>	ft	Riffle Area ( $A_{bkt}$ )	<b>525.3</b>	ft <sup>2</sup>	
	Mean Pool Depth ( $d_{bkfp}$ )		ft	Pool Width ( $W_{bkfp}$ )		ft	Pool Area ( $A_{bkfp}$ )		ft <sup>2</sup>	
	Mean Pool Depth/Mean Riffle Depth		$d_{bkfp}/d_{bkt}$	Pool Width/Riffle Width		$W_{bkfp}/W_{bkt}$	Pool Area / Riffle Area		$A_{bkfp}/A_{bkt}$	
	Max Riffle Depth ( $d_{maxrif}$ )	<b>8.5</b>	ft	Max Pool Depth ( $d_{maxp}$ )		ft	Max Riffle Depth/Mean Riffle Depth	<b>1.4</b>		
	Max Pool Depth/Mean Riffle Depth			Point Bar Slope		ft/ft	Inner Berm Width ( $W_{ib}$ )		ft	
	Inner Berm Depth ( $d_{ib}$ )		ft	Inner Berm Width/Depth Ratio			$W_{ib}/d_{ib}$	Inner Berm Area ( $A_{ib}$ )		ft <sup>2</sup>
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )				<b>1.1</b>	ft/s	Estimation Method		<b>HEC-RAS</b>	
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )				<b>600</b>	cfs	Drainage Area		<b>2011</b>	mi <sup>2</sup>

<b>Channel Pattern</b>	Geometry			Dimensionless Geometry Ratios			
	Mean	Min	Max	Mean	Min	Max	
	Meander Wavelength ( $L_m$ )	<b>745</b>			ft	Meander Length Ratio ( $L_m/W_{bkt}$ )	<b>8.8</b>
	Radius of Curvature ( $R_c$ )	<b>153</b>			ft	Radius of Curvature/Riffle Width ( $R_c/W_{bkt}$ )	<b>1.8</b>
	Belt Width ( $W_{bit}$ )	<b>1608</b>			ft	Meander Width Ratio ( $W_{bit}/W_{bkt}$ )	<b>19.1</b>
	Individual Pool Length				ft	Pool Length/Riffle Width	
	Pool to Pool Spacing				ft	Pool to Pool Spacing/Riffle Width	
Riffle Length				ft	Riffle Length/Riffle Width		

<b>Channel Profile</b>	Valley Slope (VS)		ft/ft	Average Water Surface Slope (S)		ft/ft	Sinuosity (VS/S)		
	Stream Length (SL)	<b>55572</b>	ft	Valley Length (VL)	<b>24623</b>	ft	Sinuosity (SL/VL)	<b>2.3</b>	
	Low Bank Height (LBH)	start	ft	Max Riffle Depth	start	ft	Bank-Height Ratio (BHR)	start	
		end	ft		end	ft	(LBH/Max Riffle Depth)	end	
	Facet Slopes			Dimensionless Slope Ratios			Mean	Min	Max
	Riffle Slope ( $S_{rif}$ )	<b>0.0</b>		ft/ft	Riffle Slope/Average Water Surface Slope ( $S_{rif} / S$ )	<b>1.0</b>			
	Run Slope ( $S_{run}$ )			ft/ft	Run Slope/Average Water Surface Slope ( $S_{run} / S$ )				
	Pool Slope ( $S_p$ )			ft/ft	Pool Slope/Average Water Surface Slope ( $S_p / S$ )				
	Glide Slope ( $S_g$ )			ft/ft	Glide Slope/Average Water Surface Slope ( $S_g / S$ )				
	Feature Midpoint <sup>a</sup>			Dimensionless Depth Ratios			Mean	Min	Max
	Max Riffle Depth ( $d_{maxrif}$ )	<b>8.5</b>		ft	Max Riffle Depth/Mean Riffle Depth ( $d_{maxrif} / d_{bkt}$ )	<b>1.4</b>			
	Max Run Depth ( $d_{maxrun}$ )			ft	Max Run Depth/Mean Riffle Depth ( $d_{maxrun} / d_{bkt}$ )				
	Max Pool Depth ( $d_{maxp}$ )			ft	Max Pool Depth/Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )				
Max Glide Depth ( $d_{maxg}$ )			ft	Max Glide Depth/Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )					

<b>Channel Materials</b>	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Protrusion Height <sup>d</sup>	
	% Silt/Clay	<b>89</b>			$D_{16}$	<b>&lt;.001</b>		mm
	% Sand	<b>11</b>			$D_{35}$	<b>&lt;.001</b>		mm
	% Gravel	<b>0</b>			$D_{50}$	<b>0.0029</b>		mm
	% Cobble	<b>0</b>			$D_{84}$	<b>0.05</b>		mm
	% Boulder	<b>0</b>			$D_{95}$	<b>0.3</b>		mm
	% Bedrock	<b>0</b>			$D_{100}$	<b>4.75</b>		mm

<sup>a</sup> Min, max, mean depths are ave. mid-point values except pools: taken at deepest part of pool.

<sup>b</sup> Composite sample of riffles and pools within the designated reach.

<sup>c</sup> Active bed of a riffle.

<sup>d</sup> Height of roughness feature above bed.

**Worksheet 2-1.** Gage station and field data (Rosgen and Silvey, 2007).

Summary.... <b>USGS GAGE STATION</b> Data/Records for <b>STREAM CHANNEL CLASSIFICATION</b>						
Station NAME:	Wild Rice River-1-3.01			Station Number:	N/A	
LOCATION:	Wild Rice River-1-3.01					
Period of RECORD:	N/A yrs		Mean Annual DISCHARGE:	N/A cfs		
Drainage AREA:	1287680 acres	2012 mi <sup>2</sup>	Drainage Area Mn ELEV:	875.87 ft		
Reference REACH SLOPE:	ft/ft		Valley Type:	X		
Stream Type:	E6		HUC:	-- -- -- -- --		
"BANKFULL" CHARACTERISTICS						
Determined from FIELD MEASUREMENT			Determined from GAGE DATA Analysis			
Bankfull WIDTH ( $W_{bkf}$ )	79.2	ft	Bankfull WIDTH ( $W_{bkf}$ )		ft	
Bankfull Mean DEPTH ( $d_{bkf}$ )	7.0	ft	Bankfull MEAN DEPTH ( $d_{bkf}$ )		ft	
Bankfull Xsec AREA ( $A_{bkf}$ )	556.2	ft <sup>2</sup>	Bankfull Xsec AREA ( $A_{bkf}$ )		ft <sup>2</sup>	
Wetted PERIMETER ( $W_p$ )	83.8	ft	Wetted PERIMETER ( $W_p$ )		ft	
Bankfull STAGE (Gage Ht)		ft	Bankfull STAGE (Gage Ht)		ft	
Est. Mean VELOCITY ( $u$ )	1.1	ft/sec	Mean VELOCITY ( $u$ )		ft/sec	
Est. Bkf. DISCHARGE ( $Q_{bkf}$ )	600.0	cfs	Bankfull DISCHARGE ( $Q_{bkf}$ )		cfs	
Bankfull DISCHARGE associated with "field-determined" Bankfull STAGE				600.0	cfs	
Recurrence Interval ( Log-Pearson ) associated with "field-determined" Bankfull Discharge				1.3	yrs	
From the Annual Peak Flow Frequency Analysis data for the Gage Station, determine:						
1.5 Year R.I. Discharge..... =	N/A	cfs	10 Year R.I. Discharge..... =	N/A	cfs	
2.0 Year R.I. Discharge..... =	N/A	cfs	25 Year R.I. Discharge..... =	N/A	cfs	
5.0 Year R.I. Discharge..... =	N/A	cfs	50 Year R.I. Discharge..... =	N/A	cfs	
MEANDER GEOMETRY						
Meander Length ( $L_m$ )	910	ft	Radius of Curvature ( $R_C$ )	137.0	ft	
Belt Width ( $W_{blt}$ )	1940	ft	Meander Width Ratio ( $W_{blt}/W_{bkf}$ )	24.5	ft/ft	
HYDRAULIC GEOMETRY						
Based on USGS Discharge Summary Notes data ( Form 9-207 ) and regression analyses of measured discharge ( $Q$ ) with the hydraulic parameters of Width ( $W$ ), Area ( $A$ ), Mean Depth ( $d$ ) & Mean Velocity ( $u$ ), determine the <i>intercept coefficient</i> ( $a$ ) and the <i>slope exponent</i> ( $b$ ) values for a power function of the form $Y = aX^b$ , when $Y$ is one of the selected hydraulic parameters and $X$ is a given discharge value ( $Q$ ).						
	Width ( $W$ )	Depth ( $d$ )	Area ( $A$ )	Velocity ( $u$ )		
Intercept Coefficient: ( $a$ )						
Slope Exponent: ( $b$ )						
Hydraulic Radius: $R = A / W_p$		ft	Manning's "n" at Bankfull Stage	0.045	Coeff.	
$"n" = 1.4865 [ ( Area ) ( Hydraulic Radius^{2/3} ) ( Slope^{1/2} ) ] / Q_{bkf}$						

**Worksheet 2-2.** Computations of velocity and bankfull discharge using various methods (Rosgen, 2006b; Rosgen and Silvey, 2007).

Bankfull VELOCITY / DISCHARGE Estimates									
Site	Wild Rice River-1-3.01			Location	Wild Rice River-1-3.01				
Date	10/4/2011	Stream Type	E6	Valley Type	X				
Observers	KP, AL			HUC	-- -- -- -- -- -- -- -- -- --				
INPUT VARIABLES				OUTPUT VARIABLES					
Bankfull Cross-sectional	556.2	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Mean DEPTH	7.0	$D_{bkf}$ (ft)				
Bankfull WIDTH	79.2	$W_{bkf}$ (ft)	Wetted PERIMETER $\sim 2 * d_{bkf} + W_{bkf}$	93.2	$W_p$ (ft)				
$D_{84}$ @ Riffle	0.022	Dia. (mm)	$D_{84}$ mm / 304.8 =	0.00	$D_{84}$ (ft)				
Bankfull SLOPE	0.0001	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	6.0	R (ft)				
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R (ft) / $D_{84}$ (ft)	82706					
Drainage AREA	2012.0	DA (mi <sup>2</sup> )	Shear Velocity $u^* = \sqrt{gRS}$	0.1	$u^*$ (ft / sec)				
ESTIMATION METHODS				Bankfull VELOCITY		Bankfull DISCHARGE			
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 \text{Log}\{ R / D_{84} \} ] u^*$				4.3	ft / sec	2400	cfs		
2. Roughness Coefficient: a) Manning's 'n' from friction factor / relative roughness (Figs. 2-18, 19) $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text"/>				1.1	ft / sec	614	cfs		
2. Roughness Coefficient: $u = 1.4865 * R^{2/3} * S^{1/2} / n$ b) Manning's 'n' from Jarrett ( USGS ): $n = 0.39S^{-.38}R^{-.16}$ n = <input type="text"/>				5.5	ft / sec	3085	cfs		
Note: This equation is for applications involving steep, step-pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for stream types A1, A2, A3, B1, B2, B3, C2 and E3.									
2. Roughness Coefficient: c) Manning's 'n' from Stream Type $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text" value="0.045"/>				1.1	ft / sec	614	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.) HEC-RAS				1.1	ft / sec	600	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.)					ft / sec		cfs		
4. Continuity Equations: a) Regional Curves $u = Q / A$ Return Period for Bankfull Discharge Q = <input type="text" value="1.46"/> Yr.					ft / sec		cfs		
4. Continuity Equations: b) USGS Gage Data $u = Q / A$					ft / sec		cfs		
Options for using the $D_{84}$ term in the relative roughness relation (R/ $D_{84}$ ), when using estimation method 1.									
Option 1. For sand-bed channels: Measure the "protrusion height" ( $h_{sd}$ ) of sand dunes above channel bed elevations. Substitute an average sand dune protrusion height ( $h_{sd}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 2. For boulder-dominated channels: Measure several "protrusion heights" ( $h_{bo}$ ) of boulders above channel bed elevations. Substitute an ave. boulder protrusion height ( $h_{bo}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 3. For bedrock-dominated channels: Measure several "protrusion heights" ( $h_{br}$ ) of rock separations/steps/joints/ uplifted surfaces above channel bed elevations. Substitute an average bedrock protrusion height ( $h_{br}$ in feet) for the $D_{84}$ term in estimation method 1.									

**Worksheet 2-3.** Field form for Level II stream classification (Rosgen, 1996; Rosgen , 2006b).

Stream: <b>Wild Rice River-1-3.01</b>	
Basin: <b>Red River Basin</b>	Drainage Area: <b>1E+06</b> acres <b>2012</b> mi <sup>2</sup>
Location: <b>Wild Rice River-1-3.01</b>	
Twp.&Rge: - Sec.&Qtr.: -	
Cross-Section Monuments (Lat./Long.): - Date: <b>10/4/2011</b>	
Observers: <b>KP, AL</b> Valley Type: <b>X</b>	

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>79.2</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>7.0</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>556.2</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>11.3</b>	ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>10.2</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>333.0</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>4.2</b>	ft/ft
<b>Channel Materials (Particle Size Index ) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>0.0031</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.00010</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).	<b>3.9</b>	

<div style="border: 1px solid black; padding: 5px; display: inline-block;"> <b>Stream Type</b> </div>	<div style="border: 1px solid black; padding: 5px; display: inline-block; background-color: yellow;"> <b>E6</b> </div>	<div style="border: 1px solid black; padding: 5px; display: inline-block;"> <b>See Classification Key (Figure 2-21)</b> </div>
---	--	--

**Worksheet 2-4.** Morphological relations, including dimensionless ratios of river reach sites (Rosgen, 2006b; Rosgen and Silvey 2007).

Stream: <b>Wild Rice River-1-3.01</b>		Location: <b>Wild Rice River-1-3.01</b>								
Observers: <b>KP, AL</b>		Date: <b>10/4/2011</b>		Valley Type: <b>X</b>		Stream Type: <b>E6</b>				
<b>River Reach Summary Data</b>										
<b>Channel Dimension</b>	Mean Riffle Depth ( $d_{bkt}$ )	<b>7.0</b>	ft	Riffle Width ( $W_{bkt}$ )	<b>79.2</b>	ft	Riffle Area ( $A_{bkt}$ )	<b>556.2</b>	ft <sup>2</sup>	
	Mean Pool Depth ( $d_{bkfp}$ )		ft	Pool Width ( $W_{bkfp}$ )		ft	Pool Area ( $A_{bkfp}$ )		ft <sup>2</sup>	
	Mean Pool Depth/Mean Riffle Depth		$d_{bkfp}/d_{bkt}$	Pool Width/Riffle Width		$W_{bkfp}/W_{bkt}$	Pool Area / Riffle Area		$A_{bkfp}/A_{bkt}$	
	Max Riffle Depth ( $d_{maxrif}$ )	<b>10.2</b>	ft	Max Pool Depth ( $d_{maxp}$ )		ft	Max Riffle Depth/Mean Riffle Depth	<b>1.5</b>		
	Max Pool Depth/Mean Riffle Depth			Point Bar Slope		ft/ft	Inner Berm Width ( $W_{ib}$ )		ft	
	Inner Berm Depth ( $d_{ib}$ )		ft	Inner Berm Width/Depth Ratio			$W_{ib}/d_{ib}$	Inner Berm Area ( $A_{ib}$ )		ft <sup>2</sup>
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )				<b>1.1</b>	ft/s	Estimation Method		<b>HEC-RAS</b>	
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )				<b>600</b>	cfs	Drainage Area		<b>2012</b>	mi <sup>2</sup>

<b>Channel Pattern</b>	Geometry			Dimensionless Geometry Ratios			
	Mean	Min	Max	Mean	Min	Max	
	Meander Wavelength ( $L_m$ )	<b>910</b>			ft	Meander Length Ratio ( $L_m/W_{bkt}$ )	<b>11.5</b>
	Radius of Curvature ( $R_c$ )	<b>137</b>			ft	Radius of Curvature/Riffle Width ( $R_c/W_{bkt}$ )	<b>1.7</b>
	Belt Width ( $W_{bit}$ )	<b>1940</b>			ft	Meander Width Ratio ( $W_{bit}/W_{bkt}$ )	<b>24.5</b>
	Individual Pool Length				ft	Pool Length/Riffle Width	
	Pool to Pool Spacing				ft	Pool to Pool Spacing/Riffle Width	
Riffle Length				ft	Riffle Length/Riffle Width		

<b>Channel Profile</b>	Valley Slope (VS)		ft/ft	Average Water Surface Slope (S)		ft/ft	Sinuosity (VS/S)		
	Stream Length (SL)	<b>21405</b>	ft	Valley Length (VL)	<b>5483</b>	ft	Sinuosity (SL/VL)	<b>3.9</b>	
	Low Bank Height (LBH)	start	ft	Max Riffle Depth	start	ft	Bank-Height Ratio (BHR)	start	
		end	ft		end	ft	(LBH/Max Riffle Depth)	end	
	Facet Slopes			Dimensionless Slope Ratios			Mean	Min	Max
	Riffle Slope ( $S_{rif}$ )	<b>0.0</b>		ft/ft	Riffle Slope/Average Water Surface Slope ( $S_{rif}/S$ )	<b>1.0</b>			
	Run Slope ( $S_{run}$ )			ft/ft	Run Slope/Average Water Surface Slope ( $S_{run}/S$ )				
	Pool Slope ( $S_p$ )			ft/ft	Pool Slope/Average Water Surface Slope ( $S_p/S$ )				
	Glide Slope ( $S_g$ )			ft/ft	Glide Slope/Average Water Surface Slope ( $S_g/S$ )				
	Feature Midpoint <sup>a</sup>			Dimensionless Depth Ratios			Mean	Min	Max
	Max Riffle Depth ( $d_{maxrif}$ )	<b>10.2</b>		ft	Max Riffle Depth/Mean Riffle Depth ( $d_{maxrif}/d_{bkt}$ )	<b>1.5</b>			
	Max Run Depth ( $d_{maxrun}$ )			ft	Max Run Depth/Mean Riffle Depth ( $d_{maxrun}/d_{bkt}$ )				
	Max Pool Depth ( $d_{maxp}$ )			ft	Max Pool Depth/Mean Riffle Depth ( $d_{maxp}/d_{bkt}$ )				
	Max Glide Depth ( $d_{maxg}$ )			ft	Max Glide Depth/Mean Riffle Depth ( $d_{maxg}/d_{bkt}$ )				

<b>Channel Materials</b>	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Protrusion Height <sup>d</sup>	
	% Silt/Clay	<b>95</b>			$D_{16}$	<b>&lt;.001</b>		mm
	% Sand	<b>5</b>			$D_{35}$	<b>&lt;.001</b>		mm
	% Gravel	<b>0</b>			$D_{50}$	<b>0.0031</b>		mm
	% Cobble	<b>0</b>			$D_{84}$	<b>0.022</b>		mm
	% Boulder	<b>0</b>			$D_{95}$	<b>0.075</b>		mm
	% Bedrock	<b>0</b>			$D_{100}$	<b>4.75</b>		mm

<sup>a</sup> Min, max, mean depths are ave. mid-point values except pools: taken at deepest part of pool.

<sup>b</sup> Composite sample of riffles and pools within the designated reach.

<sup>c</sup> Active bed of a riffle.

<sup>d</sup> Height of roughness feature above bed.

**Worksheet 2-1.** Gage station and field data (Rosgen and Silvey, 2007).

Summary.... <b>USGS GAGE STATION</b> Data/Records for <b>STREAM CHANNEL CLASSIFICATION</b>					
Station NAME:	Sheyenne River-8-55.75			Station Number:	N/A
LOCATION:	Sheyenne River-8-55.75				
Period of RECORD:	N/A	yrs	Mean Annual DISCHARGE:	N/A	cfs
Drainage AREA:	2179840	acres	3406	mi <sup>2</sup>	Drainage Area Mn ELEV: 911.79 ft
Reference REACH SLOPE:		ft/ft	Valley Type:	X	
Stream Type:	E5		HUC:	_ _ _ _ _	
"BANKFULL" CHARACTERISTICS					
Determined from FIELD MEASUREMENT			Determined from GAGE DATA Analysis		
Bankfull WIDTH ( $W_{bkf}$ )	74.7	ft	Bankfull WIDTH ( $W_{bkf}$ )		ft
Bankfull Mean DEPTH ( $d_{bkf}$ )	8.3	ft	Bankfull MEAN DEPTH ( $d_{bkf}$ )		ft
Bankfull Xsec AREA ( $A_{bkf}$ )	616.4	ft <sup>2</sup>	Bankfull Xsec AREA ( $A_{bkf}$ )		ft <sup>2</sup>
Wetted PERIMETER ( $W_p$ )	80.5	ft	Wetted PERIMETER ( $W_p$ )		ft
Bankfull STAGE (Gage Ht)		ft	Bankfull STAGE (Gage Ht)		ft
Est. Mean VELOCITY ( $u$ )	1.6	ft/sec	Mean VELOCITY ( $u$ )		ft/sec
Est. Bkf. DISCHARGE ( $Q_{bkf}$ )	1000.0	cfs	Bankfull DISCHARGE ( $Q_{bkf}$ )		cfs
Bankfull DISCHARGE associated with "field-determined" Bankfull STAGE				1000.0	cfs
Recurrence Interval ( Log-Pearson ) associated with "field-determined" Bankfull Discharge				1.5	yrs
From the Annual Peak Flow Frequency Analysis data for the Gage Station, determine:					
1.5 Year R.I. Discharge..... =	N/A	cfs	10 Year R.I. Discharge..... =	N/A	cfs
2.0 Year R.I. Discharge.....=	N/A	cfs	25 Year R.I. Discharge.....=	N/A	cfs
5.0 Year R.I. Discharge.....=	N/A	cfs	50 Year R.I. Discharge..... =	N/A	cfs
MEANDER GEOMETRY					
Meander Length ( $L_m$ )	1265	ft	Radius of Curvature ( $R_C$ )	210.0	ft
Belt Width ( $W_{blt}$ )	2807	ft	Meander Width Ratio ( $W_{blt}/W_{bkf}$ )	37.6	ft/ft
HYDRAULIC GEOMETRY					
Based on USGS Discharge Summary Notes data ( Form 9-207 ) and regression analyses of measured discharge ( $Q$ ) with the hydraulic parameters of Width ( $W$ ), Area ( $A$ ), Mean Depth ( $d$ ) & Mean Velocity ( $u$ ), determine the <i>intercept coefficient</i> ( $a$ ) and the <i>slope exponent</i> ( $b$ ) values for a power function of the form $Y = aX^b$ , when $Y$ is one of the selected hydraulic parameters and $X$ is a given discharge value ( $Q$ ).					
	Width ( $W$ )	Depth ( $d$ )	Area ( $A$ )	Velocity ( $u$ )	
Intercept Coefficient: ( $a$ )					
Slope Exponent: ( $b$ )					
Hydraulic Radius: $R = A / W_p$		ft	Manning's "n" at Bankfull Stage	0.052	Coeff.
$"n" = 1.4865 [ ( Area ) ( Hydraulic Radius^{2/3} ) ( Slope^{1/2} ) ] / Q_{bkf}$					

**Worksheet 2-2.** Computations of velocity and bankfull discharge using various methods (Rosgen, 2006b; Rosgen and Silvey, 2007).

Bankfull VELOCITY / DISCHARGE Estimates										
Site	Sheyenne River-8-55.75				Location	Sheyenne River-8-55.75				
Date	10/2/2011	Stream Type	E5	Valley Type	X					
Observers	KP, AL				HUC	-- -- -- -- -- -- -- -- -- --				
INPUT VARIABLES				OUTPUT VARIABLES						
Bankfull Cross-sectional	616.4	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Mean DEPTH	8.3	$D_{bkf}$ (ft)					
Bankfull WIDTH	74.7	$W_{bkf}$ (ft)	Wetted PERIMETER $\sim 2 * d_{bkf} + W_{bkf}$	91.2	$W_p$ (ft)					
$D_{84}$ @ Riffle	0.24	Dia. (mm)	$D_{84}$ mm / 304.8 =	0.00	$D_{84}$ (ft)					
Bankfull SLOPE	0.0001	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	6.8	R (ft)					
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R (ft) / $D_{84}$ (ft)	8765						
Drainage AREA	3406.0	DA (mi <sup>2</sup> )	Shear Velocity $u^* = \sqrt{gRS}$	0.2	$u^*$ (ft / sec)					
ESTIMATION METHODS				Bankfull VELOCITY		Bankfull DISCHARGE				
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 \text{Log}\{ R / D_{84} \} ] u^*$				3.8	ft / sec	2334	cfs			
2. Roughness Coefficient: a) Manning's 'n' from friction factor / relative roughness (Figs. 2-18, 19) $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text"/>				1.0	ft / sec	643	cfs			
2. Roughness Coefficient: b) Manning's 'n' from Jarrett ( USGS ): $n = 0.39S^{-.38}R^{-.16}$ n = <input type="text"/> Note: This equation is for applications involving steep, step-pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for stream types A1, A2, A3, B1, B2, B3, C2 and E3.				6.2	ft / sec	3794	cfs			
2. Roughness Coefficient: c) Manning's 'n' from Stream Type $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text" value="0.052"/>				1.0	ft / sec	643	cfs			
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.) HEC-RAS				1.6	ft / sec	1000	cfs			
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.)					ft / sec		cfs			
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge $Q = 1.46$ Yr. $u = Q / A$					ft / sec		cfs			
4. Continuity Equations: b) USGS Gage Data $u = Q / A$					ft / sec		cfs			
Options for using the $D_{84}$ term in the relative roughness relation ( $R/D_{84}$ ), when using estimation method 1.										
Option 1. For sand-bed channels: Measure the "protrusion height" ( $h_{sd}$ ) of sand dunes above channel bed elevations. Substitute an average sand dune protrusion height ( $h_{sd}$ in ft) for the $D_{84}$ term in est. method 1.										
Option 2. For boulder-dominated channels: Measure several "protrusion heights" ( $h_{bo}$ ) of boulders above channel bed elevations. Substitute an ave. boulder protrusion height ( $h_{bo}$ in ft) for the $D_{84}$ term in est. method 1.										
Option 3. For bedrock-dominated channels: Measure several "protrusion heights" ( $h_{br}$ ) of rock separations/steps/joints/uplifted surfaces above channel bed elevations. Substitute an average bedrock protrusion height ( $h_{br}$ in feet) for the $D_{84}$ term in estimation method 1.										

**Worksheet 2-3.** Field form for Level II stream classification (Rosgen, 1996; Rosgen , 2006b).

Stream: <b>Sheyenne River-8-55.75</b>	
Basin: <b>Red River Basin</b>	Drainage Area: <b>2E+06</b> acres <b>3406</b> mi <sup>2</sup>
Location: <b>Sheyenne River-8-55.75</b>	
Twp.&Rge: - Sec.&Qtr.: -	
Cross-Section Monuments (Lat./Long.): - Date: <b>40818</b>	
Observers: <b>KP, AL</b> Valley Type: <b>X</b>	

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>74.7</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>8.3</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>616.4</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>9.0</b>	ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>13.1</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>898.5</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>12.0</b>	ft/ft
<b>Channel Materials (Particle Size Index ) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>0.18</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.00010</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).	<b>4.0</b>	

<b>Stream Type</b>	<b>E5</b>	<b>See Classification Key (Figure 2-21)</b>
--------------------	-----------	---

**Worksheet 2-4.** Morphological relations, including dimensionless ratios of river reach sites (Rosgen, 2006b; Rosgen and Silvey 2007).

Stream: <b>Sheyenne River-8-55.75</b>		Location: <b>Sheyenne River-8-55.75</b>								
Observers: <b>KP, AL</b>		Date: <b>40818</b>		Valley Type: <b>X</b>		Stream Type: <b>E5</b>				
<b>River Reach Summary Data</b>										
<b>Channel Dimension</b>	Mean Riffle Depth ( $d_{bkt}$ )	<b>8.26</b>	ft	Riffle Width ( $W_{bkt}$ )	<b>74.7</b>	ft	Riffle Area ( $A_{bkt}$ )	<b>616.40</b>	ft <sup>2</sup>	
	Mean Pool Depth ( $d_{bkfp}$ )		ft	Pool Width ( $W_{bkfp}$ )		ft	Pool Area ( $A_{bkfp}$ )		ft <sup>2</sup>	
	Mean Pool Depth/Mean Riffle Depth		$d_{bkfp}/d_{bkt}$	Pool Width/Riffle Width		$W_{bkfp}/W_{bkt}$	Pool Area / Riffle Area		$A_{bkfp}/A_{bkt}$	
	Max Riffle Depth ( $d_{maxrif}$ )	<b>13.1</b>	ft	Max Pool Depth ( $d_{maxp}$ )		ft	Max Riffle Depth/Mean Riffle Depth	<b>1.584</b>		
	Max Pool Depth/Mean Riffle Depth			Point Bar Slope		ft/ft	Inner Berm Width ( $W_{ib}$ )		ft	
	Inner Berm Depth ( $d_{ib}$ )		ft	Inner Berm Width/Depth Ratio			$W_{ib}/d_{ib}$	Inner Berm Area ( $A_{ib}$ )		ft <sup>2</sup>
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )				<b>1.625</b>	ft/s	Estimation Method		<b>HEC-RAS</b>	
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )				<b>1000</b>	cfs	Drainage Area		<b>3406</b>	mi <sup>2</sup>

<b>Channel Pattern</b>	Geometry			Dimensionless Geometry Ratios			
	Mean	Min	Max	Mean	Min	Max	
	Meander Wavelength ( $L_m$ )	<b>1265</b>		ft	Meander Length Ratio ( $L_m/W_{bkt}$ )	<b>####</b>	
	Radius of Curvature ( $R_c$ )	<b>210</b>		ft	Radius of Curvature/Riffle Width ( $R_c/W_{bkt}$ )	<b>2.811</b>	
	Belt Width ( $W_{bit}$ )	<b>2807</b>		ft	Meander Width Ratio ( $W_{bit}/W_{bkt}$ )	<b>####</b>	
	Individual Pool Length			ft	Pool Length/Riffle Width		
	Pool to Pool Spacing			ft	Pool to Pool Spacing/Riffle Width		
Riffle Length			ft	Riffle Length/Riffle Width			

<b>Channel Profile</b>	Valley Slope (VS)		ft/ft	Average Water Surface Slope (S)		ft/ft	Sinuosity (VS/S)		
	Stream Length (SL)	<b>93167</b>	ft	Valley Length (VL)	<b>23447</b>	ft	Sinuosity (SL/VL)	<b>4.0</b>	
	Low Bank Height (LBH)	start: end:	ft	Max Riffle Depth	start: end:	ft	Bank-Height Ratio (BHR) (LBH/Max Riffle Depth)	start: end:	
	Facet Slopes			Dimensionless Slope Ratios			Mean	Min	Max
	Riffle Slope ( $S_{rif}$ )	<b>0.000</b>		ft/ft	Riffle Slope/Average Water Surface Slope ( $S_{rif} / S$ )	<b>1.000</b>			
	Run Slope ( $S_{run}$ )			ft/ft	Run Slope/Average Water Surface Slope ( $S_{run} / S$ )				
	Pool Slope ( $S_p$ )			ft/ft	Pool Slope/Average Water Surface Slope ( $S_p / S$ )				
	Glide Slope ( $S_g$ )			ft/ft	Glide Slope/Average Water Surface Slope ( $S_g / S$ )				
	Feature Midpoint <sup>a</sup>			Dimensionless Depth Ratios			Mean	Min	Max
	Max Riffle Depth ( $d_{maxrif}$ )	<b>####</b>		ft	Max Riffle Depth/Mean Riffle Depth ( $d_{maxrif} / d_{bkt}$ )	<b>1.584</b>			
	Max Run Depth ( $d_{maxrun}$ )			ft	Max Run Depth/Mean Riffle Depth ( $d_{maxrun} / d_{bkt}$ )				
	Max Pool Depth ( $d_{maxp}$ )			ft	Max Pool Depth/Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )				
	Max Glide Depth ( $d_{maxg}$ )			ft	Max Glide Depth/Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )				

<b>Channel Materials</b>	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Protrusion Height <sup>d</sup>
	% Silt/Clay	<b>6</b>		$D_{16}$	<b>0.125</b>		mm
	% Sand	<b>94</b>		$D_{35}$	<b>0.16</b>		mm
	% Gravel	<b>0</b>		$D_{50}$	<b>0.18</b>		mm
	% Cobble	<b>0</b>		$D_{84}$	<b>0.235</b>		mm
	% Boulder	<b>0</b>		$D_{95}$	<b>0.265</b>		mm
	% Bedrock	<b>0</b>		$D_{100}$	<b>4.75</b>		mm

<sup>a</sup> Min, max, mean depths are ave. mid-point values except pools: taken at deepest part of pool.

<sup>b</sup> Composite sample of riffles and pools within the designated reach.

<sup>c</sup> Active bed of a riffle.

<sup>d</sup> Height of roughness feature above bed.

**Worksheet 2-1.** Gage station and field data (Rosgen and Silvey, 2007).

Summary.... <b>USGS GAGE STATION</b> Data/Records for <b>STREAM CHANNEL CLASSIFICATION</b>					
Station NAME:	Sheyenne River-7-43.27			Station Number:	N/A
LOCATION:	Sheyenne River-7-43.27				
Period of RECORD:	N/A	yrs	Mean Annual DISCHARGE:	N/A	cfs
Drainage AREA:	2190720	acres	3423	mi <sup>2</sup>	Drainage Area Mn ELEV: 895.49 ft
Reference REACH SLOPE:		ft/ft	Valley Type:	X	
Stream Type:	E6		HUC:	_ _ _ _ _	
"BANKFULL" CHARACTERISTICS					
Determined from FIELD MEASUREMENT			Determined from GAGE DATA Analysis		
Bankfull WIDTH ( $W_{bkf}$ )	80.8	ft	Bankfull WIDTH ( $W_{bkf}$ )		ft
Bankfull Mean DEPTH ( $d_{bkf}$ )	10.1	ft	Bankfull MEAN DEPTH ( $d_{bkf}$ )		ft
Bankfull Xsec AREA ( $A_{bkf}$ )	819.7	ft <sup>2</sup>	Bankfull Xsec AREA ( $A_{bkf}$ )		ft <sup>2</sup>
Wetted PERIMETER ( $W_p$ )	89.0	ft	Wetted PERIMETER ( $W_p$ )		ft
Bankfull STAGE (Gage Ht)		ft	Bankfull STAGE (Gage Ht)		ft
Est. Mean VELOCITY ( $u$ )	1.5	ft/sec	Mean VELOCITY ( $u$ )		ft/sec
Est. Bkf. DISCHARGE ( $Q_{bkf}$ )	1200.0	cfs	Bankfull DISCHARGE ( $Q_{bkf}$ )		cfs
Bankfull DISCHARGE associated with "field-determined" Bankfull STAGE				1200.0	cfs
Recurrence Interval ( Log-Pearson ) associated with "field-determined" Bankfull Discharge				1.7	yrs
From the Annual Peak Flow Frequency Analysis data for the Gage Station, determine:					
1.5 Year R.I. Discharge..... =	N/A	cfs	10 Year R.I. Discharge..... =	N/A	cfs
2.0 Year R.I. Discharge.....=	N/A	cfs	25 Year R.I. Discharge.....=	N/A	cfs
5.0 Year R.I. Discharge.....=	N/A	cfs	50 Year R.I. Discharge..... =	N/A	cfs
MEANDER GEOMETRY					
Meander Length ( $L_m$ )	1028	ft	Radius of Curvature ( $R_C$ )	217.0	ft
Belt Width ( $W_{blt}$ )	1646	ft	Meander Width Ratio ( $W_{blt}/W_{bkf}$ )	20.4	ft/ft
HYDRAULIC GEOMETRY					
Based on USGS Discharge Summary Notes data ( Form 9-207 ) and regression analyses of measured discharge ( $Q$ ) with the hydraulic parameters of Width ( $W$ ), Area ( $A$ ), Mean Depth ( $d$ ) & Mean Velocity ( $u$ ), determine the <i>intercept coefficient</i> ( $a$ ) and the <i>slope exponent</i> ( $b$ ) values for a power function of the form $Y = aX^b$ , when $Y$ is one of the selected hydraulic parameters and $X$ is a given discharge value ( $Q$ ).					
	Width ( $W$ )	Depth ( $d$ )	Area ( $A$ )	Velocity ( $u$ )	
Intercept Coefficient: ( $a$ )					
Slope Exponent: ( $b$ )					
Hydraulic Radius: $R = A / W_p$		ft	Manning's "n" at Bankfull Stage	0.052	Coeff.
$"n" = 1.4865 [ ( Area ) ( Hydraulic Radius^{2/3} ) ( Slope^{1/2} ) ] / Q_{bkf}$					

**Worksheet 2-2.** Computations of velocity and bankfull discharge using various methods (Rosgen, 2006b; Rosgen and Silvey, 2007).

Bankfull VELOCITY / DISCHARGE Estimates										
Site	Sheyenne River-7-43.27				Location	Sheyenne River-7-43.27				
Date	10/5/2011	Stream Type	E6	Valley Type	X					
Observers	KD, JB				HUC	-- -- -- -- -- -- -- -- -- --				
INPUT VARIABLES				OUTPUT VARIABLES						
Bankfull Cross-sectional	819.7	$A_{b_{kf}}$ (ft <sup>2</sup> )	Bankfull Mean DEPTH	10.1	$D_{b_{kf}}$ (ft)					
Bankfull WIDTH	80.8	$W_{b_{kf}}$ (ft)	Wetted PERIMETER ~ 2 * $d_{b_{kf}}$ + $W_{b_{kf}}$	101.1	$W_p$ (ft)					
$D_{84}$ @ Riffle	0.12	Dia. (mm)	$D_{84}$ mm / 304.8 =	0.00	$D_{84}$ (ft)					
Bankfull SLOPE	0.0000	$S_{b_{kf}}$ (ft / ft)	Hydraulic RADIUS $A_{b_{kf}} / W_p$	8.1	R (ft)					
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R (ft) / $D_{84}$ (ft)	20600						
Drainage AREA	3423.0	DA (mi <sup>2</sup> )	Shear Velocity	0.0	$u^*$ (ft / sec)					
ESTIMATION METHODS				Bankfull VELOCITY		Bankfull DISCHARGE				
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 \text{Log} \{ R / D_{84} \} ] u^*$				0.5	ft / sec	380	cfs			
2. Roughness Coefficient: a) Manning's 'n' from friction factor / relative roughness (Figs. 2-18, 19) $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text"/>				0.1	ft / sec	100	cfs			
2. Roughness Coefficient: b) Manning's 'n' from Jarrett ( USGS ): $n = 0.39 S^{-.38} R^{-.16}$ n = <input type="text"/>				4.1	ft / sec	3400	cfs			
Note: This equation is for applications involving steep, step-pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for stream types A1, A2, A3, B1, B2, B3, C2 and E3.										
2. Roughness Coefficient: c) Manning's 'n' from Stream Type $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text" value="0.052"/>				0.1	ft / sec	100	cfs			
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.) HEC-RAS				1.5	ft / sec	1200	cfs			
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.)					ft / sec		cfs			
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge $Q = 1.46$ Yr. $u = Q / A$					ft / sec		cfs			
4. Continuity Equations: b) USGS Gage Data $u = Q / A$					ft / sec		cfs			
Options for using the $D_{84}$ term in the relative roughness relation ( $R/D_{84}$ ), when using estimation method 1.										
Option 1. For sand-bed channels: Measure the "protrusion height" ( $h_{sd}$ ) of sand dunes above channel bed elevations. Substitute an average sand dune protrusion height ( $h_{sd}$ in ft) for the $D_{84}$ term in est. method 1.										
Option 2. For boulder-dominated channels: Measure several "protrusion heights" ( $h_{bo}$ ) of boulders above channel bed elevations. Substitute an ave. boulder protrusion height ( $h_{bo}$ in ft) for the $D_{84}$ term in est. method 1.										
Option 3. For bedrock-dominated channels: Measure several "protrusion heights" ( $h_{br}$ ) of rock separations/steps/joints/uplifted surfaces above channel bed elevations. Substitute an average bedrock protrusion height ( $h_{br}$ in feet) for the $D_{84}$ term in estimation method 1.										

**Worksheet 2-3.** Field form for Level II stream classification (Rosgen, 1996; Rosgen, 2006b).

Stream: <b>Sheyenne River-7-43.27</b>	
Basin: <b>Red River Basin</b>	Drainage Area: <b>2E+06</b> acres <b>3423</b> mi <sup>2</sup>
Location: <b>Sheyenne River-7-43.27</b>	
Twp.&Rge: - Sec.&Qtr.: -	
Cross-Section Monuments (Lat./Long.): - Date: <b>10/5/2011</b>	
Observers: <b>KD, JB</b> Valley Type: <b>X</b>	

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>80.8</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>10.1</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>819.7</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>8.0</b>	ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>14.8</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>903.7</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>11.2</b>	ft/ft
<b>Channel Materials (Particle Size Index) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>0.0495</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.00000</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).	<b>1.8</b>	

<b>Stream Type</b>	<b>E6</b>	<b>See Classification Key (Figure 2-21)</b>
--------------------	-----------	---

**Worksheet 2-4.** Morphological relations, including dimensionless ratios of river reach sites (Rosgen, 2006b; Rosgen and Silvey 2007).

Stream: <b>Sheyenne River-7-43.27</b>		Location: <b>Sheyenne River-7-43.27</b>								
Observers: <b>KD, JB</b>		Date: <b>10/5/2011</b>		Valley Type: <b>X</b>		Stream Type: <b>E6</b>				
<b>River Reach Summary Data</b>										
<b>Channel Dimension</b>	Mean Riffle Depth ( $d_{bkt}$ )	<b>10.1</b>	ft	Riffle Width ( $W_{bkt}$ )	<b>80.8</b>	ft	Riffle Area ( $A_{bkt}$ )	<b>819.7</b>	ft <sup>2</sup>	
	Mean Pool Depth ( $d_{bkfp}$ )		ft	Pool Width ( $W_{bkfp}$ )		ft	Pool Area ( $A_{bkfp}$ )		ft <sup>2</sup>	
	Mean Pool Depth/Mean Riffle Depth		$d_{bkfp}/d_{bkt}$	Pool Width/Riffle Width		$W_{bkfp}/W_{bkt}$	Pool Area / Riffle Area		$A_{bkfp}/A_{bkt}$	
	Max Riffle Depth ( $d_{maxrif}$ )	<b>14.8</b>	ft	Max Pool Depth ( $d_{maxp}$ )		ft	Max Riffle Depth/Mean Riffle Depth	<b>1.5</b>		
	Max Pool Depth/Mean Riffle Depth			Point Bar Slope		ft/ft	Inner Berm Width ( $W_{ib}$ )		ft	
	Inner Berm Depth ( $d_{ib}$ )		ft	Inner Berm Width/Depth Ratio			$W_{ib}/d_{ib}$	Inner Berm Area ( $A_{ib}$ )		ft <sup>2</sup>
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )				<b>1.5</b>	ft/s	Estimation Method		<b>HEC-RAS</b>	
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )				<b>1200</b>	cfs	Drainage Area		<b>3423</b>	mi <sup>2</sup>

<b>Channel Pattern</b>	Geometry			Dimensionless Geometry Ratios			
	Mean	Min	Max	Mean	Min	Max	
	Meander Wavelength ( $L_m$ )	<b>1028</b>			ft	Meander Length Ratio ( $L_m/W_{bkt}$ )	<b>12.7</b>
	Radius of Curvature ( $R_c$ )	<b>217</b>			ft	Radius of Curvature/Riffle Width ( $R_c/W_{bkt}$ )	<b>2.7</b>
	Belt Width ( $W_{bit}$ )	<b>1646</b>			ft	Meander Width Ratio ( $W_{bit}/W_{bkt}$ )	<b>20.4</b>
	Individual Pool Length				ft	Pool Length/Riffle Width	
	Pool to Pool Spacing				ft	Pool to Pool Spacing/Riffle Width	
Riffle Length				ft	Riffle Length/Riffle Width		

<b>Channel Profile</b>	Valley Slope (VS)		ft/ft	Average Water Surface Slope (S)		ft/ft	Sinuosity (VS/S)		
	Stream Length (SL)	<b>43888</b>	ft	Valley Length (VL)	<b>24110</b>	ft	Sinuosity (SL/VL)	<b>1.8</b>	
	Low Bank Height (LBH)	start	ft	Max Riffle Depth	start	ft	Bank-Height Ratio (BHR)	start	
		end	ft		end	ft	(LBH/Max Riffle Depth)	end	
	Facet Slopes			Dimensionless Slope Ratios			Mean Min Max		
	Riffle Slope ( $S_{rif}$ )	<b>0.0</b>		ft/ft	Riffle Slope/Average Water Surface Slope ( $S_{rif}/S$ )	<b>1.0</b>			
	Run Slope ( $S_{run}$ )			ft/ft	Run Slope/Average Water Surface Slope ( $S_{run}/S$ )				
	Pool Slope ( $S_p$ )			ft/ft	Pool Slope/Average Water Surface Slope ( $S_p/S$ )				
	Glide Slope ( $S_g$ )			ft/ft	Glide Slope/Average Water Surface Slope ( $S_g/S$ )				
	Feature Midpoint <sup>a</sup>			Dimensionless Depth Ratios			Mean Min Max		
	Max Riffle Depth ( $d_{maxrif}$ )	<b>14.8</b>		ft	Max Riffle Depth/Mean Riffle Depth ( $d_{maxrif}/d_{bkt}$ )	<b>1.5</b>			
	Max Run Depth ( $d_{maxrun}$ )			ft	Max Run Depth/Mean Riffle Depth ( $d_{maxrun}/d_{bkt}$ )				
	Max Pool Depth ( $d_{maxp}$ )			ft	Max Pool Depth/Mean Riffle Depth ( $d_{maxp}/d_{bkt}$ )				
Max Glide Depth ( $d_{maxg}$ )			ft	Max Glide Depth/Mean Riffle Depth ( $d_{maxg}/d_{bkt}$ )					

<b>Channel Materials</b>	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Protrusion Height <sup>d</sup>	
	% Silt/Clay	<b>66</b>			$D_{16}$	<b>&lt;.001</b>		mm
	% Sand	<b>34</b>			$D_{35}$	<b>0.026</b>		mm
	% Gravel	<b>0</b>			$D_{50}$	<b>0.0495</b>		mm
	% Cobble	<b>0</b>			$D_{84}$	<b>0.12</b>		mm
	% Boulder	<b>0</b>			$D_{95}$	<b>0.19</b>		mm
	% Bedrock	<b>0</b>			$D_{100}$	<b>2</b>		mm

<sup>a</sup> Min, max, mean depths are ave. mid-point values except pools: taken at deepest part of pool.

<sup>b</sup> Composite sample of riffles and pools within the designated reach.

<sup>c</sup> Active bed of a riffle.

<sup>d</sup> Height of roughness feature above bed.

**Worksheet 2-1.** Gage station and field data (Rosgen and Silvey, 2007).

Summary.... <b>USGS GAGE STATION</b> Data/Records for <b>STREAM CHANNEL CLASSIFICATION</b>					
Station NAME:	Sheyenne River - 6 - 35.82			Station Number:	N/A
LOCATION:	Sheyenne River - 6 - 35.82				
Period of RECORD:	N/A	yrs	Mean Annual DISCHARGE:	N/A	cfs
Drainage AREA:	2197120	acres	3433	mi <sup>2</sup>	Drainage Area Mn ELEV: 891.87 ft
Reference REACH SLOPE:		ft/ft	Valley Type:	X	
Stream Type:	E6		HUC:	-- -- -- -- -- -- -- -- -- --	
"BANKFULL" CHARACTERISTICS					
Determined from FIELD MEASUREMENT			Determined from GAGE DATA Analysis		
Bankfull WIDTH ( $W_{bkf}$ )	72.0	ft	Bankfull WIDTH ( $W_{bkf}$ )		ft
Bankfull Mean DEPTH ( $d_{bkf}$ )	7.9	ft	Bankfull MEAN DEPTH ( $d_{bkf}$ )		ft
Bankfull Xsec AREA ( $A_{bkf}$ )	568.9	ft <sup>2</sup>	Bankfull Xsec AREA ( $A_{bkf}$ )		ft <sup>2</sup>
Wetted PERIMETER ( $W_p$ )	78.0	ft	Wetted PERIMETER ( $W_p$ )		ft
Bankfull STAGE (Gage Ht)		ft	Bankfull STAGE (Gage Ht)		ft
Est. Mean VELOCITY ( $u$ )	1.5	ft/sec	Mean VELOCITY ( $u$ )		ft/sec
Est. Bkf. DISCHARGE ( $Q_{bkf}$ )	860.0	cfs	Bankfull DISCHARGE ( $Q_{bkf}$ )		cfs
Bankfull DISCHARGE associated with "field-determined" Bankfull STAGE				860.0	cfs
Recurrence Interval ( Log-Pearson ) associated with "field-determined" Bankfull Discharge				1.4	yrs
From the Annual Peak Flow Frequency Analysis data for the Gage Station, determine:					
1.5 Year R.I. Discharge..... =	N/A	cfs	10 Year R.I. Discharge..... =	N/A	cfs
2.0 Year R.I. Discharge.....=	N/A	cfs	25 Year R.I. Discharge.....=	N/A	cfs
5.0 Year R.I. Discharge.....=	N/A	cfs	50 Year R.I. Discharge..... =	N/A	cfs
MEANDER GEOMETRY					
Meander Length ( $L_m$ )	936	ft	Radius of Curvature ( $R_C$ )	224.0	ft
Belt Width ( $W_{blt}$ )	1744	ft	Meander Width Ratio ( $W_{blt}/W_{bkf}$ )	24.2	ft/ft
HYDRAULIC GEOMETRY					
Based on USGS Discharge Summary Notes data ( Form 9-207 ) and regression analyses of measured discharge ( $Q$ ) with the hydraulic parameters of Width ( $W$ ), Area ( $A$ ), Mean Depth ( $d$ ) & Mean Velocity ( $u$ ), determine the <i>intercept coefficient</i> ( $a$ ) and the <i>slope exponent</i> ( $b$ ) values for a power function of the form $Y = aX^b$ , when $Y$ is one of the selected hydraulic parameters and $X$ is a given discharge value ( $Q$ ).					
	Width ( $W$ )	Depth ( $d$ )	Area ( $A$ )	Velocity ( $u$ )	
Intercept Coefficient: ( $a$ )					
Slope Exponent: ( $b$ )					
Hydraulic Radius: $R = A / W_p$		ft	Manning's "n" at Bankfull Stage	0.046	Coeff.
$"n" = 1.4865 [ ( Area ) ( Hydraulic Radius^{2/3} ) ( Slope^{1/2} ) ] / Q_{bkf}$					

**Worksheet 2-2.** Computations of velocity and bankfull discharge using various methods (Rosgen, 2006b; Rosgen and Silvey, 2007).

Bankfull VELOCITY / DISCHARGE Estimates									
Site	Sheyenne River - 6 - 35.82			Location	Sheyenne River - 6 - 35.82				
Date	11/21/2010	Stream Type	E6	Valley Type	X				
Observers	KP, AL			HUC	-- -- -- -- -- -- -- -- -- --				
INPUT VARIABLES				OUTPUT VARIABLES					
Bankfull Cross-sectional	568.9	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Mean DEPTH	7.9	$D_{bkf}$ (ft)				
Bankfull WIDTH	72.0	$W_{bkf}$ (ft)	Wetted PERIMETER $\sim 2 * d_{bkf} + W_{bkf}$	87.8	$W_p$ (ft)				
$D_{84}$ @ Riffle	0.12	Dia. (mm)	$D_{84}$ mm / 304.8 =	0.00	$D_{84}$ (ft)				
Bankfull SLOPE	0.0002	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	6.5	R (ft)				
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R (ft) / $D_{84}$ (ft)	16455					
Drainage AREA	3433.0	DA (mi <sup>2</sup> )	Shear Velocity $u^* = \sqrt{gRS}$	0.2	$u^*$ (ft / sec)				
ESTIMATION METHODS				Bankfull VELOCITY		Bankfull DISCHARGE			
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 \text{Log}\{ R / D_{84} \} ] u^*$				4.8	ft / sec	2709	cfs		
2. Roughness Coefficient: a) Manning's 'n' from friction factor / relative roughness (Figs. 2-18, 19) $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text"/>				1.4	ft / sec	789	cfs		
2. Roughness Coefficient: b) Manning's 'n' from Jarrett ( USGS ): $n = 0.39S^{-.38}R^{-.16}$ n = <input type="text"/>				6.2	ft / sec	3540	cfs		
Note: This equation is for applications involving steep, step-pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for stream types A1, A2, A3, B1, B2, B3, C2 and E3.									
2. Roughness Coefficient: c) Manning's 'n' from Stream Type $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text" value="0.046"/>				1.4	ft / sec	789	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.) HEC-RAS				1.5	ft / sec	860	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.)					ft / sec		cfs		
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge $u = Q / A$ Q = <input type="text" value="1.46"/> Yr.					ft / sec		cfs		
4. Continuity Equations: b) USGS Gage Data $u = Q / A$					ft / sec		cfs		
Options for using the $D_{84}$ term in the relative roughness relation (R/ $D_{84}$ ), when using estimation method 1.									
Option 1. For sand-bed channels: Measure the "protrusion height" ( $h_{sd}$ ) of sand dunes above channel bed elevations. Substitute an average sand dune protrusion height ( $h_{sd}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 2. For boulder-dominated channels: Measure several "protrusion heights" ( $h_{bo}$ ) of boulders above channel bed elevations. Substitute an ave. boulder protrusion height ( $h_{bo}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 3. For bedrock-dominated channels: Measure several "protrusion heights" ( $h_{br}$ ) of rock separations/steps/joints/uplifted surfaces above channel bed elevations. Substitute an average bedrock protrusion height ( $h_{br}$ in feet) for the $D_{84}$ term in estimation method 1.									

**Worksheet 2-3.** Field form for Level II stream classification (Rosgen, 1996; Rosgen , 2006b).

Stream: <b>Sheyenne River - 6 - 35.82</b>	
Basin: <b>Red River Basin</b>	Drainage Area: <b>2E+06</b> acres <b>3433</b> mi <sup>2</sup>
Location: <b>Sheyenne River - 6 - 35.82</b>	
Twp.&Rge: -	Sec.&Qtr.: -
Cross-Section Monuments (Lat./Long.): -	Date: <b>11/21/2010</b>
Observers: <b>KP, AL</b>	Valley Type: <b>X</b>

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>72.0</b> ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>7.9</b> ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>568.9</b> ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>9.1</b> ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>11.6</b> ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>810.8</b> ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>11.3</b> ft/ft
<b>Channel Materials (Particle Size Index ) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>0.0175</b> mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.00015</b> ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).	<b>1.8</b>

<div style="border: 1px solid black; padding: 5px; display: inline-block;"> <b>Stream Type</b> </div>	<div style="border: 1px solid black; padding: 5px; display: inline-block; background-color: yellow;"> <b>E6</b> </div>	<div style="border: 1px solid black; padding: 5px; display: inline-block;"> <b>See Classification Key (Figure 2-21)</b> </div>
---	--	--

**Worksheet 2-4.** Morphological relations, including dimensionless ratios of river reach sites (Rosgen, 2006b; Rosgen and Silvey 2007).

Stream: <b>Sheyenne River - 6 - 35.82</b>		Location: <b>Sheyenne River - 6 - 35.82</b>								
Observers: <b>KP, AL</b>		Date: <b>11/21/2010</b>		Valley Type: <b>X</b>		Stream Type: <b>E6</b>				
<b>River Reach Summary Data</b>										
<b>Channel Dimension</b>	Mean Riffle Depth ( $d_{bkt}$ )	<b>7.9</b>	ft	Riffle Width ( $W_{bkt}$ )	<b>72.0</b>	ft	Riffle Area ( $A_{bkt}$ )	<b>568.9</b>	ft <sup>2</sup>	
	Mean Pool Depth ( $d_{bkfp}$ )		ft	Pool Width ( $W_{bkfp}$ )		ft	Pool Area ( $A_{bkfp}$ )		ft <sup>2</sup>	
	Mean Pool Depth/Mean Riffle Depth		$d_{bkfp}/d_{bkt}$	Pool Width/Riffle Width		$W_{bkfp}/W_{bkt}$	Pool Area / Riffle Area		$A_{bkfp}/A_{bkt}$	
	Max Riffle Depth ( $d_{maxrif}$ )	<b>11.6</b>	ft	Max Pool Depth ( $d_{maxp}$ )		ft	Max Riffle Depth/Mean Riffle Depth	<b>1.5</b>		
	Max Pool Depth/Mean Riffle Depth			Point Bar Slope		ft/ft	Inner Berm Width ( $W_{ib}$ )		ft	
	Inner Berm Depth ( $d_{ib}$ )		ft	Inner Berm Width/Depth Ratio			$W_{ib}/d_{ib}$	Inner Berm Area ( $A_{ib}$ )		ft <sup>2</sup>
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )				<b>1.5</b>	ft/s	Estimation Method		<b>HEC-RAS</b>	
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )				<b>860</b>	cfs	Drainage Area		<b>3433</b>	mi <sup>2</sup>

<b>Channel Pattern</b>	Geometry			Dimensionless Geometry Ratios			
	Mean	Min	Max	Mean	Min	Max	
	Meander Wavelength ( $L_m$ )	<b>936</b>			ft	Meander Length Ratio ( $L_m/W_{bkt}$ )	<b>13.0</b>
	Radius of Curvature ( $R_c$ )	<b>224</b>			ft	Radius of Curvature/Riffle Width ( $R_c/W_{bkt}$ )	<b>3.1</b>
	Belt Width ( $W_{bit}$ )	<b>1744</b>			ft	Meander Width Ratio ( $W_{bit}/W_{bkt}$ )	<b>24.2</b>
	Individual Pool Length				ft	Pool Length/Riffle Width	
	Pool to Pool Spacing				ft	Pool to Pool Spacing/Riffle Width	
Riffle Length				ft	Riffle Length/Riffle Width		

<b>Channel Profile</b>	Valley Slope (VS)		ft/ft	Average Water Surface Slope (S)		ft/ft	Sinuosity (VS/S)		
	Stream Length (SL)	<b>61075</b>	ft	Valley Length (VL)	<b>34279</b>	ft	Sinuosity (SL/VL)	<b>1.8</b>	
	Low Bank Height (LBH)	start: end:	ft ft	Max Riffle Depth	start: end:	ft ft	Bank-Height Ratio (BHR) (LBH/Max Riffle Depth)	start: end:	
	Facet Slopes			Dimensionless Slope Ratios			Mean	Min	Max
	Riffle Slope ( $S_{rif}$ )	<b>0.0</b>		ft/ft	Riffle Slope/Average Water Surface Slope ( $S_{rif} / S$ )	<b>1.0</b>			
	Run Slope ( $S_{run}$ )			ft/ft	Run Slope/Average Water Surface Slope ( $S_{run} / S$ )				
	Pool Slope ( $S_p$ )			ft/ft	Pool Slope/Average Water Surface Slope ( $S_p / S$ )				
	Glide Slope ( $S_g$ )			ft/ft	Glide Slope/Average Water Surface Slope ( $S_g / S$ )				
	Feature Midpoint <sup>a</sup>			Dimensionless Depth Ratios			Mean	Min	Max
	Max Riffle Depth ( $d_{maxrif}$ )	<b>11.6</b>		ft	Max Riffle Depth/Mean Riffle Depth ( $d_{maxrif} / d_{bkt}$ )	<b>1.5</b>			
	Max Run Depth ( $d_{maxrun}$ )			ft	Max Run Depth/Mean Riffle Depth ( $d_{maxrun} / d_{bkt}$ )				
	Max Pool Depth ( $d_{maxp}$ )			ft	Max Pool Depth/Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )				
	Max Glide Depth ( $d_{maxg}$ )			ft	Max Glide Depth/Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )				

<b>Channel Materials</b>	Reach <sup>b</sup>		Riffle <sup>c</sup>	Bar	Reach <sup>b</sup>		Riffle <sup>c</sup>	Bar	Protrusion Height <sup>d</sup>	
	% Silt/Clay	<b>73</b>			$D_{16}$	<b>&lt;.001</b>				mm
	% Sand	<b>27</b>			$D_{35}$	<b>0.0035</b>				mm
	% Gravel	<b>0</b>			$D_{50}$	<b>0.0175</b>				mm
	% Cobble	<b>0</b>			$D_{84}$	<b>0.12</b>				mm
	% Boulder	<b>0</b>			$D_{95}$	<b>0.18</b>				mm
	% Bedrock	<b>0</b>			$D_{100}$	<b>2</b>				mm

<sup>a</sup> Min, max, mean depths are ave. mid-point values except pools: taken at deepest part of pool.

<sup>b</sup> Composite sample of riffles and pools within the designated reach.

<sup>c</sup> Active bed of a riffle.

<sup>d</sup> Height of roughness feature above bed.

**Worksheet 2-1.** Gage station and field data (Rosgen and Silvey, 2007).

Summary.... <b>USGS GAGE STATION</b> Data/Records for <b>STREAM CHANNEL CLASSIFICATION</b>					
Station NAME:	Sheyenne River-5-26.47			Station Number:	N/A
LOCATION:	Sheyenne River-5-26.47				
Period of RECORD:	N/A	yrs	Mean Annual DISCHARGE:	N/A	cfs
Drainage AREA:	2224640	acres	3476	mi <sup>2</sup>	Drainage Area Mn ELEV: 881.57 ft
Reference REACH SLOPE:		ft/ft	Valley Type:	X	
Stream Type:	E5		HUC:	-- -- -- -- -- -- -- -- -- --	
"BANKFULL" CHARACTERISTICS					
Determined from FIELD MEASUREMENT			Determined from GAGE DATA Analysis		
Bankfull WIDTH ( $W_{bkf}$ )	62.7	ft	Bankfull WIDTH ( $W_{bkf}$ )		ft
Bankfull Mean DEPTH ( $d_{bkf}$ )	6.1	ft	Bankfull MEAN DEPTH ( $d_{bkf}$ )		ft
Bankfull Xsec AREA ( $A_{bkf}$ )	379.3	ft <sup>2</sup>	Bankfull Xsec AREA ( $A_{bkf}$ )		ft <sup>2</sup>
Wetted PERIMETER ( $W_p$ )	67.5	ft	Wetted PERIMETER ( $W_p$ )		ft
Bankfull STAGE (Gage Ht)		ft	Bankfull STAGE (Gage Ht)		ft
Est. Mean VELOCITY ( $u$ )	1.5	ft/sec	Mean VELOCITY ( $u$ )		ft/sec
Est. Bkf. DISCHARGE ( $Q_{bkf}$ )	580.0	cfs	Bankfull DISCHARGE ( $Q_{bkf}$ )		cfs
Bankfull DISCHARGE associated with "field-determined" Bankfull STAGE				580.0	cfs
Recurrence Interval ( Log-Pearson ) associated with "field-determined" Bankfull Discharge				1.2	yrs
From the Annual Peak Flow Frequency Analysis data for the Gage Station, determine:					
1.5 Year R.I. Discharge..... =	N/A	cfs	10 Year R.I. Discharge..... =	N/A	cfs
2.0 Year R.I. Discharge..... =	N/A	cfs	25 Year R.I. Discharge..... =	N/A	cfs
5.0 Year R.I. Discharge..... =	N/A	cfs	50 Year R.I. Discharge..... =	N/A	cfs
MEANDER GEOMETRY					
Meander Length ( $L_m$ )	850	ft	Radius of Curvature ( $R_C$ )	196.0	ft
Belt Width ( $W_{blt}$ )	2230	ft	Meander Width Ratio ( $W_{blt}/W_{bkf}$ )	35.5	ft/ft
HYDRAULIC GEOMETRY					
Based on USGS Discharge Summary Notes data ( Form 9-207 ) and regression analyses of measured discharge ( $Q$ ) with the hydraulic parameters of Width ( $W$ ), Area ( $A$ ), Mean Depth ( $d$ ) & Mean Velocity ( $u$ ), determine the <i>intercept coefficient</i> ( $a$ ) and the <i>slope exponent</i> ( $b$ ) values for a power function of the form $Y = aX^b$ , when $Y$ is one of the selected hydraulic parameters and $X$ is a given discharge value ( $Q$ ).					
	Width ( $W$ )	Depth ( $d$ )	Area ( $A$ )	Velocity ( $u$ )	
Intercept Coefficient: ( $a$ )					
Slope Exponent: ( $b$ )					
Hydraulic Radius: $R = A / W_p$		ft	Manning's "n" at Bankfull Stage	0.046	Coeff.
$"n" = 1.4865 [ ( Area ) ( Hydraulic Radius^{2/3} ) ( Slope^{1/2} ) ] / Q_{bkf}$					

**Worksheet 2-2.** Computations of velocity and bankfull discharge using various methods (Rosgen, 2006b; Rosgen and Silvey, 2007).

Bankfull VELOCITY / DISCHARGE Estimates										
Site	Sheyenne River-5-26.47				Location	Sheyenne River-5-26.47				
Date	10/5/2011	Stream Type	E5	Valley Type	X					
Observers	KP, AL				HUC	-- -- -- -- -- -- -- -- -- --				
INPUT VARIABLES				OUTPUT VARIABLES						
Bankfull Cross-sectional	379.3	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Mean DEPTH	6.1	$D_{bkf}$ (ft)					
Bankfull WIDTH	62.7	$W_{bkf}$ (ft)	Wetted PERIMETER $\sim 2 * d_{bkf} + W_{bkf}$	74.9	$W_p$ (ft)					
$D_{84}$ @ Riffle	0.24	Dia. (mm)	$D_{84}$ mm / 304.8 =	0.00	$D_{84}$ (ft)					
Bankfull SLOPE	0.0002	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	5.1	R (ft)					
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R (ft) / $D_{84}$ (ft)	6435						
Drainage AREA	3476.0	DA (mi <sup>2</sup> )	Shear Velocity $u^* = \sqrt{gRS}$	0.2	$u^*$ (ft / sec)					
ESTIMATION METHODS					Bankfull VELOCITY		Bankfull DISCHARGE			
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66\text{Log}\{ R / D_{84} \} ] u^*$					4.0	ft / sec	1525	cfs		
2. Roughness Coefficient: a) Manning's 'n' from friction factor / relative roughness (Figs. 2-18, 19) $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text"/>					1.2	ft / sec	467	cfs		
2. Roughness Coefficient: b) Manning's 'n' from Jarrett ( USGS ): $n = 0.39S^{-.38}R^{-.16}$ n = <input type="text"/> Note: This equation is for applications involving steep, step-pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for stream types A1, A2, A3, B1, B2, B3, C2 and E3.					5.1	ft / sec	1946	cfs		
2. Roughness Coefficient: c) Manning's 'n' from Stream Type $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text" value="0.046"/>					1.2	ft / sec	467	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.) HEC-RAS					1.5	ft / sec	580	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.)						ft / sec		cfs		
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge $u = Q / A$ Q = <input type="text" value="1.46"/> Yr.						ft / sec		cfs		
4. Continuity Equations: b) USGS Gage Data $u = Q / A$						ft / sec		cfs		
Options for using the $D_{84}$ term in the relative roughness relation ( $R/D_{84}$ ), when using estimation method 1.										
Option 1. For sand-bed channels: Measure the "protrusion height" ( $h_{sd}$ ) of sand dunes above channel bed elevations. Substitute an average sand dune protrusion height ( $h_{sd}$ in ft) for the $D_{84}$ term in est. method 1.										
Option 2. For boulder-dominated channels: Measure several "protrusion heights" ( $h_{bo}$ ) of boulders above channel bed elevations. Substitute an ave. boulder protrusion height ( $h_{bo}$ in ft) for the $D_{84}$ term in est. method 1.										
Option 3. For bedrock-dominated channels: Measure several "protrusion heights" ( $h_{br}$ ) of rock separations/steps/joints/uplifted surfaces above channel bed elevations. Substitute an average bedrock protrusion height ( $h_{br}$ in feet) for the $D_{84}$ term in estimation method 1.										

**Worksheet 2-3.** Field form for Level II stream classification (Rosgen, 1996; Rosgen , 2006b).

Stream: <b>Sheyenne River-5-26.47</b>	
Basin: <b>Red River Basin</b>	Drainage Area: <b>2E+06</b> acres <b>3476</b> mi <sup>2</sup>
Location: <b>Sheyenne River-5-26.47</b>	
Twp.&Rge: - Sec.&Qtr.: -	
Cross-Section Monuments (Lat./Long.): - Date: <b>10/5/2011</b>	
Observers: <b>KP, AL</b> Valley Type: <b>X</b>	

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>62.7</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>6.1</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>379.3</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>10.4</b>	ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>9.9</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>376.7</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>6.0</b>	ft/ft
<b>Channel Materials (Particle Size Index ) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>0.12</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.00017</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).	<b>1.7</b>	

<b>Stream Type</b>	<b>E5</b>	<b>See Classification Key (Figure 2-21)</b>
--------------------	-----------	---

**Worksheet 2-4.** Morphological relations, including dimensionless ratios of river reach sites (Rosgen, 2006b; Rosgen and Silvey 2007).

Stream: <b>Sheyenne River-5-26.47</b>		Location: <b>Sheyenne River-5-26.47</b>								
Observers: <b>KP, AL</b>		Date: <b>10/5/2011</b>		Valley Type: <b>X</b>		Stream Type: <b>E5</b>				
<b>River Reach Summary Data</b>										
<b>Channel Dimension</b>	Mean Riffle Depth ( $d_{bkt}$ )	<b>6.1</b>	ft	Riffle Width ( $W_{bkt}$ )	<b>62.7</b>	ft	Riffle Area ( $A_{bkt}$ )	<b>379.3</b>	ft <sup>2</sup>	
	Mean Pool Depth ( $d_{bkfp}$ )		ft	Pool Width ( $W_{bkfp}$ )		ft	Pool Area ( $A_{bkfp}$ )		ft <sup>2</sup>	
	Mean Pool Depth/Mean Riffle Depth		$d_{bkfp}/d_{bkt}$	Pool Width/Riffle Width		$W_{bkfp}/W_{bkt}$	Pool Area / Riffle Area		$A_{bkfp}/A_{bkt}$	
	Max Riffle Depth ( $d_{maxrif}$ )	<b>9.89</b>	ft	Max Pool Depth ( $d_{maxp}$ )		ft	Max Riffle Depth/Mean Riffle Depth	<b>1.6</b>		
	Max Pool Depth/Mean Riffle Depth			Point Bar Slope		ft/ft	Inner Berm Width ( $W_{ib}$ )		ft	
	Inner Berm Depth ( $d_{ib}$ )		ft	Inner Berm Width/Depth Ratio			$W_{ib}/d_{ib}$	Inner Berm Area ( $A_{ib}$ )		ft <sup>2</sup>
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )				<b>1.5</b>	ft/s	Estimation Method		<b>HEC-RAS</b>	
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )				<b>580</b>	cfs	Drainage Area		<b>3476</b>	mi <sup>2</sup>

<b>Channel Pattern</b>	Geometry			Dimensionless Geometry Ratios			
	Mean	Min	Max	Mean	Min	Max	
	Meander Wavelength ( $L_m$ )	<b>850</b>			ft	Meander Length Ratio ( $L_m/W_{bkt}$ )	<b>13.5</b>
	Radius of Curvature ( $R_c$ )	<b>196</b>			ft	Radius of Curvature/Riffle Width ( $R_c/W_{bkt}$ )	<b>3.1</b>
	Belt Width ( $W_{bit}$ )	<b>2230</b>			ft	Meander Width Ratio ( $W_{bit}/W_{bkt}$ )	<b>35.5</b>
	Individual Pool Length				ft	Pool Length/Riffle Width	
	Pool to Pool Spacing				ft	Pool to Pool Spacing/Riffle Width	
Riffle Length				ft	Riffle Length/Riffle Width		

<b>Channel Profile</b>	Valley Slope (VS)		ft/ft	Average Water Surface Slope (S)		ft/ft	Sinuosity (VS/S)		
	Stream Length (SL)	<b>32606</b>	ft	Valley Length (VL)	<b>19226</b>	ft	Sinuosity (SL/VL)	<b>1.7</b>	
	Low Bank Height (LBH)	start	ft	Max Riffle Depth	start	ft	Bank-Height Ratio (BHR)	start	
		end	ft		end	ft	(LBH/Max Riffle Depth)	end	
	Facet Slopes			Dimensionless Slope Ratios			Mean	Min	Max
	Riffle Slope ( $S_{rif}$ )	<b>0.0</b>		ft/ft	Riffle Slope/Average Water Surface Slope ( $S_{rif} / S$ )	<b>1.0</b>			
	Run Slope ( $S_{run}$ )			ft/ft	Run Slope/Average Water Surface Slope ( $S_{run} / S$ )				
	Pool Slope ( $S_p$ )			ft/ft	Pool Slope/Average Water Surface Slope ( $S_p / S$ )				
	Glide Slope ( $S_g$ )			ft/ft	Glide Slope/Average Water Surface Slope ( $S_g / S$ )				
	Feature Midpoint <sup>a</sup>			Dimensionless Depth Ratios			Mean	Min	Max
	Max Riffle Depth ( $d_{maxrif}$ )	<b>9.9</b>		ft	Max Riffle Depth/Mean Riffle Depth ( $d_{maxrif} / d_{bkt}$ )	<b>1.6</b>			
	Max Run Depth ( $d_{maxrun}$ )			ft	Max Run Depth/Mean Riffle Depth ( $d_{maxrun} / d_{bkt}$ )				
Max Pool Depth ( $d_{maxp}$ )			ft	Max Pool Depth/Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )					
Max Glide Depth ( $d_{maxg}$ )			ft	Max Glide Depth/Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )					

<b>Channel Materials</b>	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Protrusion Height <sup>d</sup>	
	% Silt/Clay	<b>37</b>			$D_{16}$	<b>&lt;.001</b>		mm
	% Sand	<b>63</b>			$D_{35}$	<b>0.071</b>		mm
	% Gravel	<b>0</b>			$D_{50}$	<b>0.12</b>		mm
	% Cobble	<b>0</b>			$D_{84}$	<b>0.24</b>		mm
	% Boulder	<b>0</b>			$D_{95}$	<b>0.49</b>		mm
	% Bedrock	<b>0</b>			$D_{100}$	<b>5</b>		mm

<sup>a</sup> Min, max, mean depths are ave. mid-point values except pools: taken at deepest part of pool.

<sup>b</sup> Composite sample of riffles and pools within the designated reach.

<sup>c</sup> Active bed of a riffle.

<sup>d</sup> Height of roughness feature above bed.

**Worksheet 2-1.** Gage station and field data (Rosgen and Silvey, 2007).

Summary.... <b>USGS GAGE STATION</b> Data/Records for <b>STREAM CHANNEL CLASSIFICATION</b>					
Station NAME:	Sheyenne River-4-22.27			Station Number:	N/A
LOCATION:	Sheyenne River-4-22.27				
Period of RECORD:	N/A	yrs	Mean Annual DISCHARGE:	N/A	cfs
Drainage AREA:	2229120	acres	3483	mi <sup>2</sup>	Drainage Area Mn ELEV: 871.97 ft
Reference REACH SLOPE:		ft/ft	Valley Type:	X	
Stream Type:	E6		HUC:	-- -- -- -- -- -- -- -- -- -- -- -- -- -- -- --	
"BANKFULL" CHARACTERISTICS					
Determined from FIELD MEASUREMENT			Determined from GAGE DATA Analysis		
Bankfull WIDTH ( $W_{bkf}$ )	71.5	ft	Bankfull WIDTH ( $W_{bkf}$ )		ft
Bankfull Mean DEPTH ( $d_{bkf}$ )	8.6	ft	Bankfull MEAN DEPTH ( $d_{bkf}$ )		ft
Bankfull Xsec AREA ( $A_{bkf}$ )	571.8	ft <sup>2</sup>	Bankfull Xsec AREA ( $A_{bkf}$ )		ft <sup>2</sup>
Wetted PERIMETER ( $W_p$ )	73.8	ft	Wetted PERIMETER ( $W_p$ )		ft
Bankfull STAGE (Gage Ht)		ft	Bankfull STAGE (Gage Ht)		ft
Est. Mean VELOCITY ( $u$ )	1.8	ft/sec	Mean VELOCITY ( $u$ )		ft/sec
Est. Bkf. DISCHARGE ( $Q_{bkf}$ )	1030.0	cfs	Bankfull DISCHARGE ( $Q_{bkf}$ )		cfs
Bankfull DISCHARGE associated with "field-determined" Bankfull STAGE				1030.0	cfs
Recurrence Interval ( Log-Pearson ) associated with "field-determined" Bankfull Discharge				1.5	yrs
From the Annual Peak Flow Frequency Analysis data for the Gage Station, determine:					
1.5 Year R.I. Discharge..... =	N/A	cfs	10 Year R.I. Discharge..... =	N/A	cfs
2.0 Year R.I. Discharge..... =	N/A	cfs	25 Year R.I. Discharge..... =	N/A	cfs
5.0 Year R.I. Discharge..... =	N/A	cfs	50 Year R.I. Discharge..... =	N/A	cfs
MEANDER GEOMETRY					
Meander Length ( $L_m$ )	923	ft	Radius of Curvature ( $R_C$ )	178.0	ft
Belt Width ( $W_{blt}$ )	1243	ft	Meander Width Ratio ( $W_{blt}/W_{bkf}$ )	17.4	ft/ft
HYDRAULIC GEOMETRY					
Based on USGS Discharge Summary Notes data ( Form 9-207 ) and regression analyses of measured discharge ( $Q$ ) with the hydraulic parameters of Width ( $W$ ), Area ( $A$ ), Mean Depth ( $d$ ) & Mean Velocity ( $u$ ), determine the <i>intercept coefficient</i> ( $a$ ) and the <i>slope exponent</i> ( $b$ ) values for a power function of the form $Y = aX^b$ , when $Y$ is one of the selected hydraulic parameters and $X$ is a given discharge value ( $Q$ ).					
	Width ( $W$ )	Depth ( $d$ )	Area ( $A$ )	Velocity ( $u$ )	
Intercept Coefficient: ( $a$ )					
Slope Exponent: ( $b$ )					
Hydraulic Radius: $R = A / W_p$		ft	Manning's "n" at Bankfull Stage	0.054	Coeff.
$"n" = 1.4865 [ ( Area ) ( Hydraulic Radius^{2/3} ) ( Slope^{1/2} ) ] / Q_{bkf}$					

**Worksheet 2-2.** Computations of velocity and bankfull discharge using various methods (Rosgen, 2006b; Rosgen and Silvey, 2007).

Bankfull VELOCITY / DISCHARGE Estimates										
Site	Sheyenne River-4-22.27				Location	Sheyenne River-4-22.27				
Date	10/1/2011	Stream Type	E6	Valley Type	X					
Observers	KP, AL				HUC	-- -- -- -- -- -- -- -- -- --				
INPUT VARIABLES				OUTPUT VARIABLES						
Bankfull Cross-sectional	571.8	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Mean DEPTH	8.6	$D_{bkf}$ (ft)					
Bankfull WIDTH	71.5	$W_{bkf}$ (ft)	Wetted PERIMETER $\sim 2 * d_{bkf} + W_{bkf}$	88.6	$W_p$ (ft)					
$D_{84}$ @ Riffle	0.13	Dia. (mm)	$D_{84}$ mm / 304.8 =	0.00	$D_{84}$ (ft)					
Bankfull SLOPE	0.0003	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	6.5	R (ft)					
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R (ft) / $D_{84}$ (ft)	14902						
Drainage AREA	3483.0	DA (mi <sup>2</sup> )	Shear Velocity $u^* = \sqrt{gRS}$	0.3	$u^*$ (ft / sec)					
ESTIMATION METHODS				Bankfull VELOCITY		Bankfull DISCHARGE				
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 \text{Log}\{ R / D_{84} \} ] u^*$				7.0	ft / sec	3980	cfs			
2. Roughness Coefficient: a) Manning's 'n' from friction factor / relative roughness (Figs. 2-18, 19) $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text"/>				1.7	ft / sec	996	cfs			
2. Roughness Coefficient: b) Manning's 'n' from Jarrett ( USGS ): $n = 0.39S^{-.38}R^{-.16}$ n = <input type="text"/>				6.8	ft / sec	3895	cfs			
Note: This equation is for applications involving steep, step-pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for stream types A1, A2, A3, B1, B2, B3, C2 and E3.										
2. Roughness Coefficient: c) Manning's 'n' from Stream Type $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text" value="0.054"/>				1.7	ft / sec	996	cfs			
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.) HEC-RAS				1.8	ft / sec	1030	cfs			
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.)					ft / sec		cfs			
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge Q = <input type="text" value="1.46"/> Yr. $u = Q / A$					ft / sec		cfs			
4. Continuity Equations: b) USGS Gage Data $u = Q / A$					ft / sec		cfs			
Options for using the $D_{84}$ term in the relative roughness relation (R/ $D_{84}$ ), when using estimation method 1.										
Option 1. For sand-bed channels: Measure the "protrusion height" ( $h_{sd}$ ) of sand dunes above channel bed elevations. Substitute an average sand dune protrusion height ( $h_{sd}$ in ft) for the $D_{84}$ term in est. method 1.										
Option 2. For boulder-dominated channels: Measure several "protrusion heights" ( $h_{bo}$ ) of boulders above channel bed elevations. Substitute an ave. boulder protrusion height ( $h_{bo}$ in ft) for the $D_{84}$ term in est. method 1.										
Option 3. For bedrock-dominated channels: Measure several "protrusion heights" ( $h_{br}$ ) of rock separations/steps/joints/uplifted surfaces above channel bed elevations. Substitute an average bedrock protrusion height ( $h_{br}$ in feet) for the $D_{84}$ term in estimation method 1.										

**Worksheet 2-3.** Field form for Level II stream classification (Rosgen, 1996; Rosgen , 2006b).

Stream: <b>Sheyenne River-4-22.27</b>	
Basin: <b>Red River Basin</b>	Drainage Area: <b>2E+06</b> acres <b>3483</b> mi <sup>2</sup>
Location: <b>Sheyenne River-4-22.27</b>	
Twp.&Rge: - Sec.&Qtr.: -	
Cross-Section Monuments (Lat./Long.): - Date: <b>10/1/2011</b>	
Observers: <b>KP, AL</b> Valley Type: <b>X</b>	

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>71.5</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>8.6</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>571.8</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>8.4</b>	ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>12.8</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>535.7</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>7.5</b>	ft/ft
<b>Channel Materials (Particle Size Index ) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>0.073</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.00033</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).	<b>1.8</b>	

<div style="border: 1px solid black; padding: 5px; display: inline-block;"> <b>Stream Type</b> </div>	<div style="border: 1px solid black; padding: 5px; display: inline-block; background-color: yellow;"> <b>E6</b> </div>	<div style="border: 1px solid black; padding: 5px; display: inline-block;"> <b>See Classification Key (Figure 2-21)</b> </div>
---	--	--

**Worksheet 2-4.** Morphological relations, including dimensionless ratios of river reach sites (Rosgen, 2006b; Rosgen and Silvey 2007).

Stream: <b>Sheyenne River-4-22.27</b>		Location: <b>Sheyenne River-4-22.27</b>								
Observers: <b>KP, AL</b>		Date: <b>10/1/2011</b>		Valley Type: <b>X</b>		Stream Type: <b>E6</b>				
<b>River Reach Summary Data</b>										
<b>Channel Dimension</b>	Mean Riffle Depth ( $d_{bkt}$ )	<b>8.6</b>	ft	Riffle Width ( $W_{bkt}$ )	<b>71.5</b>	ft	Riffle Area ( $A_{bkt}$ )	<b>571.8</b>	ft <sup>2</sup>	
	Mean Pool Depth ( $d_{bkfp}$ )		ft	Pool Width ( $W_{bkfp}$ )		ft	Pool Area ( $A_{bkfp}$ )		ft <sup>2</sup>	
	Mean Pool Depth/Mean Riffle Depth		$d_{bkfp}/d_{bkt}$	Pool Width/Riffle Width		$W_{bkfp}/W_{bkt}$	Pool Area / Riffle Area		$A_{bkfp}/A_{bkt}$	
	Max Riffle Depth ( $d_{maxrif}$ )	<b>12.8</b>	ft	Max Pool Depth ( $d_{maxp}$ )		ft	Max Riffle Depth/Mean Riffle Depth	<b>1.5</b>		
	Max Pool Depth/Mean Riffle Depth			Point Bar Slope		ft/ft	Inner Berm Width ( $W_{ib}$ )		ft	
	Inner Berm Depth ( $d_{ib}$ )		ft	Inner Berm Width/Depth Ratio			$W_{ib}/d_{ib}$	Inner Berm Area ( $A_{ib}$ )		ft <sup>2</sup>
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )				<b>1.8</b>	ft/s	Estimation Method		<b>HEC-RAS</b>	
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )				<b>1030</b>	cfs	Drainage Area		<b>3483</b>	mi <sup>2</sup>

<b>Channel Pattern</b>	Geometry			Dimensionless Geometry Ratios			
	Mean	Min	Max	Mean	Min	Max	
	Meander Wavelength ( $L_m$ )	<b>923</b>			ft	Meander Length Ratio ( $L_m/W_{bkt}$ )	<b>12.9</b>
	Radius of Curvature ( $R_c$ )	<b>178</b>			ft	Radius of Curvature/Riffle Width ( $R_c/W_{bkt}$ )	<b>2.5</b>
	Belt Width ( $W_{bit}$ )	<b>1243</b>			ft	Meander Width Ratio ( $W_{bit}/W_{bkt}$ )	<b>17.4</b>
	Individual Pool Length				ft	Pool Length/Riffle Width	
	Pool to Pool Spacing				ft	Pool to Pool Spacing/Riffle Width	
Riffle Length				ft	Riffle Length/Riffle Width		

<b>Channel Profile</b>	Valley Slope (VS)		ft/ft	Average Water Surface Slope (S)		ft/ft	Sinuosity (VS/S)		
	Stream Length (SL)	<b>23284</b>	ft	Valley Length (VL)	<b>13295</b>	ft	Sinuosity (SL/VL)	<b>1.8</b>	
	Low Bank Height (LBH)	start	ft	Max Riffle Depth	start	ft	Bank-Height Ratio (BHR)	start	
		end	ft		end	ft	(LBH/Max Riffle Depth)	end	
	Facet Slopes			Dimensionless Slope Ratios			Mean	Min	Max
	Riffle Slope ( $S_{rif}$ )	<b>0.0</b>		ft/ft	Riffle Slope/Average Water Surface Slope ( $S_{rif}/S$ )	<b>1.0</b>			
	Run Slope ( $S_{run}$ )			ft/ft	Run Slope/Average Water Surface Slope ( $S_{run}/S$ )				
	Pool Slope ( $S_p$ )			ft/ft	Pool Slope/Average Water Surface Slope ( $S_p/S$ )				
	Glide Slope ( $S_g$ )			ft/ft	Glide Slope/Average Water Surface Slope ( $S_g/S$ )				
	Feature Midpoint <sup>a</sup>			Dimensionless Depth Ratios			Mean	Min	Max
	Max Riffle Depth ( $d_{maxrif}$ )	<b>12.8</b>		ft	Max Riffle Depth/Mean Riffle Depth ( $d_{maxrif}/d_{bkt}$ )	<b>1.5</b>			
	Max Run Depth ( $d_{maxrun}$ )			ft	Max Run Depth/Mean Riffle Depth ( $d_{maxrun}/d_{bkt}$ )				
	Max Pool Depth ( $d_{maxp}$ )			ft	Max Pool Depth/Mean Riffle Depth ( $d_{maxp}/d_{bkt}$ )				
Max Glide Depth ( $d_{maxg}$ )			ft	Max Glide Depth/Mean Riffle Depth ( $d_{maxg}/d_{bkt}$ )					

<b>Channel Materials</b>	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Protrusion Height <sup>d</sup>	
	% Silt/Clay	<b>54</b>			$D_{16}$	<b>0.0029</b>		mm
	% Sand	<b>46</b>			$D_{35}$	<b>0.045</b>		mm
	% Gravel	<b>0</b>			$D_{50}$	<b>0.073</b>		mm
	% Cobble	<b>0</b>			$D_{84}$	<b>0.132</b>		mm
	% Boulder	<b>0</b>			$D_{95}$	<b>0.16</b>		mm
	% Bedrock	<b>0</b>			$D_{100}$	<b>4.75</b>		mm

<sup>a</sup> Min, max, mean depths are ave. mid-point values except pools: taken at deepest part of pool.

<sup>b</sup> Composite sample of riffles and pools within the designated reach.

<sup>c</sup> Active bed of a riffle.

<sup>d</sup> Height of roughness feature above bed.

**Worksheet 2-1.** Gage station and field data (Rosgen and Silvey, 2007).

Summary.... <b>USGS GAGE STATION</b> Data/Records for <b>STREAM CHANNEL CLASSIFICATION</b>					
Station NAME:	Sheyenne River-3-18.15			Station Number:	N/A
LOCATION:	Sheyenne River-3-18.15				
Period of RECORD:	N/A	yrs	Mean Annual DISCHARGE:	N/A	cfs
Drainage AREA:	3179520	acres	4968	mi <sup>2</sup>	Drainage Area Mn ELEV: 867.44 ft
Reference REACH SLOPE:		ft/ft	Valley Type:	X	
Stream Type:	E6		HUC:	-- -- -- -- -- -- -- -- -- --	
"BANKFULL" CHARACTERISTICS					
Determined from FIELD MEASUREMENT			Determined from GAGE DATA Analysis		
Bankfull WIDTH ( $W_{bkf}$ )	93.8	ft	Bankfull WIDTH ( $W_{bkf}$ )		ft
Bankfull Mean DEPTH ( $d_{bkf}$ )	9.4	ft	Bankfull MEAN DEPTH ( $d_{bkf}$ )		ft
Bankfull Xsec AREA ( $A_{bkf}$ )	881.1	ft <sup>2</sup>	Bankfull Xsec AREA ( $A_{bkf}$ )		ft <sup>2</sup>
Wetted PERIMETER ( $W_p$ )	100.3	ft	Wetted PERIMETER ( $W_p$ )		ft
Bankfull STAGE (Gage Ht)		ft	Bankfull STAGE (Gage Ht)		ft
Est. Mean VELOCITY ( $u$ )	1.9	ft/sec	Mean VELOCITY ( $u$ )		ft/sec
Est. Bkf. DISCHARGE ( $Q_{bkf}$ )	1680.0	cfs	Bankfull DISCHARGE ( $Q_{bkf}$ )		cfs
Bankfull DISCHARGE associated with "field-determined" Bankfull STAGE				1680.0	cfs
Recurrence Interval ( Log-Pearson ) associated with "field-determined" Bankfull Discharge				1.4	yrs
From the Annual Peak Flow Frequency Analysis data for the Gage Station, determine:					
1.5 Year R.I. Discharge..... =	N/A	cfs	10 Year R.I. Discharge..... =	N/A	cfs
2.0 Year R.I. Discharge..... =	N/A	cfs	25 Year R.I. Discharge..... =	N/A	cfs
5.0 Year R.I. Discharge..... =	N/A	cfs	50 Year R.I. Discharge..... =	N/A	cfs
MEANDER GEOMETRY					
Meander Length ( $L_m$ )	1538	ft	Radius of Curvature ( $R_C$ )	246.0	ft
Belt Width ( $W_{blt}$ )	1749	ft	Meander Width Ratio ( $W_{blt}/W_{bkf}$ )	18.6	ft/ft
HYDRAULIC GEOMETRY					
Based on USGS Discharge Summary Notes data ( Form 9-207 ) and regression analyses of measured discharge ( $Q$ ) with the hydraulic parameters of Width ( $W$ ), Area ( $A$ ), Mean Depth ( $d$ ) & Mean Velocity ( $u$ ), determine the <i>intercept coefficient</i> ( $a$ ) and the <i>slope exponent</i> ( $b$ ) values for a power function of the form $Y = aX^b$ , when $Y$ is one of the selected hydraulic parameters and $X$ is a given discharge value ( $Q$ ).					
	Width ( $W$ )	Depth ( $d$ )	Area ( $A$ )	Velocity ( $u$ )	
Intercept Coefficient: ( $a$ )					
Slope Exponent: ( $b$ )					
Hydraulic Radius: $R = A / W_p$		ft	Manning's "n" at Bankfull Stage	0.048	Coeff.
$"n" = 1.4865 [ ( Area ) ( Hydraulic Radius^{2/3} ) ( Slope^{1/2} ) ] / Q_{bkf}$					

**Worksheet 2-2.** Computations of velocity and bankfull discharge using various methods (Rosgen, 2006b; Rosgen and Silvey, 2007).

Bankfull VELOCITY / DISCHARGE Estimates									
Site	Sheyenne River-3-18.15			Location	Sheyenne River-3-18.15				
Date	9/30/2011	Stream Type	E6	Valley Type	X				
Observers	KD, JB			HUC	-- -- -- -- -- -- -- -- -- --				
INPUT VARIABLES				OUTPUT VARIABLES					
Bankfull Cross-sectional	881.1	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Mean DEPTH	9.4	$D_{bkf}$ (ft)				
Bankfull WIDTH	93.8	$W_{bkf}$ (ft)	Wetted PERIMETER ~ 2 * $d_{bkf}$ + $W_{bkf}$	112.6	$W_p$ (ft)				
$D_{84}$ @ Riffle	0.1	Dia. (mm)	$D_{84}$ mm / 304.8 =	0.00	$D_{84}$ (ft)				
Bankfull SLOPE	0.0002	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	7.8	R (ft)				
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R (ft) / $D_{84}$ (ft)	18340					
Drainage AREA	4968.0	DA (mi <sup>2</sup> )	Shear Velocity	0.2	$u^*$ (ft / sec)				
ESTIMATION METHODS				Bankfull VELOCITY		Bankfull DISCHARGE			
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 \text{Log}\{ R / D_{84} \} ] u^*$				6.4	ft / sec	5644	cfs		
2. Roughness Coefficient: a) Manning's 'n' from friction factor / relative roughness (Figs. 2-18, 19) $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text"/>				1.8	ft / sec	1610	cfs		
2. Roughness Coefficient: b) Manning's 'n' from Jarrett ( USGS ): $n = 0.39 S^{-.38} R^{-.16}$ n = <input type="text"/>				7.6	ft / sec	6709	cfs		
Note: This equation is for applications involving steep, step-pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for stream types A1, A2, A3, B1, B2, B3, C2 and E3.									
2. Roughness Coefficient: c) Manning's 'n' from Stream Type $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text" value="0.048"/>				1.8	ft / sec	1610	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.) HEC-RAS				1.9	ft / sec	1680	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.)					ft / sec		cfs		
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge Q = <input type="text" value="1.46"/> Yr. $u = Q / A$					ft / sec		cfs		
4. Continuity Equations: b) USGS Gage Data $u = Q / A$					ft / sec		cfs		
Options for using the $D_{84}$ term in the relative roughness relation ( $R/D_{84}$ ), when using estimation method 1.									
Option 1. For sand-bed channels: Measure the "protrusion height" ( $h_{sd}$ ) of sand dunes above channel bed elevations. Substitute an average sand dune protrusion height ( $h_{sd}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 2. For boulder-dominated channels: Measure several "protrusion heights" ( $h_{bo}$ ) of boulders above channel bed elevations. Substitute an ave. boulder protrusion height ( $h_{bo}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 3. For bedrock-dominated channels: Measure several "protrusion heights" ( $h_{br}$ ) of rock separations/steps/joints/uplifted surfaces above channel bed elevations. Substitute an average bedrock protrusion height ( $h_{br}$ in feet) for the $D_{84}$ term in estimation method 1.									

**Worksheet 2-3.** Field form for Level II stream classification (Rosgen, 1996; Rosgen , 2006b).

Stream: <b>Sheyenne River-3-18.15</b>	
Basin: <b>Red River Basin</b>	Drainage Area: <b>3E+06</b> acres <b>4968</b> mi <sup>2</sup>
Location: <b>Sheyenne River-3-18.15</b>	
Twp.&Rge: - Sec.&Qtr.: -	
Cross-Section Monuments (Lat./Long.): - Date: <b>9/30/2011</b>	
Observers: <b>KD, JB</b> Valley Type: <b>X</b>	

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>93.8</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>9.4</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>881.1</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>10.0</b>	ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>12.9</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>534.7</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>5.7</b>	ft/ft
<b>Channel Materials (Particle Size Index ) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>0.73</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.00022</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).	<b>1.9</b>	

<div style="border: 1px solid black; padding: 5px; display: inline-block;"> <b>Stream Type</b> </div>	<div style="border: 1px solid black; padding: 5px; display: inline-block; background-color: yellow;"> <b>E6</b> </div>	<div style="border: 1px solid black; padding: 5px; display: inline-block;"> <b>See Classification Key (Figure 2-21)</b> </div>
---	--	--

**Worksheet 2-4.** Morphological relations, including dimensionless ratios of river reach sites (Rosgen, 2006b; Rosgen and Silvey 2007).

Stream: <b>Sheyenne River-3-18.15</b>		Location: <b>Sheyenne River-3-18.15</b>								
Observers: <b>KD, JB</b>		Date: <b>9/30/2011</b>		Valley Type: <b>X</b>		Stream Type: <b>E6</b>				
<b>River Reach Summary Data</b>										
<b>Channel Dimension</b>	Mean Riffle Depth ( $d_{bkt}$ )	<b>9.4</b>	ft	Riffle Width ( $W_{bkt}$ )	<b>93.8</b>	ft	Riffle Area ( $A_{bkt}$ )	<b>881.1</b>	ft <sup>2</sup>	
	Mean Pool Depth ( $d_{bkfp}$ )		ft	Pool Width ( $W_{bkfp}$ )		ft	Pool Area ( $A_{bkfp}$ )		ft <sup>2</sup>	
	Mean Pool Depth/Mean Riffle Depth		$d_{bkfp}/d_{bkt}$	Pool Width/Riffle Width		$W_{bkfp}/W_{bkt}$	Pool Area / Riffle Area		$A_{bkfp}/A_{bkt}$	
	Max Riffle Depth ( $d_{maxrif}$ )	<b>12.9</b>	ft	Max Pool Depth ( $d_{maxp}$ )		ft	Max Riffle Depth/Mean Riffle Depth	<b>1.4</b>		
	Max Pool Depth/Mean Riffle Depth			Point Bar Slope		ft/ft	Inner Berm Width ( $W_{ib}$ )		ft	
	Inner Berm Depth ( $d_{ib}$ )		ft	Inner Berm Width/Depth Ratio			$W_{ib}/d_{ib}$	Inner Berm Area ( $A_{ib}$ )		ft <sup>2</sup>
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )				<b>1.9</b>	ft/s	Estimation Method		<b>HEC-RAS</b>	
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )				<b>1680</b>	cfs	Drainage Area		<b>4968</b>	mi <sup>2</sup>

<b>Channel Pattern</b>	Geometry			Dimensionless Geometry Ratios			
	Mean	Min	Max	Mean	Min	Max	
	Meander Wavelength ( $L_m$ )	<b>1538</b>			ft	Meander Length Ratio ( $L_m/W_{bkt}$ )	<b>16.4</b>
	Radius of Curvature ( $R_c$ )	<b>246</b>			ft	Radius of Curvature/Riffle Width ( $R_c/W_{bkt}$ )	<b>2.6</b>
	Belt Width ( $W_{bit}$ )	<b>1749</b>			ft	Meander Width Ratio ( $W_{bit}/W_{bkt}$ )	<b>18.6</b>
	Individual Pool Length				ft	Pool Length/Riffle Width	
	Pool to Pool Spacing				ft	Pool to Pool Spacing/Riffle Width	
Riffle Length				ft	Riffle Length/Riffle Width		

<b>Channel Profile</b>	Valley Slope (VS)		ft/ft	Average Water Surface Slope (S)		ft/ft	Sinuosity (VS/S)		
	Stream Length (SL)	<b>34110</b>	ft	Valley Length (VL)	<b>18101</b>	ft	Sinuosity (SL/VL)	<b>1.9</b>	
	Low Bank Height (LBH)	start: _____ end: _____	ft	Max Riffle Depth	start: _____ end: _____	ft	Bank-Height Ratio (BHR) (LBH/Max Riffle Depth)	start: _____ end: _____	
	Facet Slopes			Dimensionless Slope Ratios			Mean	Min	Max
	Riffle Slope ( $S_{rif}$ )	<b>0.0</b>		ft/ft	Riffle Slope/Average Water Surface Slope ( $S_{rif} / S$ )	<b>1.0</b>			
	Run Slope ( $S_{run}$ )			ft/ft	Run Slope/Average Water Surface Slope ( $S_{run} / S$ )				
	Pool Slope ( $S_p$ )			ft/ft	Pool Slope/Average Water Surface Slope ( $S_p / S$ )				
	Glide Slope ( $S_g$ )			ft/ft	Glide Slope/Average Water Surface Slope ( $S_g / S$ )				
	Feature Midpoint <sup>a</sup>			Dimensionless Depth Ratios			Mean	Min	Max
	Max Riffle Depth ( $d_{maxrif}$ )	<b>12.9</b>		ft	Max Riffle Depth/Mean Riffle Depth ( $d_{maxrif} / d_{bkt}$ )	<b>1.4</b>			
	Max Run Depth ( $d_{maxrun}$ )			ft	Max Run Depth/Mean Riffle Depth ( $d_{maxrun} / d_{bkt}$ )				
	Max Pool Depth ( $d_{maxp}$ )			ft	Max Pool Depth/Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )				
	Max Glide Depth ( $d_{maxg}$ )			ft	Max Glide Depth/Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )				

<b>Channel Materials</b>	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Protrusion Height <sup>d</sup>	
	% Silt/Clay	<b>56</b>			$D_{16}$	<b>&lt;.001</b>		mm
	% Sand	<b>44</b>			$D_{35}$	<b>0.035</b>		mm
	% Gravel	<b>0</b>			$D_{50}$	<b>0.73</b>		mm
	% Cobble	<b>0</b>			$D_{84}$	<b>0.13</b>		mm
	% Boulder	<b>0</b>			$D_{95}$	<b>0.155</b>		mm
	% Bedrock	<b>0</b>			$D_{100}$	<b>0.3</b>		mm

<sup>a</sup> Min, max, mean depths are ave. mid-point values except pools: taken at deepest part of pool.

<sup>b</sup> Composite sample of riffles and pools within the designated reach.

<sup>c</sup> Active bed of a riffle.

<sup>d</sup> Height of roughness feature above bed.

**Worksheet 2-1.** Gage station and field data (Rosgen and Silvey, 2007).

Summary.... <b>USGS GAGE STATION</b> Data/Records for <b>STREAM CHANNEL CLASSIFICATION</b>					
Station NAME:	Sheyenne River-2-11.56			Station Number:	N/A
LOCATION:	Sheyenne River-2-11.56				
Period of RECORD:	N/A	yrs	Mean Annual DISCHARGE:	N/A	cfs
Drainage AREA:	3255040	acres	5086	mi <sup>2</sup>	Drainage Area Mn ELEV: 862.08 ft
Reference REACH SLOPE:		ft/ft	Valley Type:	X	
Stream Type:	E5		HUC:	_ _ _ _ _	
"BANKFULL" CHARACTERISTICS					
Determined from FIELD MEASUREMENT			Determined from GAGE DATA Analysis		
Bankfull WIDTH ( $W_{bkf}$ )	111.5	ft	Bankfull WIDTH ( $W_{bkf}$ )		ft
Bankfull Mean DEPTH ( $d_{bkf}$ )	8.8	ft	Bankfull MEAN DEPTH ( $d_{bkf}$ )		ft
Bankfull Xsec AREA ( $A_{bkf}$ )	988.1	ft <sup>2</sup>	Bankfull Xsec AREA ( $A_{bkf}$ )		ft <sup>2</sup>
Wetted PERIMETER ( $W_p$ )	116.6	ft	Wetted PERIMETER ( $W_p$ )		ft
Bankfull STAGE (Gage Ht)		ft	Bankfull STAGE (Gage Ht)		ft
Est. Mean VELOCITY ( $u$ )	1.8	ft/sec	Mean VELOCITY ( $u$ )		ft/sec
Est. Bkf. DISCHARGE ( $Q_{bkf}$ )	1750.0	cfs	Bankfull DISCHARGE ( $Q_{bkf}$ )		cfs
Bankfull DISCHARGE associated with "field-determined" Bankfull STAGE				1750.0	cfs
Recurrence Interval ( Log-Pearson ) associated with "field-determined" Bankfull Discharge				1.5	yrs
From the Annual Peak Flow Frequency Analysis data for the Gage Station, determine:					
1.5 Year R.I. Discharge..... =	N/A	cfs	10 Year R.I. Discharge..... =	N/A	cfs
2.0 Year R.I. Discharge.....=	N/A	cfs	25 Year R.I. Discharge.....=	N/A	cfs
5.0 Year R.I. Discharge.....=	N/A	cfs	50 Year R.I. Discharge..... =	N/A	cfs
MEANDER GEOMETRY					
Meander Length ( $L_m$ )	1474	ft	Radius of Curvature ( $R_C$ )	291.0	ft
Belt Width ( $W_{blt}$ )	1861	ft	Meander Width Ratio ( $W_{blt}/W_{bkf}$ )	16.7	ft/ft
HYDRAULIC GEOMETRY					
Based on USGS Discharge Summary Notes data ( Form 9-207 ) and regression analyses of measured discharge ( $Q$ ) with the hydraulic parameters of Width ( $W$ ), Area ( $A$ ), Mean Depth ( $d$ ) & Mean Velocity ( $u$ ), determine the <i>intercept coefficient</i> ( $a$ ) and the <i>slope exponent</i> ( $b$ ) values for a power function of the form $Y = aX^b$ , when $Y$ is one of the selected hydraulic parameters and $X$ is a given discharge value ( $Q$ ).					
	Width ( $W$ )	Depth ( $d$ )	Area ( $A$ )	Velocity ( $u$ )	
Intercept Coefficient: ( $a$ )					
Slope Exponent: ( $b$ )					
Hydraulic Radius: $R = A / W_p$		ft	Manning's "n" at Bankfull Stage	0.048	Coeff.
$"n" = 1.4865 [ ( Area ) ( Hydraulic Radius^{2/3} ) ( Slope^{1/2} ) ] / Q_{bkf}$					

**Worksheet 2-2.** Computations of velocity and bankfull discharge using various methods (Rosgen, 2006b; Rosgen and Silvey, 2007).

Bankfull VELOCITY / DISCHARGE Estimates									
Site	Sheyenne River-2-11.56			Location	Sheyenne River-2-11.56				
Date	10/3/2011	Stream Type	E5	Valley Type	X				
Observers	KP, AL			HUC	-- -- -- -- -- -- -- -- -- --				
INPUT VARIABLES				OUTPUT VARIABLES					
Bankfull Cross-sectional	988.1	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Mean DEPTH	8.8	$D_{bkf}$ (ft)				
Bankfull WIDTH	111.5	$W_{bkf}$ (ft)	Wetted PERIMETER ~ $2 * d_{bkf} + W_{bkf}$	129.2	$W_p$ (ft)				
$D_{84}$ @ Riffle	1.8	Dia. (mm)	$D_{84}$ mm / 304.8 =	0.01	$D_{84}$ (ft)				
Bankfull SLOPE	0.0002	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	7.7	R (ft)				
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R (ft) / $D_{84}$ (ft)	1318					
Drainage AREA	5086.0	DA (mi <sup>2</sup> )	Shear Velocity $u^* = \sqrt{gRS}$	0.2	$u^*$ (ft / sec)				
ESTIMATION METHODS				Bankfull VELOCITY		Bankfull DISCHARGE			
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 \text{Log}\{ R / D_{84} \} ] u^*$				4.1	ft / sec	4032	cfs		
2. Roughness Coefficient: a) Manning's 'n' from friction factor / relative roughness (Figs. 2-18, 19) $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text"/>				1.5	ft / sec	1508	cfs		
2. Roughness Coefficient: b) Manning's 'n' from Jarrett ( USGS ): $n = 0.39S^{-.38}R^{-.16}$ n = <input type="text"/> Note: This equation is for applications involving steep, step-pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for stream types A1, A2, A3, B1, B2, B3, C2 and E3.				7.2	ft / sec	7100	cfs		
2. Roughness Coefficient: c) Manning's 'n' from Stream Type $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text" value="0.048"/>				1.5	ft / sec	1508	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.) HEC-RAS				1.8	ft / sec	1750	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.)					ft / sec		cfs		
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge Q = <input type="text" value="1.46"/> Yr. $u = Q / A$					ft / sec		cfs		
4. Continuity Equations: b) USGS Gage Data $u = Q / A$					ft / sec		cfs		
Options for using the $D_{84}$ term in the relative roughness relation ( $R/D_{84}$ ), when using estimation method 1.									
Option 1. For sand-bed channels: Measure the "protrusion height" ( $h_{sd}$ ) of sand dunes above channel bed elevations. Substitute an average sand dune protrusion height ( $h_{sd}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 2. For boulder-dominated channels: Measure several "protrusion heights" ( $h_{bo}$ ) of boulders above channel bed elevations. Substitute an ave. boulder protrusion height ( $h_{bo}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 3. For bedrock-dominated channels: Measure several "protrusion heights" ( $h_{br}$ ) of rock separations/steps/joints/uplifted surfaces above channel bed elevations. Substitute an average bedrock protrusion height ( $h_{br}$ in feet) for the $D_{84}$ term in estimation method 1.									

**Worksheet 2-3.** Field form for Level II stream classification (Rosgen, 1996; Rosgen , 2006b).

Stream: <b>Sheyenne River-2-11.56</b>	
Basin: <b>Red River Basin</b>	Drainage Area: <b>3E+06</b> acres <b>5086</b> mi <sup>2</sup>
Location: <b>Sheyenne River-2-11.56</b>	
Twp.&Rge: - Sec.&Qtr.: -	
Cross-Section Monuments (Lat./Long.): - Date: <b>10/3/2011</b>	
Observers: <b>KP, AL</b> Valley Type: <b>X</b>	

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>111.5</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>8.8</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>988.1</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>12.6</b>	ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>13.0</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>787.7</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>7.1</b>	ft/ft
<b>Channel Materials (Particle Size Index ) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>0.51</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.00016</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).	<b>1.5</b>	

<b>Stream Type</b>	<b>E5</b>	<b>See Classification Key (Figure 2-21)</b>
--------------------	-----------	---

**Worksheet 2-4.** Morphological relations, including dimensionless ratios of river reach sites (Rosgen, 2006b; Rosgen and Silvey 2007).

Stream: <b>Sheyenne River-2-11.56</b>		Location: <b>Sheyenne River-2-11.56</b>								
Observers: <b>KP, AL</b>		Date: <b>10/3/2011</b>		Valley Type: <b>X</b>		Stream Type: <b>E5</b>				
<b>River Reach Summary Data</b>										
<b>Channel Dimension</b>	Mean Riffle Depth ( $d_{bkt}$ )	<b>8.8</b>	ft	Riffle Width ( $W_{bkt}$ )	<b>111.5</b>	ft	Riffle Area ( $A_{bkt}$ )	<b>988.1</b>	ft <sup>2</sup>	
	Mean Pool Depth ( $d_{bkfp}$ )		ft	Pool Width ( $W_{bkfp}$ )		ft	Pool Area ( $A_{bkfp}$ )		ft <sup>2</sup>	
	Mean Pool Depth/Mean Riffle Depth		$d_{bkfp}/d_{bkt}$	Pool Width/Riffle Width		$W_{bkfp}/W_{bkt}$	Pool Area / Riffle Area		$A_{bkfp}/A_{bkt}$	
	Max Riffle Depth ( $d_{maxrif}$ )	<b>13</b>	ft	Max Pool Depth ( $d_{maxp}$ )		ft	Max Riffle Depth/Mean Riffle Depth	<b>1.5</b>		
	Max Pool Depth/Mean Riffle Depth			Point Bar Slope		ft/ft	Inner Berm Width ( $W_{ib}$ )		ft	
	Inner Berm Depth ( $d_{ib}$ )		ft	Inner Berm Width/Depth Ratio			$W_{ib}/d_{ib}$	Inner Berm Area ( $A_{ib}$ )		ft <sup>2</sup>
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )				<b>1.8</b>	ft/s	Estimation Method		<b>HEC-RAS</b>	
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )				<b>1750</b>	cfs	Drainage Area		<b>5086</b>	mi <sup>2</sup>

<b>Channel Pattern</b>	Geometry			Dimensionless Geometry Ratios			
	Mean	Min	Max	Mean	Min	Max	
	Meander Wavelength ( $L_m$ )	<b>1474</b>			ft	Meander Length Ratio ( $L_m/W_{bkt}$ )	<b>13.2</b>
	Radius of Curvature ( $R_c$ )	<b>291</b>			ft	Radius of Curvature/Riffle Width ( $R_c/W_{bkt}$ )	<b>2.6</b>
	Belt Width ( $W_{bit}$ )	<b>1861</b>			ft	Meander Width Ratio ( $W_{bit}/W_{bkt}$ )	<b>16.7</b>
	Individual Pool Length				ft	Pool Length/Riffle Width	
	Pool to Pool Spacing				ft	Pool to Pool Spacing/Riffle Width	
Riffle Length				ft	Riffle Length/Riffle Width		

<b>Channel Profile</b>	Valley Slope (VS)		ft/ft	Average Water Surface Slope (S)		ft/ft	Sinuosity (VS/S)		
	Stream Length (SL)	<b>8966</b>	ft	Valley Length (VL)	<b>6195</b>	ft	Sinuosity (SL/VL)	<b>1.4</b>	
	Low Bank Height (LBH)	start: _____ end: _____	ft	Max Riffle Depth	start: _____ end: _____	ft	Bank-Height Ratio (BHR) (LBH/Max Riffle Depth)	start: _____ end: _____	
	Facet Slopes			Dimensionless Slope Ratios			Mean	Min	Max
	Riffle Slope ( $S_{rif}$ )	<b>0.0</b>		ft/ft	Riffle Slope/Average Water Surface Slope ( $S_{rif} / S$ )	<b>1.0</b>			
	Run Slope ( $S_{run}$ )			ft/ft	Run Slope/Average Water Surface Slope ( $S_{run} / S$ )				
	Pool Slope ( $S_p$ )			ft/ft	Pool Slope/Average Water Surface Slope ( $S_p / S$ )				
	Glide Slope ( $S_g$ )			ft/ft	Glide Slope/Average Water Surface Slope ( $S_g / S$ )				
	Feature Midpoint <sup>a</sup>			Dimensionless Depth Ratios			Mean	Min	Max
	Max Riffle Depth ( $d_{maxrif}$ )	<b>13.0</b>		ft	Max Riffle Depth/Mean Riffle Depth ( $d_{maxrif} / d_{bkt}$ )	<b>1.5</b>			
	Max Run Depth ( $d_{maxrun}$ )			ft	Max Run Depth/Mean Riffle Depth ( $d_{maxrun} / d_{bkt}$ )				
	Max Pool Depth ( $d_{maxp}$ )			ft	Max Pool Depth/Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )				
	Max Glide Depth ( $d_{maxg}$ )			ft	Max Glide Depth/Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )				

<b>Channel Materials</b>	Reach <sup>b</sup>		Riffle <sup>c</sup>	Bar	Reach <sup>b</sup>		Riffle <sup>c</sup>	Bar	Protrusion Height <sup>d</sup>	
	% Silt/Clay	<b>26</b>			$D_{16}$	<b>0.016</b>				mm
	% Sand	<b>72</b>			$D_{35}$	<b>0.16</b>				mm
	% Gravel	<b>2</b>			$D_{50}$	<b>0.51</b>				mm
	% Cobble	<b>0</b>			$D_{84}$	<b>1.77</b>				mm
	% Boulder	<b>0</b>			$D_{95}$	<b>3.4</b>				mm
	% Bedrock	<b>0</b>			$D_{100}$	<b>9.5</b>				mm

<sup>a</sup> Min, max, mean depths are ave. mid-point values except pools: taken at deepest part of pool.

<sup>b</sup> Composite sample of riffles and pools within the designated reach.

<sup>c</sup> Active bed of a riffle.

<sup>d</sup> Height of roughness feature above bed.

**Worksheet 2-1.** Gage station and field data (Rosgen and Silvey, 2007).

Summary.... <b>USGS GAGE STATION</b> Data/Records for <b>STREAM CHANNEL CLASSIFICATION</b>					
Station NAME:	Sheyenne River-1-4.20			Station Number:	N/A
LOCATION:	Sheyenne River-1-4.20				
Period of RECORD:	N/A yrs		Mean Annual DISCHARGE:	N/A cfs	
Drainage AREA:	3359360 acres	5249 mi <sup>2</sup>	Drainage Area Mn ELEV:	851.8 ft	
Reference REACH SLOPE:	ft/ft		Valley Type:	X	
Stream Type:	E6		HUC:	-----	
"BANKFULL" CHARACTERISTICS					
Determined from FIELD MEASUREMENT			Determined from GAGE DATA Analysis		
Bankfull WIDTH ( $W_{bkf}$ )	86.9	ft	Bankfull WIDTH ( $W_{bkf}$ )		ft
Bankfull Mean DEPTH ( $d_{bkf}$ )	9.4	ft	Bankfull MEAN DEPTH ( $d_{bkf}$ )		ft
Bankfull Xsec AREA ( $A_{bkf}$ )	820.3	ft <sup>2</sup>	Bankfull Xsec AREA ( $A_{bkf}$ )		ft <sup>2</sup>
Wetted PERIMETER ( $W_p$ )	93.2	ft	Wetted PERIMETER ( $W_p$ )		ft
Bankfull STAGE (Gage Ht)		ft	Bankfull STAGE (Gage Ht)		ft
Est. Mean VELOCITY ( $u$ )	2.3	ft/sec	Mean VELOCITY ( $u$ )		ft/sec
Est. Bkf. DISCHARGE ( $Q_{bkf}$ )	1900.0	cfs	Bankfull DISCHARGE ( $Q_{bkf}$ )		cfs
Bankfull DISCHARGE associated with "field-determined" Bankfull STAGE				1900.0	cfs
Recurrence Interval ( Log-Pearson ) associated with "field-determined" Bankfull Discharge				1.5	yrs
From the Annual Peak Flow Frequency Analysis data for the Gage Station, determine:					
1.5 Year R.I. Discharge..... =	N/A	cfs	10 Year R.I. Discharge..... =	N/A	cfs
2.0 Year R.I. Discharge..... =	N/A	cfs	25 Year R.I. Discharge..... =	N/A	cfs
5.0 Year R.I. Discharge..... =	N/A	cfs	50 Year R.I. Discharge..... =	N/A	cfs
MEANDER GEOMETRY					
Meander Length ( $L_m$ )	1238	ft	Radius of Curvature ( $R_C$ )	283.0	ft
Belt Width ( $W_{blt}$ )	2100	ft	Meander Width Ratio ( $W_{blt}/W_{bkf}$ )	24.2	ft/ft
HYDRAULIC GEOMETRY					
Based on <i>USGS Discharge Summary Notes</i> data ( Form 9-207 ) and regression analyses of measured discharge ( $Q$ ) with the hydraulic parameters of Width ( $W$ ), Area ( $A$ ), Mean Depth ( $d$ ) & Mean Velocity ( $u$ ), determine the <i>intercept coefficient</i> ( $a$ ) and the <i>slope exponent</i> ( $b$ ) values for a power function of the form $Y = aX^b$ , when $Y$ is one of the selected hydraulic parameters and $X$ is a given discharge value ( $Q$ ).					
	Width ( $W$ )	Depth ( $d$ )	Area ( $A$ )	Velocity ( $u$ )	
Intercept Coefficient: ( $a$ )					
Slope Exponent: ( $b$ )					
Hydraulic Radius: $R = A / W_p$		ft	Manning's "n" at Bankfull Stage	0.036	Coeff.
$"n" = 1.4865 [ ( Area ) ( Hydraulic Radius^{2/3} ) ( Slope^{1/2} ) ] / Q_{bkf}$					

**Worksheet 2-2.** Computations of velocity and bankfull discharge using various methods (Rosgen, 2006b; Rosgen and Silvey, 2007).

Bankfull VELOCITY / DISCHARGE Estimates									
Site	Sheyenne River-1-4.20			Location	Sheyenne River-1-4.20				
Date	10/6/2011	Stream Type	E6	Valley Type	X				
Observers	KP, AL			HUC	-- -- -- -- -- -- -- -- -- --				
INPUT VARIABLES				OUTPUT VARIABLES					
Bankfull Cross-sectional	820.3	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Mean DEPTH	9.4	$D_{bkf}$ (ft)				
Bankfull WIDTH	86.9	$W_{bkf}$ (ft)	Wetted PERIMETER $\sim 2 * d_{bkf} + W_{bkf}$	105.8	$W_p$ (ft)				
$D_{84}$ @ Riffle	0.15	Dia. (mm)	$D_{84}$ mm / 304.8 =	0.00	$D_{84}$ (ft)				
Bankfull SLOPE	0.0002	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	7.8	R (ft)				
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R (ft) / $D_{84}$ (ft)	15763					
Drainage AREA	5249.0	DA (mi <sup>2</sup> )	Shear Velocity $u^* = \sqrt{gRS}$	0.2	$u^*$ (ft / sec)				
ESTIMATION METHODS				Bankfull VELOCITY		Bankfull DISCHARGE			
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 \text{Log}\{ R / D_{84} \} ] u^*$				5.5	ft / sec	4476	cfs		
2. Roughness Coefficient: a) Manning's 'n' from friction factor / relative roughness (Figs. 2-18, 19) $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text"/>				2.1	ft / sec	1724	cfs		
2. Roughness Coefficient: $u = 1.4865 * R^{2/3} * S^{1/2} / n$ b) Manning's 'n' from Jarrett ( USGS ): $n = 0.39S^{-.38}R^{-.16}$ n = <input type="text"/>				7.3	ft / sec	5995	cfs		
Note: This equation is for applications involving steep, step-pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for stream types A1, A2, A3, B1, B2, B3, C2 and E3.									
2. Roughness Coefficient: c) Manning's 'n' from Stream Type $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text" value="0.036"/>				2.1	ft / sec	1724	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.) HEC-RAS				2.3	ft / sec	1900	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.)					ft / sec		cfs		
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge Q = <input type="text" value="1.46"/> Yr. $u = Q / A$					ft / sec		cfs		
4. Continuity Equations: b) USGS Gage Data $u = Q / A$					ft / sec		cfs		
Options for using the $D_{84}$ term in the relative roughness relation ( $R/D_{84}$ ), when using estimation method 1.									
Option 1. For sand-bed channels: Measure the "protrusion height" ( $h_{sd}$ ) of sand dunes above channel bed elevations. Substitute an average sand dune protrusion height ( $h_{sd}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 2. For boulder-dominated channels: Measure several "protrusion heights" ( $h_{bo}$ ) of boulders above channel bed elevations. Substitute an ave. boulder protrusion height ( $h_{bo}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 3. For bedrock-dominated channels: Measure several "protrusion heights" ( $h_{br}$ ) of rock separations/steps/joints/uplifted surfaces above channel bed elevations. Substitute an average bedrock protrusion height ( $h_{br}$ in feet) for the $D_{84}$ term in estimation method 1.									

**Worksheet 2-3.** Field form for Level II stream classification (Rosgen, 1996; Rosgen, 2006b).

Stream: <b>Sheyenne River-1-4.20</b>	
Basin: <b>Red River Basin</b>	Drainage Area: <b>3E+06</b> acres <b>5249</b> mi <sup>2</sup>
Location: <b>Sheyenne River-1-4.20</b>	
Twp.&Rge: - Sec.&Qtr.: -	
Cross-Section Monuments (Lat./Long.): - Date: <b>10/6/2011</b>	
Observers: <b>KP, AL</b> Valley Type: <b>X</b>	

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>86.9</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>9.4</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>820.3</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>9.2</b>	ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>14.7</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>437.3</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>5.0</b>	ft/ft
<b>Channel Materials (Particle Size Index) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>0.175</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.00017</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).	<b>2.8</b>	

<div style="border: 1px solid black; padding: 5px; display: inline-block;"> <b>Stream Type</b> </div>	<div style="border: 1px solid black; padding: 5px; display: inline-block; background-color: yellow;"> <b>E6</b> </div>	<div style="border: 1px solid black; padding: 5px; display: inline-block;"> <b>See Classification Key (Figure 2-21)</b> </div>
---	--	--

**Worksheet 2-4.** Morphological relations, including dimensionless ratios of river reach sites (Rosgen, 2006b; Rosgen and Silvey 2007).

Stream: <b>Sheyenne River-1-4.20</b>		Location: <b>Sheyenne River-1-4.20</b>								
Observers: <b>KP, AL</b>		Date: <b>10/6/2011</b>		Valley Type: <b>X</b>		Stream Type: <b>E6</b>				
<b>River Reach Summary Data</b>										
<b>Channel Dimension</b>	Mean Riffle Depth ( $d_{bkt}$ )	<b>9.4</b>	ft	Riffle Width ( $W_{bkt}$ )	<b>86.9</b>	ft	Riffle Area ( $A_{bkt}$ )	<b>820.3</b>	ft <sup>2</sup>	
	Mean Pool Depth ( $d_{bkfp}$ )		ft	Pool Width ( $W_{bkfp}$ )		ft	Pool Area ( $A_{bkfp}$ )		ft <sup>2</sup>	
	Mean Pool Depth/Mean Riffle Depth		$d_{bkfp}/d_{bkt}$	Pool Width/Riffle Width		$W_{bkfp}/W_{bkt}$	Pool Area / Riffle Area		$A_{bkfp}/A_{bkt}$	
	Max Riffle Depth ( $d_{maxrif}$ )	<b>14.7</b>	ft	Max Pool Depth ( $d_{maxp}$ )		ft	Max Riffle Depth/Mean Riffle Depth	<b>1.6</b>		
	Max Pool Depth/Mean Riffle Depth			Point Bar Slope		ft/ft	Inner Berm Width ( $W_{ib}$ )		ft	
	Inner Berm Depth ( $d_{ib}$ )		ft	Inner Berm Width/Depth Ratio			$W_{ib}/d_{ib}$	Inner Berm Area ( $A_{ib}$ )		ft <sup>2</sup>
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )				<b>2.3</b>	ft/s	Estimation Method		<b>HEC-RAS</b>	
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )				<b>1900</b>	cfs	Drainage Area		<b>5249</b>	mi <sup>2</sup>

<b>Channel Pattern</b>	Geometry			Dimensionless Geometry Ratios			
	Mean	Min	Max	Mean	Min	Max	
	Meander Wavelength ( $L_m$ )	<b>1238</b>			ft	Meander Length Ratio ( $L_m/W_{bkt}$ )	<b>14.3</b>
	Radius of Curvature ( $R_c$ )	<b>283</b>			ft	Radius of Curvature/Riffle Width ( $R_c/W_{bkt}$ )	<b>3.3</b>
	Belt Width ( $W_{bit}$ )	<b>2100</b>			ft	Meander Width Ratio ( $W_{bit}/W_{bkt}$ )	<b>24.2</b>
	Individual Pool Length				ft	Pool Length/Riffle Width	
	Pool to Pool Spacing				ft	Pool to Pool Spacing/Riffle Width	
Riffle Length				ft	Riffle Length/Riffle Width		

<b>Channel Profile</b>	Valley Slope (VS)		ft/ft	Average Water Surface Slope (S)		ft/ft	Sinuosity (VS/S)		
	Stream Length (SL)	<b>59311</b>	ft	Valley Length (VL)	<b>21222</b>	ft	Sinuosity (SL/VL)	<b>2.8</b>	
	Low Bank Height (LBH)	start	ft	Max Riffle Depth	start	ft	Bank-Height Ratio (BHR) (LBH/Max Riffle Depth)	start	
		end	ft		end	ft		end	
	Facet Slopes			Dimensionless Slope Ratios			Mean Min Max		
	Riffle Slope ( $S_{rif}$ )	<b>0.0</b>		ft/ft	Riffle Slope/Average Water Surface Slope ( $S_{rif} / S$ )	<b>1.0</b>			
	Run Slope ( $S_{run}$ )			ft/ft	Run Slope/Average Water Surface Slope ( $S_{run} / S$ )				
	Pool Slope ( $S_p$ )			ft/ft	Pool Slope/Average Water Surface Slope ( $S_p / S$ )				
	Glide Slope ( $S_g$ )			ft/ft	Glide Slope/Average Water Surface Slope ( $S_g / S$ )				
	Feature Midpoint <sup>a</sup>			Dimensionless Depth Ratios			Mean Min Max		
	Max Riffle Depth ( $d_{maxrif}$ )	<b>14.7</b>		ft	Max Riffle Depth/Mean Riffle Depth ( $d_{maxrif} / d_{bkt}$ )	<b>1.6</b>			
	Max Run Depth ( $d_{maxrun}$ )			ft	Max Run Depth/Mean Riffle Depth ( $d_{maxrun} / d_{bkt}$ )				
	Max Pool Depth ( $d_{maxp}$ )			ft	Max Pool Depth/Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )				
Max Glide Depth ( $d_{maxg}$ )			ft	Max Glide Depth/Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )					

<b>Channel Materials</b>	Reach <sup>b</sup>			Riffle <sup>c</sup>			Bar			Protrusion Height <sup>d</sup>		
	% Silt/Clay	<b>71</b>			$D_{16}$	<b>&lt;.001</b>						mm
	% Sand	<b>28</b>			$D_{35}$	<b>0.0033</b>					mm	
	% Gravel	<b>1</b>			$D_{50}$	<b>0.175</b>					mm	
	% Cobble	<b>0</b>			$D_{84}$	<b>0.15</b>					mm	
	% Boulder	<b>0</b>			$D_{95}$	<b>0.22</b>					mm	
	% Bedrock	<b>0</b>			$D_{100}$	<b>9.5</b>					mm	

<sup>a</sup> Min, max, mean depths are ave. mid-point values except pools: taken at deepest part of pool.

<sup>b</sup> Composite sample of riffles and pools within the designated reach.

<sup>c</sup> Active bed of a riffle.

<sup>d</sup> Height of roughness feature above bed.

**Worksheet 2-1.** Gage station and field data (Rosgen and Silvey, 2007).

Summary.... <b>USGS GAGE STATION</b> Data/Records for <b>STREAM CHANNEL CLASSIFICATION</b>							
Station NAME:	Rush River-2-6.15			Station Number:	N/A		
LOCATION:	Rush River-2-6.15						
Period of RECORD:	N/A		yrs	Mean Annual DISCHARGE:	N/A		cfs
Drainage AREA:	89152	acres	139.3	mi <sup>2</sup>	Drainage Area Mn ELEV:	884.59	ft
Reference REACH SLOPE:			ft/ft	Valley Type:	X		
Stream Type:	E6		HUC: _____				
"BANKFULL" CHARACTERISTICS							
Determined from FIELD MEASUREMENT				Determined from GAGE DATA Analysis			
Bankfull WIDTH ( $W_{bkf}$ )	27.0	ft		Bankfull WIDTH ( $W_{bkf}$ )		ft	
Bankfull Mean DEPTH ( $d_{bkf}$ )	3.1	ft		Bankfull MEAN DEPTH ( $d_{bkf}$ )		ft	
Bankfull Xsec AREA ( $A_{bkf}$ )	84.4	ft <sup>2</sup>		Bankfull Xsec AREA ( $A_{bkf}$ )		ft <sup>2</sup>	
Wetted PERIMETER ( $W_p$ )	29.7	ft		Wetted PERIMETER ( $W_p$ )		ft	
Bankfull STAGE (Gage Ht)		ft		Bankfull STAGE (Gage Ht)		ft	
Est. Mean VELOCITY ( $u$ )	1.9	ft/sec		Mean VELOCITY ( $u$ )		ft/sec	
Est. Bkf. DISCHARGE ( $Q_{bkf}$ )	150.0	cfs		Bankfull DISCHARGE ( $Q_{bkf}$ )		cfs	
Bankfull DISCHARGE associated with "field-determined" Bankfull STAGE					150.0	cfs	
Recurrence Interval ( Log-Pearson ) associated with "field-determined" Bankfull Discharge					1.2	yrs	
From the Annual Peak Flow Frequency Analysis data for the Gage Station, determine:							
1.5 Year R.I. Discharge..... =	N/A	cfs		10 Year R.I. Discharge..... =	N/A	cfs	
2.0 Year R.I. Discharge..... =	N/A	cfs		25 Year R.I. Discharge..... =	N/A	cfs	
5.0 Year R.I. Discharge..... =	N/A	cfs		50 Year R.I. Discharge..... =	N/A	cfs	
MEANDER GEOMETRY							
Meander Length ( $L_m$ )	2344	ft		Radius of Curvature ( $R_C$ )	234.0	ft	
Belt Width ( $W_{blt}$ )	1408	ft		Meander Width Ratio ( $W_{blt}/W_{bkf}$ )	52.2	ft/ft	
HYDRAULIC GEOMETRY							
Based on <i>USGS Discharge Summary Notes</i> data ( Form 9-207 ) and regression analyses of measured discharge ( $Q$ ) with the hydraulic parameters of Width ( $W$ ), Area ( $A$ ), Mean Depth ( $d$ ) & Mean Velocity ( $u$ ), determine the <i>intercept coefficient</i> ( $a$ ) and the <i>slope exponent</i> ( $b$ ) values for a power function of the form $Y = aX^b$ , when $Y$ is one of the selected hydraulic parameters and $X$ is a given discharge value ( $Q$ ).							
		Width ( $W$ )	Depth ( $d$ )	Area ( $A$ )	Velocity ( $u$ )		
Intercept Coefficient:	( $a$ )						
Slope Exponent:	( $b$ )						
Hydraulic Radius: $R = A / W_p$			ft	Manning's "n" at Bankfull Stage		0.04	Coeff.
$"n" = 1.4865 [ ( Area ) ( Hydraulic Radius^{2/3} ) ( Slope^{1/2} ) ] / Q_{bkf}$							

**Worksheet 2-2.** Computations of velocity and bankfull discharge using various methods (Rosgen, 2006b; Rosgen and Silvey, 2007).

Bankfull VELOCITY / DISCHARGE Estimates									
Site	Rush River-2-6.15			Location	Rush River-2-6.15				
Date	9/27/2011	Stream Type	E6	Valley Type	X				
Observers	KP, AL			HUC	-- -- -- -- -- -- -- -- -- --				
INPUT VARIABLES				OUTPUT VARIABLES					
Bankfull Cross-sectional	84.4	$A_{b_{kf}}$ (ft <sup>2</sup> )	Bankfull Mean DEPTH	3.1	$D_{b_{kf}}$ (ft)				
Bankfull WIDTH	27.0	$W_{b_{kf}}$ (ft)	Wetted PERIMETER $\sim 2 * d_{b_{kf}} + W_{b_{kf}}$	33.2	$W_p$ (ft)				
$D_{84}$ @ Riffle	0.0017	Dia. (mm)	$D_{84}$ mm / 304.8 =	0.00	$D_{84}$ (ft)				
Bankfull SLOPE	0.0007	$S_{b_{kf}}$ (ft / ft)	Hydraulic RADIUS $A_{b_{kf}} / W_p$	2.5	R (ft)				
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R (ft) / $D_{84}$ (ft)	456233					
Drainage AREA	139.3	DA (mi <sup>2</sup> )	Shear Velocity $u^* = \sqrt{gRS}$	0.2	$u^*$ (ft / sec)				
ESTIMATION METHODS				Bankfull VELOCITY		Bankfull DISCHARGE			
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 \text{Log}\{ R / D_{84} \} ] u^*$				8.1	ft / sec	688	cfs		
2. Roughness Coefficient: a) Manning's 'n' from friction factor / relative roughness (Figs. 2-18, 19) $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text"/>				1.8	ft / sec	151	cfs		
2. Roughness Coefficient: b) Manning's 'n' from Jarrett ( USGS ): $n = 0.39S^{-.38}R^{-.16}$ n = <input type="text"/> Note: This equation is for applications involving steep, step-pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for stream types A1, A2, A3, B1, B2, B3, C2 and E3.				3.4	ft / sec	290	cfs		
2. Roughness Coefficient: c) Manning's 'n' from Stream Type $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text" value="0.04"/>				1.8	ft / sec	151	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.) HEC-RAS				1.9	ft / sec	150	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.)					ft / sec		cfs		
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge Q = <input type="text" value="1.46"/> Yr. $u = Q / A$					ft / sec		cfs		
4. Continuity Equations: b) USGS Gage Data $u = Q / A$					ft / sec		cfs		
Options for using the $D_{84}$ term in the relative roughness relation (R/ $D_{84}$ ), when using estimation method 1.									
Option 1. For sand-bed channels: Measure the "protrusion height" ( $h_{sd}$ ) of sand dunes above channel bed elevations. Substitute an average sand dune protrusion height ( $h_{sd}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 2. For boulder-dominated channels: Measure several "protrusion heights" ( $h_{bo}$ ) of boulders above channel bed elevations. Substitute an ave. boulder protrusion height ( $h_{bo}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 3. For bedrock-dominated channels: Measure several "protrusion heights" ( $h_{br}$ ) of rock separations/steps/joints/uplifted surfaces above channel bed elevations. Substitute an average bedrock protrusion height ( $h_{br}$ in feet) for the $D_{84}$ term in estimation method 1.									

**Worksheet 2-3.** Field form for Level II stream classification (Rosgen, 1996; Rosgen, 2006b).

Stream: <b>Rush River-2-6.15</b>	
Basin: <b>Red River Basin</b>	Drainage Area: <b>89152</b> acres <b>139.3</b> mi <sup>2</sup>
Location: <b>Rush River-2-6.15</b>	
Twp.&Rge: -	Sec.&Qtr.: -
Cross-Section Monuments (Lat./Long.): -	Date: <b>9/27/2011</b>
Observers: <b>KP, AL</b>	Valley Type: <b>X</b>

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>27.0</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>3.1</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>84.4</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>8.7</b>	ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>5.0</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>79.3</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>2.9</b>	ft/ft
<b>Channel Materials (Particle Size Index) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>&lt;0.001</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.00067</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).	<b>1.43</b>	

<b>Stream Type</b>	<b>E6</b>	<b>See Classification Key (Figure 2-21)</b>
--------------------	-----------	---

**Worksheet 2-4.** Morphological relations, including dimensionless ratios of river reach sites (Rosgen, 2006b; Rosgen and Silvey 2007).

Stream: <b>Rush River-2-6.15</b>		Location: <b>Rush River-2-6.15</b>								
Observers: <b>KP, AL</b>		Date: <b>9/27/2011</b>		Valley Type: <b>X</b>		Stream Type: <b>E6</b>				
<b>River Reach Summary Data</b>										
<b>Channel Dimension</b>	Mean Riffle Depth ( $d_{bkt}$ )	<b>3.1</b>	ft	Riffle Width ( $W_{bkt}$ )	<b>27.0</b>	ft	Riffle Area ( $A_{bkt}$ )	<b>84.4</b>	ft <sup>2</sup>	
	Mean Pool Depth ( $d_{bkfp}$ )		ft	Pool Width ( $W_{bkfp}$ )		ft	Pool Area ( $A_{bkfp}$ )		ft <sup>2</sup>	
	Mean Pool Depth/Mean Riffle Depth		$d_{bkfp}/d_{bkt}$	Pool Width/Riffle Width		$W_{bkfp}/W_{bkt}$	Pool Area / Riffle Area		$A_{bkfp}/A_{bkt}$	
	Max Riffle Depth ( $d_{maxrif}$ )	<b>5.0</b>	ft	Max Pool Depth ( $d_{maxp}$ )		ft	Max Riffle Depth/Mean Riffle Depth	<b>1.6</b>		
	Max Pool Depth/Mean Riffle Depth			Point Bar Slope		ft/ft	Inner Berm Width ( $W_{ib}$ )		ft	
	Inner Berm Depth ( $d_{ib}$ )		ft	Inner Berm Width/Depth Ratio			$W_{ib}/d_{ib}$	Inner Berm Area ( $A_{ib}$ )		ft <sup>2</sup>
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )				<b>1.9</b>	ft/s	Estimation Method		<b>HEC-RAS</b>	
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )				<b>150</b>	cfs	Drainage Area		<b>139.3</b>	mi <sup>2</sup>

<b>Channel Pattern</b>	Geometry			Dimensionless Geometry Ratios			
	Mean	Min	Max	Mean	Min	Max	
	Meander Wavelength ( $L_m$ )	<b>2344</b>			ft	Meander Length Ratio ( $L_m/W_{bkt}$ )	<b>86.9</b>
	Radius of Curvature ( $R_c$ )	<b>234</b>			ft	Radius of Curvature/Riffle Width ( $R_c/W_{bkt}$ )	<b>8.7</b>
	Belt Width ( $W_{bit}$ )	<b>1408</b>			ft	Meander Width Ratio ( $W_{bit}/W_{bkt}$ )	<b>52.2</b>
	Individual Pool Length				ft	Pool Length/Riffle Width	
	Pool to Pool Spacing				ft	Pool to Pool Spacing/Riffle Width	
Riffle Length				ft	Riffle Length/Riffle Width		

<b>Channel Profile</b>	Valley Slope (VS)		ft/ft	Average Water Surface Slope (S)		ft/ft	Sinuosity (VS/S)		
	Stream Length (SL)	<b>48503</b>	ft	Valley Length (VL)	<b>39164</b>	ft	Sinuosity (SL/VL)	<b>1.2</b>	
	Low Bank Height (LBH)	start: end:	ft ft	Max Riffle Depth	start: end:	ft ft	Bank-Height Ratio (BHR) (LBH/Max Riffle Depth)	start: end:	
	Facet Slopes			Dimensionless Slope Ratios			Mean	Min	Max
	Riffle Slope ( $S_{rif}$ )	<b>0.0</b>		ft/ft	Riffle Slope/Average Water Surface Slope ( $S_{rif} / S$ )	<b>1.0</b>			
	Run Slope ( $S_{run}$ )			ft/ft	Run Slope/Average Water Surface Slope ( $S_{run} / S$ )				
	Pool Slope ( $S_p$ )			ft/ft	Pool Slope/Average Water Surface Slope ( $S_p / S$ )				
	Glide Slope ( $S_g$ )			ft/ft	Glide Slope/Average Water Surface Slope ( $S_g / S$ )				
	Feature Midpoint <sup>a</sup>			Dimensionless Depth Ratios			Mean	Min	Max
	Max Riffle Depth ( $d_{maxrif}$ )	<b>5.0</b>		ft	Max Riffle Depth/Mean Riffle Depth ( $d_{maxrif} / d_{bkt}$ )	<b>1.6</b>			
	Max Run Depth ( $d_{maxrun}$ )			ft	Max Run Depth/Mean Riffle Depth ( $d_{maxrun} / d_{bkt}$ )				
	Max Pool Depth ( $d_{maxp}$ )			ft	Max Pool Depth/Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )				
	Max Glide Depth ( $d_{maxg}$ )			ft	Max Glide Depth/Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )				

<b>Channel Materials</b>	Reach <sup>b</sup>			Riffle <sup>c</sup>			Bar			Protrusion Height <sup>d</sup>		
	% Silt/Clay	<b>98</b>			$D_{16}$	<b>&lt;.001</b>						mm
	% Sand	<b>2</b>			$D_{35}$	<b>&lt;.001</b>					mm	
	% Gravel	<b>0</b>			$D_{50}$	<b>&lt;0.001</b>					mm	
	% Cobble	<b>0</b>			$D_{84}$	<b>0.0017</b>					mm	
	% Boulder	<b>0</b>			$D_{95}$	<b>0.0046</b>					mm	
	% Bedrock	<b>0</b>			$D_{100}$	<b>4.75</b>					mm	

<sup>a</sup> Min, max, mean depths are ave. mid-point values except pools: taken at deepest part of pool.

<sup>b</sup> Composite sample of riffles and pools within the designated reach.

<sup>c</sup> Active bed of a riffle.

<sup>d</sup> Height of roughness feature above bed.

**Worksheet 2-1.** Gage station and field data (Rosgen and Silvey, 2007).

Summary.... <b>USGS GAGE STATION</b> Data/Records for <b>STREAM CHANNEL CLASSIFICATION</b>					
Station NAME:	Rush River - 1 - 0.08			Station Number:	N/A
LOCATION:	Rush River - 1 - 0.08				
Period of RECORD:	N/A	yrs	Mean Annual DISCHARGE:	N/A	cfs
Drainage AREA:	98944	acres	154.6	mi <sup>2</sup>	Drainage Area Mn ELEV: 869.61 ft
Reference REACH SLOPE:		ft/ft	Valley Type:	X	
Stream Type:	E6		HUC:	-- -- -- -- -- -- -- -- -- -- -- --	
"BANKFULL" CHARACTERISTICS					
Determined from FIELD MEASUREMENT			Determined from GAGE DATA Analysis		
Bankfull WIDTH ( $W_{bkf}$ )	37.4	ft	Bankfull WIDTH ( $W_{bkf}$ )		ft
Bankfull Mean DEPTH ( $d_{bkf}$ )	3.3	ft	Bankfull MEAN DEPTH ( $d_{bkf}$ )		ft
Bankfull Xsec AREA ( $A_{bkf}$ )	111.1	ft <sup>2</sup>	Bankfull Xsec AREA ( $A_{bkf}$ )		ft <sup>2</sup>
Wetted PERIMETER ( $W_p$ )	36.0	ft	Wetted PERIMETER ( $W_p$ )		ft
Bankfull STAGE (Gage Ht)		ft	Bankfull STAGE (Gage Ht)		ft
Est. Mean VELOCITY ( $u$ )	1.4	ft/sec	Mean VELOCITY ( $u$ )		ft/sec
Est. Bkf. DISCHARGE ( $Q_{bkf}$ )	150.0	cfs	Bankfull DISCHARGE ( $Q_{bkf}$ )		cfs
Bankfull DISCHARGE associated with "field-determined" Bankfull STAGE				150.0	cfs
Recurrence Interval ( Log-Pearson ) associated with "field-determined" Bankfull Discharge				1.2	yrs
From the Annual Peak Flow Frequency Analysis data for the Gage Station, determine:					
1.5 Year R.I. Discharge..... =	N/A	cfs	10 Year R.I. Discharge..... =	N/A	cfs
2.0 Year R.I. Discharge..... =	N/A	cfs	25 Year R.I. Discharge..... =	N/A	cfs
5.0 Year R.I. Discharge..... =	N/A	cfs	50 Year R.I. Discharge..... =	N/A	cfs
MEANDER GEOMETRY					
Meander Length ( $L_m$ )		ft	Radius of Curvature ( $R_C$ )		ft
Belt Width ( $W_{blt}$ )		ft	Meander Width Ratio ( $W_{blt}/W_{bkf}$ )	0.0	ft/ft
HYDRAULIC GEOMETRY					
Based on <i>USGS Discharge Summary Notes</i> data ( Form 9-207 ) and regression analyses of measured discharge ( $Q$ ) with the hydraulic parameters of Width ( $W$ ), Area ( $A$ ), Mean Depth ( $d$ ) & Mean Velocity ( $u$ ), determine the <i>intercept coefficient</i> ( $a$ ) and the <i>slope exponent</i> ( $b$ ) values for a power function of the form $Y = aX^b$ , when $Y$ is one of the selected hydraulic parameters and $X$ is a given discharge value ( $Q$ ).					
	Width ( $W$ )	Depth ( $d$ )	Area ( $A$ )	Velocity ( $u$ )	
Intercept Coefficient: ( $a$ )					
Slope Exponent: ( $b$ )					
Hydraulic Radius: $R = A / W_p$		ft	Manning's "n" at Bankfull Stage	0.04	Coeff.
$"n" = 1.4865 [ ( Area ) ( Hydraulic Radius^{2/3} ) ( Slope^{1/2} ) ] / Q_{bkf}$					

**Worksheet 2-2.** Computations of velocity and bankfull discharge using various methods (Rosgen, 2006b; Rosgen and Silvey, 2007).

Bankfull VELOCITY / DISCHARGE Estimates									
Site	Rush River - 1 - 0.08			Location	Rush River - 1 - 0.08				
Date	9/29/2011	Stream Type	E6	Valley Type	X				
Observers	KP, AL			HUC	-- -- -- -- -- -- -- -- -- --				
INPUT VARIABLES				OUTPUT VARIABLES					
Bankfull Cross-sectional	111.1	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Mean DEPTH	3.3	$D_{bkf}$ (ft)				
Bankfull WIDTH	37.4	$W_{bkf}$ (ft)	Wetted PERIMETER $\sim 2 * d_{bkf} + W_{bkf}$	43.9	$W_p$ (ft)				
$D_{84}$ @ Riffle	0.0055	Dia. (mm)	$D_{84}$ mm / 304.8 =	0.00	$D_{84}$ (ft)				
Bankfull SLOPE	0.0004	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	2.5	R (ft)				
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R (ft) / $D_{84}$ (ft)	140176					
Drainage AREA	154.6	DA (mi <sup>2</sup> )	Shear Velocity $u^* = \sqrt{gRS}$	0.2	$u^*$ (ft / sec)				
ESTIMATION METHODS				Bankfull VELOCITY		Bankfull DISCHARGE			
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 \text{Log}\{ R / D_{84} \} ] u^*$				6.0	ft / sec	663	cfs		
2. Roughness Coefficient: a) Manning's 'n' from friction factor / relative roughness (Figs. 2-18, 19) $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text"/>				1.4	ft / sec	159	cfs		
2. Roughness Coefficient: $u = 1.4865 * R^{2/3} * S^{1/2} / n$ b) Manning's 'n' from Jarrett ( USGS ): $n = 0.39S^{-.38}R^{-.16}$ n = <input type="text"/>				3.2	ft / sec	359	cfs		
Note: This equation is for applications involving steep, step-pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for stream types A1, A2, A3, B1, B2, B3, C2 and E3.									
2. Roughness Coefficient: c) Manning's 'n' from Stream Type $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text" value="0.04"/>				1.4	ft / sec	159	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.) HEC-RAS				1.4	ft / sec	150	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.)					ft / sec		cfs		
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge Q = <input type="text" value="1.46"/> Yr. $u = Q / A$					ft / sec		cfs		
4. Continuity Equations: b) USGS Gage Data $u = Q / A$					ft / sec		cfs		
Options for using the $D_{84}$ term in the relative roughness relation ( $R/D_{84}$ ), when using estimation method 1.									
Option 1. For sand-bed channels: Measure the "protrusion height" ( $h_{sd}$ ) of sand dunes above channel bed elevations. Substitute an average sand dune protrusion height ( $h_{sd}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 2. For boulder-dominated channels: Measure several "protrusion heights" ( $h_{bo}$ ) of boulders above channel bed elevations. Substitute an ave. boulder protrusion height ( $h_{bo}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 3. For bedrock-dominated channels: Measure several "protrusion heights" ( $h_{br}$ ) of rock separations/steps/joints/uplifted surfaces above channel bed elevations. Substitute an average bedrock protrusion height ( $h_{br}$ in feet) for the $D_{84}$ term in estimation method 1.									

**Worksheet 2-3.** Field form for Level II stream classification (Rosgen, 1996; Rosgen, 2006b).

Stream: <b>Rush River - 1 - 0.08</b>	
Basin: <b>Red River Basin</b>	Drainage Area: <b>98944</b> acres <b>154.6</b> mi <sup>2</sup>
Location: <b>Rush River - 1 - 0.08</b>	
Twp.&Rge: - Sec.&Qtr.: -	
Cross-Section Monuments (Lat./Long.): - Date: <b>9/29/2011</b>	
Observers: <b>KP, AL</b> Valley Type: <b>X</b>	

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>37.4</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>3.3</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>111.1</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>11.5</b>	ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>5.2</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>91.7</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>2.5</b>	ft/ft
<b>Channel Materials (Particle Size Index) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>&lt;0.001</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.00043</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).		

<b>Stream Type</b>	<b>E6</b>	<b>See Classification Key (Figure 2-21)</b>
--------------------	-----------	---

**Worksheet 2-4.** Morphological relations, including dimensionless ratios of river reach sites (Rosgen, 2006b; Rosgen and Silvey 2007).

Stream: <b>Rush River - 1 - 0.08</b>		Location: <b>Rush River - 1 - 0.08</b>								
Observers: <b>KP, AL</b>		Date: <b>9/29/2011</b>		Valley Type: <b>X</b>		Stream Type: <b>E6</b>				
<b>River Reach Summary Data</b>										
<b>Channel Dimension</b>	Mean Riffle Depth ( $d_{bkt}$ )	<b>3.3</b>	ft	Riffle Width ( $W_{bkt}$ )	<b>37.4</b>	ft	Riffle Area ( $A_{bkt}$ )	<b>111.1</b>	ft <sup>2</sup>	
	Mean Pool Depth ( $d_{bkfp}$ )		ft	Pool Width ( $W_{bkfp}$ )		ft	Pool Area ( $A_{bkfp}$ )		ft <sup>2</sup>	
	Mean Pool Depth/Mean Riffle Depth		$d_{bkfp}/d_{bkt}$	Pool Width/Riffle Width		$W_{bkfp}/W_{bkt}$	Pool Area / Riffle Area		$A_{bkfp}/A_{bkt}$	
	Max Riffle Depth ( $d_{maxrif}$ )	<b>5.2</b>	ft	Max Pool Depth ( $d_{maxp}$ )		ft	Max Riffle Depth/Mean Riffle Depth	<b>1.6</b>		
	Max Pool Depth/Mean Riffle Depth			Point Bar Slope		ft/ft	Inner Berm Width ( $W_{ib}$ )		ft	
	Inner Berm Depth ( $d_{ib}$ )		ft	Inner Berm Width/Depth Ratio			$W_{ib}/d_{ib}$	Inner Berm Area ( $A_{ib}$ )		ft <sup>2</sup>
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )				<b>1.4</b>	ft/s	Estimation Method		<b>HEC-RAS</b>	
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )				<b>150</b>	cfs	Drainage Area		<b>154.6</b>	mi <sup>2</sup>

<b>Channel Pattern</b>	Geometry			Dimensionless Geometry Ratios			
	Mean	Min	Max	Mean	Min	Max	
	Meander Wavelength ( $L_m$ )	<b>0</b>			ft	Meander Length Ratio ( $L_m/W_{bkt}$ )	<b>0.0</b>
	Radius of Curvature ( $R_c$ )	<b>0</b>			ft	Radius of Curvature/Riffle Width ( $R_c/W_{bkt}$ )	<b>0.0</b>
	Belt Width ( $W_{bit}$ )	<b>0</b>			ft	Meander Width Ratio ( $W_{bit}/W_{bkt}$ )	<b>0.0</b>
	Individual Pool Length				ft	Pool Length/Riffle Width	
	Pool to Pool Spacing				ft	Pool to Pool Spacing/Riffle Width	
Riffle Length				ft	Riffle Length/Riffle Width		

<b>Channel Profile</b>	Valley Slope (VS)		ft/ft	Average Water Surface Slope (S)		ft/ft	Sinuosity (VS/S)		
	Stream Length (SL)	<b>48503</b>	ft	Valley Length (VL)	<b>39164</b>	ft	Sinuosity (SL/VL)	<b>1.2</b>	
	Low Bank Height (LBH)	start: end:	ft	Max Riffle Depth	start: end:	ft	Bank-Height Ratio (BHR) (LBH/Max Riffle Depth)	start: end:	
	Facet Slopes			Dimensionless Slope Ratios			Mean	Min	Max
	Riffle Slope ( $S_{rif}$ )	<b>0.0</b>		ft/ft	Riffle Slope/Average Water Surface Slope ( $S_{rif} / S$ )	<b>1.0</b>			
	Run Slope ( $S_{run}$ )			ft/ft	Run Slope/Average Water Surface Slope ( $S_{run} / S$ )				
	Pool Slope ( $S_p$ )			ft/ft	Pool Slope/Average Water Surface Slope ( $S_p / S$ )				
	Glide Slope ( $S_g$ )			ft/ft	Glide Slope/Average Water Surface Slope ( $S_g / S$ )				
	Feature Midpoint <sup>a</sup>			Dimensionless Depth Ratios			Mean	Min	Max
	Max Riffle Depth ( $d_{maxrif}$ )	<b>5.2</b>		ft	Max Riffle Depth/Mean Riffle Depth ( $d_{maxrif} / d_{bkt}$ )	<b>1.6</b>			
	Max Run Depth ( $d_{maxrun}$ )			ft	Max Run Depth/Mean Riffle Depth ( $d_{maxrun} / d_{bkt}$ )				
	Max Pool Depth ( $d_{maxp}$ )			ft	Max Pool Depth/Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )				
	Max Glide Depth ( $d_{maxg}$ )			ft	Max Glide Depth/Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )				

<b>Channel Materials</b>	Reach <sup>b</sup>			Riffle <sup>c</sup>			Bar			Protrusion Height <sup>d</sup>		
	% Silt/Clay	<b>99</b>			$D_{16}$	<b>&lt;.001</b>						mm
	% Sand	<b>1</b>			$D_{35}$	<b>&lt;.001</b>					mm	
	% Gravel	<b>0</b>			$D_{50}$	<b>&lt;.001</b>					mm	
	% Cobble	<b>0</b>			$D_{84}$	<b>0.0055</b>					mm	
	% Boulder	<b>0</b>			$D_{95}$	<b>0.06</b>					mm	
	% Bedrock	<b>0</b>			$D_{100}$	<b>0.25</b>					mm	

<sup>a</sup> Min, max, mean depths are ave. mid-point values except pools: taken at deepest part of pool.

<sup>b</sup> Composite sample of riffles and pools within the designated reach.

<sup>c</sup> Active bed of a riffle.

<sup>d</sup> Height of roughness feature above bed.

**Worksheet 2-1.** Gage station and field data (Rosgen and Silvey, 2007).

Summary.... <b>USGS GAGE STATION</b> Data/Records for <b>STREAM CHANNEL CLASSIFICATION</b>					
Station NAME:	Red River-8-521.18			Station Number:	N/A
LOCATION:	Red River-8-521.18				
Period of RECORD:	N/A	yrs	Mean Annual DISCHARGE:	N/A	cfs
Drainage AREA:	2189440	acres	3421	mi <sup>2</sup>	Drainage Area Mn ELEV: 902.14 ft
Reference REACH SLOPE:		ft/ft	Valley Type:	X	
Stream Type:	C6c-		HUC:	-- -- -- -- --	
"BANKFULL" CHARACTERISTICS					
Determined from FIELD MEASUREMENT			Determined from GAGE DATA Analysis		
Bankfull WIDTH ( $W_{bkf}$ )	138.0	ft	Bankfull WIDTH ( $W_{bkf}$ )		ft
Bankfull Mean DEPTH ( $d_{bkf}$ )	6.6	ft	Bankfull MEAN DEPTH ( $d_{bkf}$ )		ft
Bankfull Xsec AREA ( $A_{bkf}$ )	914.5	ft <sup>2</sup>	Bankfull Xsec AREA ( $A_{bkf}$ )		ft <sup>2</sup>
Wetted PERIMETER ( $W_p$ )	141.6	ft	Wetted PERIMETER ( $W_p$ )		ft
Bankfull STAGE (Gage Ht)		ft	Bankfull STAGE (Gage Ht)		ft
Est. Mean VELOCITY ( $u$ )	1.8	ft/sec	Mean VELOCITY ( $u$ )		ft/sec
Est. Bkf. DISCHARGE ( $Q_{bkf}$ )	1650.0	cfs	Bankfull DISCHARGE ( $Q_{bkf}$ )		cfs
Bankfull DISCHARGE associated with "field-determined" Bankfull STAGE				1650.0	cfs
Recurrence Interval ( Log-Pearson ) associated with "field-determined" Bankfull Discharge				1.2	yrs
From the Annual Peak Flow Frequency Analysis data for the Gage Station, determine:					
1.5 Year R.I. Discharge..... =	N/A	cfs	10 Year R.I. Discharge..... =	N/A	cfs
2.0 Year R.I. Discharge..... =	N/A	cfs	25 Year R.I. Discharge..... =	N/A	cfs
5.0 Year R.I. Discharge..... =	N/A	cfs	50 Year R.I. Discharge..... =	N/A	cfs
MEANDER GEOMETRY					
Meander Length ( $L_m$ )	1298	ft	Radius of Curvature ( $R_C$ )	507.0	ft
Belt Width ( $W_{blt}$ )	2568	ft	Meander Width Ratio ( $W_{blt}/W_{bkf}$ )	18.6	ft/ft
HYDRAULIC GEOMETRY					
Based on USGS Discharge Summary Notes data ( Form 9-207 ) and regression analyses of measured discharge ( $Q$ ) with the hydraulic parameters of Width ( $W$ ), Area ( $A$ ), Mean Depth ( $d$ ) & Mean Velocity ( $u$ ), determine the <i>intercept coefficient</i> ( $a$ ) and the <i>slope exponent</i> ( $b$ ) values for a power function of the form $Y = aX^b$ , when $Y$ is one of the selected hydraulic parameters and $X$ is a given discharge value ( $Q$ ).					
	Width ( $W$ )	Depth ( $d$ )	Area ( $A$ )	Velocity ( $u$ )	
Intercept Coefficient: ( $a$ )					
Slope Exponent: ( $b$ )					
Hydraulic Radius: $R = A / W_p$		ft	Manning's "n" at Bankfull Stage	0.035	Coeff.
$"n" = 1.4865 [( Area ) ( Hydraulic Radius^{2/3} ) ( Slope^{1/2} )] / Q_{bkf}$					

**Worksheet 2-2.** Computations of velocity and bankfull discharge using various methods (Rosgen, 2006b; Rosgen and Silvey, 2007).

Bankfull VELOCITY / DISCHARGE Estimates										
Site	Red River-8-521.18				Location	Red River-8-521.18				
Date	10/5/2011	Stream Type	C6c-	Valley Type	X					
Observers	KD, JB				HUC	-- -- -- -- -- -- -- -- -- --				
INPUT VARIABLES				OUTPUT VARIABLES						
Bankfull Cross-sectional	914.5	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Mean DEPTH	6.6	$D_{bkf}$ (ft)					
Bankfull WIDTH	138.0	$W_{bkf}$ (ft)	Wetted PERIMETER ~ 2 * $d_{bkf}$ + $W_{bkf}$	151.3	$W_p$ (ft)					
$D_{84}$ @ Riffle	3.2	Dia. (mm)	$D_{84}$ mm / 304.8 =	0.01	$D_{84}$ (ft)					
Bankfull SLOPE	0.0002	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	6.0	R (ft)					
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R (ft) / $D_{84}$ (ft)	576						
Drainage AREA	3421.0	DA (mi <sup>2</sup> )	Shear Velocity	0.2	$u^*$ (ft / sec)					
ESTIMATION METHODS				Bankfull VELOCITY		Bankfull DISCHARGE				
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 \text{Log}\{ R / D_{84} \} ] u^*$				3.2	ft / sec	2943	cfs			
2. Roughness Coefficient: a) Manning's 'n' from friction factor / relative roughness (Figs. 2-18, 19) $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text"/>				1.8	ft / sec	1611	cfs			
2. Roughness Coefficient: b) Manning's 'n' from Jarrett ( USGS ): $n = 0.39 S^{-.38} R^{-.16}$ n = <input type="text"/>				5.9	ft / sec	5389	cfs			
Note: This equation is for applications involving steep, step-pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for stream types A1, A2, A3, B1, B2, B3, C2 and E3.										
2. Roughness Coefficient: c) Manning's 'n' from Stream Type n = <input type="text" value="0.035"/>				1.8	ft / sec	1611	cfs			
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.) HEC-RAS				1.8	ft / sec	1650	cfs			
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.)					ft / sec		cfs			
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge Q = <input type="text" value="1.46"/> Yr. $u = Q / A$					ft / sec		cfs			
4. Continuity Equations: b) USGS Gage Data $u = Q / A$					ft / sec		cfs			
Options for using the $D_{84}$ term in the relative roughness relation ( $R/D_{84}$ ), when using estimation method 1.										
Option 1. For sand-bed channels: Measure the "protrusion height" ( $h_{sd}$ ) of sand dunes above channel bed elevations. Substitute an average sand dune protrusion height ( $h_{sd}$ in ft) for the $D_{84}$ term in est. method 1.										
Option 2. For boulder-dominated channels: Measure several "protrusion heights" ( $h_{bo}$ ) of boulders above channel bed elevations. Substitute an ave. boulder protrusion height ( $h_{bo}$ in ft) for the $D_{84}$ term in est. method 1.										
Option 3. For bedrock-dominated channels: Measure several "protrusion heights" ( $h_{br}$ ) of rock separations/steps/joints/uplifted surfaces above channel bed elevations. Substitute an average bedrock protrusion height ( $h_{br}$ in feet) for the $D_{84}$ term in estimation method 1.										

**Worksheet 2-3.** Field form for Level II stream classification (Rosgen, 1996; Rosgen , 2006b).

Stream: <b>Red River-8-521.18</b>	
Basin: <b>Red River Basin</b>	Drainage Area: <b>2E+06</b> acres <b>3421</b> mi <sup>2</sup>
Location: <b>Red River-8-521.18</b>	
Twp.&Rge: -	Sec.&Qtr.: -
Cross-Section Monuments (Lat./Long.): -	Date: <b>10/5/2011</b>
Observers: <b>KD, JB</b>	Valley Type: <b>X</b>

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>138.0</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>6.6</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>914.5</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>20.8</b>	ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>9.7</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>788.0</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>5.7</b>	ft/ft
<b>Channel Materials (Particle Size Index ) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>0.007</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.00016</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).	<b>2.6</b>	

<div style="border: 1px solid black; padding: 5px; display: inline-block;"> <b>Stream Type</b> </div>	<div style="border: 1px solid black; padding: 5px; display: inline-block; background-color: yellow;"> <b>C6c-</b> </div>	<div style="border: 1px solid black; padding: 5px; display: inline-block;"> <b>See Classification Key (Figure 2-21)</b> </div>
---	--	--

**Worksheet 2-4.** Morphological relations, including dimensionless ratios of river reach sites (Rosgen, 2006b; Rosgen and Silvey 2007).

Stream: <b>Red River-8-521.18</b>		Location: <b>Red River-8-521.18</b>								
Observers: <b>KD, JB</b>		Date: <b>10/5/2011</b>		Valley Type: <b>X</b>		Stream Type: <b>C6c-</b>				
<b>River Reach Summary Data</b>										
<b>Channel Dimension</b>	Mean Riffle Depth ( $d_{bkt}$ )	<b>6.6</b>	ft	Riffle Width ( $W_{bkt}$ )	<b>138.0</b>	ft	Riffle Area ( $A_{bkt}$ )	<b>914.5</b>	ft <sup>2</sup>	
	Mean Pool Depth ( $d_{bkfp}$ )		ft	Pool Width ( $W_{bkfp}$ )		ft	Pool Area ( $A_{bkfp}$ )		ft <sup>2</sup>	
	Mean Pool Depth/Mean Riffle Depth		$d_{bkfp}/d_{bkt}$	Pool Width/Riffle Width		$W_{bkfp}/W_{bkt}$	Pool Area / Riffle Area		$A_{bkfp}/A_{bkt}$	
	Max Riffle Depth ( $d_{maxrif}$ )	<b>9.72</b>	ft	Max Pool Depth ( $d_{maxp}$ )		ft	Max Riffle Depth/Mean Riffle Depth	<b>1.5</b>		
	Max Pool Depth/Mean Riffle Depth			Point Bar Slope		ft/ft	Inner Berm Width ( $W_{ib}$ )		ft	
	Inner Berm Depth ( $d_{ib}$ )		ft	Inner Berm Width/Depth Ratio			$W_{ib}/d_{ib}$	Inner Berm Area ( $A_{ib}$ )		ft <sup>2</sup>
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )				<b>1.8</b>	ft/s	Estimation Method		<b>HEC-RAS</b>	
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )				<b>1650</b>	cfs	Drainage Area		<b>3421</b>	mi <sup>2</sup>

<b>Channel Pattern</b>	Geometry			Dimensionless Geometry Ratios			
	Mean	Min	Max	Mean	Min	Max	
	Meander Wavelength ( $L_m$ )	<b>1298</b>		ft	Meander Length Ratio ( $L_m/W_{bkt}$ )	<b>9.4</b>	
	Radius of Curvature ( $R_c$ )	<b>507</b>		ft	Radius of Curvature/Riffle Width ( $R_c/W_{bkt}$ )	<b>3.7</b>	
	Belt Width ( $W_{bit}$ )	<b>2568</b>		ft	Meander Width Ratio ( $W_{bit}/W_{bkt}$ )	<b>18.6</b>	
	Individual Pool Length			ft	Pool Length/Riffle Width		
	Pool to Pool Spacing			ft	Pool to Pool Spacing/Riffle Width		
Riffle Length			ft	Riffle Length/Riffle Width			

<b>Channel Profile</b>	Valley Slope (VS)		ft/ft	Average Water Surface Slope (S)		ft/ft	Sinuosity (VS/S)		
	Stream Length (SL)	<b>138749</b>	ft	Valley Length (VL)	<b>53266</b>	ft	Sinuosity (SL/VL)	<b>2.6</b>	
	Low Bank Height (LBH)	start: _____ end: _____	ft	Max Riffle Depth	start: _____ end: _____	ft	Bank-Height Ratio (BHR) (LBH/Max Riffle Depth)	start: _____ end: _____	
	Facet Slopes			Dimensionless Slope Ratios			Mean	Min	Max
	Riffle Slope ( $S_{rif}$ )	<b>0.0</b>		ft/ft	Riffle Slope/Average Water Surface Slope ( $S_{rif} / S$ )	<b>1.0</b>			
	Run Slope ( $S_{run}$ )			ft/ft	Run Slope/Average Water Surface Slope ( $S_{run} / S$ )				
	Pool Slope ( $S_p$ )			ft/ft	Pool Slope/Average Water Surface Slope ( $S_p / S$ )				
	Glide Slope ( $S_g$ )			ft/ft	Glide Slope/Average Water Surface Slope ( $S_g / S$ )				
	Feature Midpoint <sup>a</sup>			Dimensionless Depth Ratios			Mean	Min	Max
	Max Riffle Depth ( $d_{maxrif}$ )	<b>9.7</b>		ft	Max Riffle Depth/Mean Riffle Depth ( $d_{maxrif} / d_{bkt}$ )	<b>1.5</b>			
	Max Run Depth ( $d_{maxrun}$ )			ft	Max Run Depth/Mean Riffle Depth ( $d_{maxrun} / d_{bkt}$ )				
	Max Pool Depth ( $d_{maxp}$ )			ft	Max Pool Depth/Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )				
	Max Glide Depth ( $d_{maxg}$ )			ft	Max Glide Depth/Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )				

<b>Channel Materials</b>	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Protrusion Height <sup>d</sup>
	% Silt/Clay	<b>63</b>		$D_{16}$	<b>&lt;.001</b>		mm
	% Sand	<b>25</b>		$D_{35}$	<b>0.0025</b>		mm
	% Gravel	<b>12</b>		$D_{50}$	<b>0.007</b>		mm
	% Cobble	<b>0</b>		$D_{84}$	<b>3.2</b>		mm
	% Boulder	<b>0</b>		$D_{95}$	<b>13.5</b>		mm
	% Bedrock	<b>0</b>		$D_{100}$	<b>19</b>		mm

<sup>a</sup> Min, max, mean depths are ave. mid-point values except pools: taken at deepest part of pool.

<sup>b</sup> Composite sample of riffles and pools within the designated reach.

<sup>c</sup> Active bed of a riffle.

<sup>d</sup> Height of roughness feature above bed.

**Worksheet 2-1.** Gage station and field data (Rosgen and Silvey, 2007).

Summary.... <b>USGS GAGE STATION</b> Data/Records for <b>STREAM CHANNEL CLASSIFICATION</b>					
Station NAME:	Red River-7-492.47			Station Number:	N/A
LOCATION:	Red River-7-492.47				
Period of RECORD:	N/A	yrs	Mean Annual DISCHARGE:	N/A	cfs
Drainage AREA:	2215040	acres	3461	mi <sup>2</sup>	Drainage Area Mn ELEV: 879.8 ft
Reference REACH SLOPE:		ft/ft	Valley Type:	X	
Stream Type:	C6c-		HUC:	-- -- -- -- --	
"BANKFULL" CHARACTERISTICS					
Determined from FIELD MEASUREMENT			Determined from GAGE DATA Analysis		
Bankfull WIDTH ( $W_{bkf}$ )	120.8	ft	Bankfull WIDTH ( $W_{bkf}$ )		ft
Bankfull Mean DEPTH ( $d_{bkf}$ )	8.9	ft	Bankfull MEAN DEPTH ( $d_{bkf}$ )		ft
Bankfull Xsec AREA ( $A_{bkf}$ )	1073.7	ft <sup>2</sup>	Bankfull Xsec AREA ( $A_{bkf}$ )		ft <sup>2</sup>
Wetted PERIMETER ( $W_p$ )	125.4	ft	Wetted PERIMETER ( $W_p$ )		ft
Bankfull STAGE (Gage Ht)		ft	Bankfull STAGE (Gage Ht)		ft
Est. Mean VELOCITY ( $u$ )	1.5	ft/sec	Mean VELOCITY ( $u$ )		ft/sec
Est. Bkf. DISCHARGE ( $Q_{bkf}$ )	1650.0	cfs	Bankfull DISCHARGE ( $Q_{bkf}$ )		cfs
Bankfull DISCHARGE associated with "field-determined" Bankfull STAGE				1650.0	cfs
Recurrence Interval ( Log-Pearson ) associated with "field-determined" Bankfull Discharge				1.2	yrs
From the Annual Peak Flow Frequency Analysis data for the Gage Station, determine:					
1.5 Year R.I. Discharge..... =	N/A	cfs	10 Year R.I. Discharge..... =	N/A	cfs
2.0 Year R.I. Discharge..... =	N/A	cfs	25 Year R.I. Discharge..... =	N/A	cfs
5.0 Year R.I. Discharge..... =	N/A	cfs	50 Year R.I. Discharge..... =	N/A	cfs
MEANDER GEOMETRY					
Meander Length ( $L_m$ )	2002	ft	Radius of Curvature ( $R_C$ )	500.0	ft
Belt Width ( $W_{blt}$ )	3121	ft	Meander Width Ratio ( $W_{blt}/W_{bkf}$ )	25.8	ft/ft
HYDRAULIC GEOMETRY					
Based on <i>USGS Discharge Summary Notes</i> data ( Form 9-207 ) and regression analyses of measured discharge ( $Q$ ) with the hydraulic parameters of Width ( $W$ ), Area ( $A$ ), Mean Depth ( $d$ ) & Mean Velocity ( $u$ ), determine the <i>intercept coefficient</i> ( $a$ ) and the <i>slope exponent</i> ( $b$ ) values for a power function of the form $Y = aX^b$ , when $Y$ is one of the selected hydraulic parameters and $X$ is a given discharge value ( $Q$ ).					
	Width ( $W$ )	Depth ( $d$ )	Area ( $A$ )	Velocity ( $u$ )	
Intercept Coefficient: ( $a$ )					
Slope Exponent: ( $b$ )					
Hydraulic Radius: $R = A / W_p$		ft	Manning's "n" at Bankfull Stage	0.035	Coeff.
$"n" = 1.4865 [ ( Area ) ( Hydraulic Radius^{2/3} ) ( Slope^{1/2} ) ] / Q_{bkf}$					

**Worksheet 2-2.** Computations of velocity and bankfull discharge using various methods (Rosgen, 2006b; Rosgen and Silvey, 2007).

Bankfull VELOCITY / DISCHARGE Estimates										
Site	Red River-7-492.47				Location	Red River-7-492.47				
Date	9/30/2011	Stream Type	C6c-	Valley Type	X					
Observers	KD, JB				HUC	-- -- -- -- -- -- -- -- -- --				
INPUT VARIABLES				OUTPUT VARIABLES						
Bankfull Cross-sectional	1073.7	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Mean DEPTH	8.9	$D_{bkf}$ (ft)					
Bankfull WIDTH	120.8	$W_{bkf}$ (ft)	Wetted PERIMETER $\sim 2 * d_{bkf} + W_{bkf}$	138.6	$W_p$ (ft)					
$D_{84}$ @ Riffle	1.0	Dia. (mm)	$D_{84}$ mm / 304.8 =	0.0	$D_{84}$ (ft)					
Bankfull SLOPE	0.0001	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	7.7	R (ft)					
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R (ft) / $D_{84}$ (ft)	2271						
Drainage AREA	3461.0	DA (mi <sup>2</sup> )	Shear Velocity $u^* = \sqrt{gRS}$	0.1	$u^*$ (ft / sec)					
ESTIMATION METHODS				Bankfull VELOCITY		Bankfull DISCHARGE				
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 \text{Log}\{ R / D_{84} \} ] u^*$				3.0	ft / sec	3197	cfs			
2. Roughness Coefficient: a) Manning's 'n' from friction factor / relative roughness (Figs. 2-18, 19) $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text"/>				1.4	ft / sec	1542	cfs			
2. Roughness Coefficient: b) Manning's 'n' from Jarrett ( USGS ): $n = 0.39S^{-.38}R^{-.16}$ n = <input type="text"/>				6.6	ft / sec	7109	cfs			
Note: This equation is for applications involving steep, step-pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for stream types A1, A2, A3, B1, B2, B3, C2 and E3.										
2. Roughness Coefficient: c) Manning's 'n' from Stream Type $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text" value="0.035"/>				1.4	ft / sec	1542	cfs			
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.) HEC-RAS				1.5	ft / sec	1650	cfs			
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.)					ft / sec		cfs			
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge Q = <input type="text" value="1.46"/> Yr. $u = Q / A$					ft / sec		cfs			
4. Continuity Equations: b) USGS Gage Data $u = Q / A$					ft / sec		cfs			
Options for using the $D_{84}$ term in the relative roughness relation (R/ $D_{84}$ ), when using estimation method 1.										
Option 1. For sand-bed channels: Measure the "protrusion height" ( $h_{sd}$ ) of sand dunes above channel bed elevations. Substitute an average sand dune protrusion height ( $h_{sd}$ in ft) for the $D_{84}$ term in est. method 1.										
Option 2. For boulder-dominated channels: Measure several "protrusion heights" ( $h_{bo}$ ) of boulders above channel bed elevations. Substitute an ave. boulder protrusion height ( $h_{bo}$ in ft) for the $D_{84}$ term in est. method 1.										
Option 3. For bedrock-dominated channels: Measure several "protrusion heights" ( $h_{br}$ ) of rock separations/steps/joints/uplifted surfaces above channel bed elevations. Substitute an average bedrock protrusion height ( $h_{br}$ in feet) for the $D_{84}$ term in estimation method 1.										

**Worksheet 2-3.** Field form for Level II stream classification (Rosgen, 1996; Rosgen , 2006b).

Stream: <b>Red River-7-492.47</b>	
Basin: <b>Red River Basin</b>	Drainage Area: <b>2E+06</b> acres <b>3461</b> mi <sup>2</sup>
Location: <b>Red River-7-492.47</b>	
Twp.&Rge: - Sec.&Qtr.: -	
Cross-Section Monuments (Lat./Long.): - Date: <b>9/30/2011</b>	
Observers: <b>KD, JB</b> Valley Type: <b>X</b>	

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>120.8</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>8.9</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>1073.7</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>13.6</b>	ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>13.3</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>404.0</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>3.3</b>	ft/ft
<b>Channel Materials (Particle Size Index ) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>0.025</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.000075</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).	<b>2.6</b>	

<div style="border: 1px solid black; padding: 5px; display: inline-block;">Stream Type</div>	<div style="border: 1px solid black; padding: 5px; display: inline-block; background-color: yellow;"><b>C6c-</b></div>	<div style="border: 1px solid black; padding: 5px; display: inline-block;">See Classification Key (Figure 2-21)</div>
--	--	---

**Worksheet 2-4.** Morphological relations, including dimensionless ratios of river reach sites (Rosgen, 2006b; Rosgen and Silvey 2007).

Stream: <b>Red River-7-492.47</b>		Location: <b>Red River-7-492.47</b>								
Observers: <b>KD, JB</b>		Date: <b>9/30/2011</b>		Valley Type: <b>X</b>		Stream Type: <b>C6c-</b>				
<b>River Reach Summary Data</b>										
<b>Channel Dimension</b>	Mean Riffle Depth ( $d_{bkt}$ )	<b>8.9</b>	ft	Riffle Width ( $W_{bkt}$ )	<b>120.8</b>	ft	Riffle Area ( $A_{bkt}$ )	<b>1073.7</b>	ft <sup>2</sup>	
	Mean Pool Depth ( $d_{bkfp}$ )		ft	Pool Width ( $W_{bkfp}$ )		ft	Pool Area ( $A_{bkfp}$ )		ft <sup>2</sup>	
	Mean Pool Depth/Mean Riffle Depth		$d_{bkfp}/d_{bkt}$	Pool Width/Riffle Width		$W_{bkfp}/W_{bkt}$	Pool Area / Riffle Area		$A_{bkfp}/A_{bkt}$	
	Max Riffle Depth ( $d_{maxrif}$ )	<b>13.3</b>	ft	Max Pool Depth ( $d_{maxp}$ )		ft	Max Riffle Depth/Mean Riffle Depth	<b>1.5</b>		
	Max Pool Depth/Mean Riffle Depth			Point Bar Slope		ft/ft	Inner Berm Width ( $W_{ib}$ )		ft	
	Inner Berm Depth ( $d_{ib}$ )		ft	Inner Berm Width/Depth Ratio			$W_{ib}/d_{ib}$	Inner Berm Area ( $A_{ib}$ )		ft <sup>2</sup>
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )				<b>1.5</b>	ft/s	Estimation Method		<b>HEC-RAS</b>	
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )				<b>1650</b>	cfs	Drainage Area		<b>3461</b>	mi <sup>2</sup>

<b>Channel Pattern</b>	Geometry			Dimensionless Geometry Ratios			
	Mean	Min	Max	Mean	Min	Max	
	Meander Wavelength ( $L_m$ )	<b>2002</b>			ft	Meander Length Ratio ( $L_m/W_{bkt}$ )	<b>16.6</b>
	Radius of Curvature ( $R_c$ )	<b>500</b>			ft	Radius of Curvature/Riffle Width ( $R_c/W_{bkt}$ )	<b>4.1</b>
	Belt Width ( $W_{bit}$ )	<b>3121</b>			ft	Meander Width Ratio ( $W_{bit}/W_{bkt}$ )	<b>25.8</b>
	Individual Pool Length				ft	Pool Length/Riffle Width	
	Pool to Pool Spacing				ft	Pool to Pool Spacing/Riffle Width	
Riffle Length				ft	Riffle Length/Riffle Width		

<b>Channel Profile</b>	Valley Slope (VS)		ft/ft	Average Water Surface Slope (S)		ft/ft	Sinuosity (VS/S)		
	Stream Length (SL)	<b>74148</b>	ft	Valley Length (VL)	<b>29010</b>	ft	Sinuosity (SL/VL)	<b>2.6</b>	
	Low Bank Height (LBH)	start: _____ end: _____	ft	Max Riffle Depth	start: _____ end: _____	ft	Bank-Height Ratio (BHR) (LBH/Max Riffle Depth)	start: _____ end: _____	
	Facet Slopes			Dimensionless Slope Ratios			Mean	Min	Max
	Riffle Slope ( $S_{rif}$ )	<b>0.0</b>		ft/ft	Riffle Slope/Average Water Surface Slope ( $S_{rif} / S$ )	<b>1.0</b>			
	Run Slope ( $S_{run}$ )			ft/ft	Run Slope/Average Water Surface Slope ( $S_{run} / S$ )				
	Pool Slope ( $S_p$ )			ft/ft	Pool Slope/Average Water Surface Slope ( $S_p / S$ )				
	Glide Slope ( $S_g$ )			ft/ft	Glide Slope/Average Water Surface Slope ( $S_g / S$ )				
	Feature Midpoint <sup>a</sup>			Dimensionless Depth Ratios			Mean	Min	Max
	Max Riffle Depth ( $d_{maxrif}$ )	<b>13.3</b>		ft	Max Riffle Depth/Mean Riffle Depth ( $d_{maxrif} / d_{bkt}$ )	<b>1.5</b>			
	Max Run Depth ( $d_{maxrun}$ )			ft	Max Run Depth/Mean Riffle Depth ( $d_{maxrun} / d_{bkt}$ )				
	Max Pool Depth ( $d_{maxp}$ )			ft	Max Pool Depth/Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )				
	Max Glide Depth ( $d_{maxg}$ )			ft	Max Glide Depth/Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )				

<b>Channel Materials</b>	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Protrusion Height <sup>d</sup>	
	% Silt/Clay	<b>53</b>			$D_{16}$	<b>&lt;.001</b>		mm
	% Sand	<b>47</b>			$D_{35}$	<b>0.0035</b>		mm
	% Gravel	<b>0</b>			$D_{50}$	<b>0.025</b>		mm
	% Cobble	<b>0</b>			$D_{84}$	<b>1.04</b>		mm
	% Boulder	<b>0</b>			$D_{95}$	<b>1.78</b>		mm
	% Bedrock	<b>0</b>			$D_{100}$	<b>2.2</b>		mm

<sup>a</sup> Min, max, mean depths are ave. mid-point values except pools: taken at deepest part of pool.

<sup>b</sup> Composite sample of riffles and pools within the designated reach.

<sup>c</sup> Active bed of a riffle.

<sup>d</sup> Height of roughness feature above bed.

**Summary....USGS GAGE STATION Data/Records for  
STREAM CHANNEL CLASSIFICATION**

Station NAME:	Red River - 6 - 470.23			Station Number:	N/A		
LOCATION:	Red River - 6 - 470.23						
Period of RECORD:	N/A		yrs	Mean Annual DISCHARGE:	N/A		cfs
Drainage AREA:	2298240	acres	3591	mi <sup>2</sup>	Drainage Area Mn ELEV:	869.48	ft
Reference REACH SLOPE:				ft/ft	Valley Type:	X	
Stream Type:	C6c-		HUC: _____				

**"BANKFULL" CHARACTERISTICS**

Determined from FIELD MEASUREMENT			Determined from GAGE DATA Analysis			
Bankfull WIDTH ( $W_{bkf}$ )	118.0	ft	Bankfull WIDTH ( $W_{bkf}$ )		ft	
Bankfull Mean DEPTH ( $d_{bkf}$ )	9.3	ft	Bankfull MEAN DEPTH ( $d_{bkf}$ )		ft	
Bankfull Xsec AREA ( $A_{bkf}$ )	1084.1	ft <sup>2</sup>	Bankfull Xsec AREA ( $A_{bkf}$ )		ft <sup>2</sup>	
Wetted PERIMETER ( $W_p$ )	124.0	ft	Wetted PERIMETER ( $W_p$ )		ft	
Bankfull STAGE (Gage Ht)		ft	Bankfull STAGE (Gage Ht)		ft	
Est. Mean VELOCITY ( $u$ )	1.7	ft/sec	Mean VELOCITY ( $u$ )		ft/sec	
Est. Bkf. DISCHARGE ( $Q_{bkf}$ )	1780.0	cfs	Bankfull DISCHARGE ( $Q_{bkf}$ )		cfs	
Bankfull DISCHARGE associated with "field-determined" Bankfull STAGE					1780.0	cfs
Recurrence Interval ( Log-Pearson ) associated with "field-determined" Bankfull Discharge					1.3	yrs

**From the Annual Peak Flow Frequency Analysis data for the Gage Station, determine:**

1.5 Year R.I. Discharge..... =	N/A	cfs	10 Year R.I. Discharge..... =	N/A	cfs
2.0 Year R.I. Discharge..... =	N/A	cfs	25 Year R.I. Discharge..... =	N/A	cfs
5.0 Year R.I. Discharge..... =	N/A	cfs	50 Year R.I. Discharge..... =	N/A	cfs

**MEANDER GEOMETRY**

Meander Length ( $L_m$ )	1310	ft	Radius of Curvature ( $R_C$ )	350.0	ft
Belt Width ( $W_{bit}$ )	1880	ft	Meander Width Ratio ( $W_{bit}/W_{bkf}$ )	15.9	ft/ft

**HYDRAULIC GEOMETRY**

Based on USGS Discharge Summary Notes data ( Form 9-207 ) and regression analyses of measured discharge ( $Q$ ) with the hydraulic parameters of Width ( $W$ ), Area ( $A$ ), Mean Depth ( $d$ ) & Mean Velocity ( $u$ ), determine the *intercept coefficient* ( $a$ ) and the *slope exponent* ( $b$ ) values for a power function of the form  $Y = aX^b$ , when  $Y$  is one of the selected hydraulic parameters and  $X$  is a given discharge value ( $Q$ ).

		Width ( $W$ )	Depth ( $d$ )	Area ( $A$ )	Velocity ( $u$ )
Intercept Coefficient:	( $a$ )				
Slope Exponent:	( $b$ )				

Hydraulic Radius: $R = A / W_p$		ft	Manning's "n" at Bankfull Stage	0.040	Coeff.
---------------------------------	--	----	---------------------------------	-------	--------

$$"n" = 1.4865 [ ( Area ) ( Hydraulic Radius^{2/3} ) ( Slope^{1/2} ) ] / Q_{bkf}$$

### Bankfull VELOCITY / DISCHARGE Estimates

Site	Red River			Location	Red River - 6 - 470.23											
Date	11/16/2010	Stream Type	C6c-	Valley Type	X											
Observers	KD, JB			HUC	0	9	0	2	0	1	0	4	0	5	0	1

INPUT VARIABLES				OUTPUT VARIABLES			
Bankfull Cross-sectional	1084.1	$A_{b\text{kf}}$ (ft <sup>2</sup> )		Bankfull Mean DEPTH	9.3	$D_{b\text{kf}}$ (ft)	
Bankfull WIDTH	118.0	$W_{b\text{kf}}$ (ft)		Wetted PERIMETER ~ 2 * $d_{b\text{kf}}$ + $W_{b\text{kf}}$	136.5	$W_p$ (ft)	
$D_{84}$ @ Riffle	0.0125	Dia. (mm)		$D_{84}$ mm / 304.8 =	0.0	$D_{84}$ (ft)	
Bankfull SLOPE	0.0001	$S_{b\text{kf}}$ (ft / ft)		Hydraulic RADIUS $A_{b\text{kf}} / W_p$	7.9	R (ft)	
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )		Relative Roughness R (ft) / $D_{84}$ (ft)	193627		
Drainage AREA	3591.0	DA (mi <sup>2</sup> )		Shear Velocity $u^* = \sqrt{gRS}$	0.2	$u^*$ (ft / sec)	

ESTIMATION METHODS	Bankfull VELOCITY		Bankfull DISCHARGE	
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 \text{Log} \{ R / D_{84} \} ] u^*$	6.2	ft / sec	6694	cfs
2. Roughness Coefficient: a) Manning's 'n' from friction factor / relative roughness (Figs. 2-18, 19) $u = 1.4865 * R^{2/3} * S^{1/2} / n$ $n =$ <input type="text"/>	1.7	ft / sec	1891	cfs
2. Roughness Coefficient: b) Manning's 'n' from Jarrett ( USGS ): $n = 0.39S^{-38R^{-16}}$ $n =$ <input type="text"/>	7.3	ft / sec	7893	cfs
Note: This equation is for applications involving steep, step-pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for stream types A1, A2, A3, B1, B2, B3, C2 and E3.				
2. Roughness Coefficient: c) Manning's 'n' from Stream Type $u = 1.4865 * R^{2/3} * S^{1/2} / n$ $n =$ <input type="text" value="0.04"/>	1.7	ft / sec	1891	cfs
3. Other Methods (Hev. Darcy-Weisbach, Chezy C, etc.) HEC-RAS	1.7	ft / sec	1780.0	cfs
3. Other Methods (Hev. Darcy-Weisbach, Chezy C, etc.) <input type="text"/>		ft / sec		cfs
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge $u = Q / A$ $Q =$ <input type="text" value="1.46"/> Yr.		ft / sec		cfs
4. Continuity Equations: b) USGS Gage Data $u = Q / A$		ft / sec		cfs

- Options for using the  $D_{84}$  term in the relative roughness relation ( $R/D_{84}$ ), when using estimation method 1.**
- Option 1. For **sand-bed** channels: Measure the "**protrusion height**" ( $h_{sd}$ ) of sand dunes above channel bed elevations. Substitute an average sand dune protrusion height ( $h_{sd}$  in ft) for the  $D_{84}$  term in est. method 1.
  - Option 2. For **boulder-dominated** channels: Measure several "**protrusion heights**" ( $h_{bo}$ ) of boulders above channel bed elevations. Substitute an ave. boulder protrusion height ( $h_{bo}$  in ft) for the  $D_{84}$  term in est. method 1.
  - Option 3. For **bedrock-dominated** channels: Measure several "**protrusion heights**" ( $h_{br}$ ) of rock separations/steps/joints/uplifted surfaces above channel bed elevations. Substitute an average bedrock protrusion height ( $h_{br}$  in feet) for the  $D_{84}$  term in estimation method 1.

Stream:	<b>Red River of the North</b>		
Basin:	<b>Red River Basin</b>	Drainage Area: <b>2298240</b> acres	<b>3591</b> mi <sup>2</sup>
Location:	<b>Red River - 6 - 470.23</b>		
Twp.&Rge: -	Sec.&Qtr.: -		
Cross-Section Monuments (Lat./Long.): -	Date: <b>11/16/2010</b>		
Observers: <b>KD, JB</b>	Valley Type: <b>X</b>		

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>118.0</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>9.3</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>1084.1</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>12.7</b>	ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>16.2</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>404.7</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>3.4</b>	ft/ft
<b>Channel Materials (Particle Size Index ) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>0.0017</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.00014</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).	<b>2.3</b>	

**Stream Type**

**C6c-**

**See Classification Key (Figure 2-21)**

Stream: **Red River of the North** Location: **RM66.89-66.07**

Observers: **KD, JB** Date: **11/16/2010** Valley Type: **X** Stream Type: **C6c-**

**River Reach Summary Data**

<b>Channel Dimension</b>	Mean Riffle Depth ( $d_{bkt}$ )	<b>9.3</b>	ft	Riffle Width ( $W_{bkt}$ )	<b>118.0</b>	ft	Riffle Area ( $A_{bkt}$ )	<b>1084.1</b>	ft <sup>2</sup>
	Mean Pool Depth ( $d_{bktp}$ )		ft	Pool Width ( $W_{bktp}$ )		ft	Pool Area ( $A_{bktp}$ )		ft <sup>2</sup>
	Mean Pool Depth/Mean Riffle Depth		$d_{bktp}/d_{bkt}$	Pool Width/Riffle Width		$W_{bktp}/W_{bkt}$	Pool Area / Riffle Area		$A_{bktp}/A_{bkt}$
	Max Riffle Depth ( $d_{maxrif}$ )	<b>16.2</b>	ft	Max Pool Depth ( $d_{maxp}$ )		ft	Max Riffle Depth/Mean Riffle Depth	<b>1.7</b>	
	Max Pool Depth/Mean Riffle Depth			Point Bar Slope		ft/ft	Inner Berm Width ( $W_{ib}$ )		ft
	Inner Berm Depth ( $d_{ib}$ )		ft	Inner Berm Width/Depth Ratio			$W_{ib}/d_{ib}$	Inner Berm Area ( $A_{ib}$ )	ft <sup>2</sup>
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )			<b>1.7</b>	ft/s	Estimation Method	<b>HEC-RAS</b>		
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )			<b>1780</b>	cfs	Drainage Area	<b>3591</b> mi <sup>2</sup>		

<b>Channel Pattern</b>	Geometry			Dimensionless Geometry Ratios			
	Mean	Min	Max	Mean	Min	Max	
	Meander Wavelength ( $L_m$ )	<b>1310</b>		ft	Meander Length Ratio ( $L_m/W_{bkt}$ )	<b>11.1</b>	
	Radius of Curvature ( $R_c$ )	<b>350</b>		ft	Radius of Curvature/Riffle Width ( $R_c/W_{bkt}$ )	<b>3.0</b>	
	Belt Width ( $W_{bit}$ )	<b>1880</b>		ft	Meander Width Ratio ( $W_{bit}/W_{bkt}$ )	<b>15.9</b>	
	Individual Pool Length			ft	Pool Length/Riffle Width		
	Pool to Pool Spacing			ft	Pool to Pool Spacing/Riffle Width		
Riffle Length			ft	Riffle Length/Riffle Width			

<b>Channel Profile</b>	Valley Slope (VS)		ft/ft	Average Water Surface Slope (S)		ft/ft	Sinuosity (VS/S)		
	Stream Length (SL)	<b>68433</b>	ft	Valley Length (VL)	<b>30431</b>	ft	Sinuosity (SL/VL)	<b>2.2</b>	
	Low Bank Height (LBH)	start: end:	ft	Max Riffle Depth	start: end:	ft	Bank-Height Ratio (BHR) (LBH/Max Riffle Depth)	start: end:	
	Facet Slopes			Dimensionless Slope Ratios			Mean	Min	Max
	Riffle Slope ( $S_{rif}$ )	<b>0.0</b>		ft/ft	Riffle Slope/Average Water Surface Slope ( $S_{rif} / S$ )	<b>1.0</b>			
	Run Slope ( $S_{run}$ )			ft/ft	Run Slope/Average Water Surface Slope ( $S_{run} / S$ )				
	Pool Slope ( $S_p$ )			ft/ft	Pool Slope/Average Water Surface Slope ( $S_p / S$ )				
	Glide Slope ( $S_g$ )			ft/ft	Glide Slope/Average Water Surface Slope ( $S_g / S$ )				
	Feature Midpoint <sup>a</sup>			Dimensionless Depth Ratios			Mean	Min	Max
	Max Riffle Depth ( $d_{maxrif}$ )	<b>16.2</b>		ft	Max Riffle Depth/Mean Riffle Depth ( $d_{maxrif} / d_{bkt}$ )	<b>1.7</b>			
	Max Run Depth ( $d_{maxrun}$ )			ft	Max Run Depth/Mean Riffle Depth ( $d_{maxrun} / d_{bkt}$ )				
	Max Pool Depth ( $d_{maxp}$ )			ft	Max Pool Depth/Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )				
Max Glide Depth ( $d_{maxg}$ )			ft	Max Glide Depth/Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )					

<b>Channel Materials</b>	Reach <sup>b</sup>			Riffle <sup>c</sup>			Bar			Protrusion Height <sup>d</sup>		
	% Silt/Clay	<b>95</b>			$D_{16}$	<b>&lt;.001</b>						mm
	% Sand	<b>5</b>			$D_{35}$	<b>&lt;.001</b>						mm
	% Gravel	<b>0</b>			$D_{50}$	<b>0.00165</b>						mm
	% Cobble	<b>0</b>			$D_{84}$	<b>0.0125</b>						mm
	% Boulder	<b>0</b>			$D_{95}$	<b>0.1125</b>						mm
	% Bedrock	<b>0</b>			$D_{100}$	<b>4.75</b>						mm

**Worksheet 2-1.** Gage station and field data (Rosgen and Silvey, 2007).

Summary.... <b>USGS GAGE STATION</b> Data/Records for <b>STREAM CHANNEL CLASSIFICATION</b>					
Station NAME:	Red River-5-463.56			Station Number:	N/A
LOCATION:	Red River-5-463.56				
Period of RECORD:	N/A	yrs	Mean Annual DISCHARGE:	N/A	cfs
Drainage AREA:	3585920	acres	5603	mi <sup>2</sup>	Drainage Area Mn ELEV: 864.46 ft
Reference REACH SLOPE:		ft/ft	Valley Type:	X	
Stream Type:	C6c-		HUC:	-- -- -- -- --	
"BANKFULL" CHARACTERISTICS					
Determined from FIELD MEASUREMENT			Determined from GAGE DATA Analysis		
Bankfull WIDTH ( $W_{bkf}$ )	143.1	ft	Bankfull WIDTH ( $W_{bkf}$ )		ft
Bankfull Mean DEPTH ( $d_{bkf}$ )	11.1	ft	Bankfull MEAN DEPTH ( $d_{bkf}$ )		ft
Bankfull Xsec AREA ( $A_{bkf}$ )	1581.4	ft <sup>2</sup>	Bankfull Xsec AREA ( $A_{bkf}$ )		ft <sup>2</sup>
Wetted PERIMETER ( $W_p$ )	149.3	ft	Wetted PERIMETER ( $W_p$ )		ft
Bankfull STAGE (Gage Ht)		ft	Bankfull STAGE (Gage Ht)		ft
Est. Mean VELOCITY ( $u$ )	1.5	ft/sec	Mean VELOCITY ( $u$ )		ft/sec
Est. Bkf. DISCHARGE ( $Q_{bkf}$ )	2380.0	cfs	Bankfull DISCHARGE ( $Q_{bkf}$ )		cfs
Bankfull DISCHARGE associated with "field-determined" Bankfull STAGE				2380.0	cfs
Recurrence Interval ( Log-Pearson ) associated with "field-determined" Bankfull Discharge				1.3	yrs
From the Annual Peak Flow Frequency Analysis data for the Gage Station, determine:					
1.5 Year R.I. Discharge..... =	N/A	cfs	10 Year R.I. Discharge..... =	N/A	cfs
2.0 Year R.I. Discharge..... =	N/A	cfs	25 Year R.I. Discharge..... =	N/A	cfs
5.0 Year R.I. Discharge..... =	N/A	cfs	50 Year R.I. Discharge..... =	N/A	cfs
MEANDER GEOMETRY					
Meander Length ( $L_m$ )	2449	ft	Radius of Curvature ( $R_C$ )	449.0	ft
Belt Width ( $W_{blt}$ )	1646	ft	Meander Width Ratio ( $W_{blt}/W_{bkf}$ )	11.5	ft/ft
HYDRAULIC GEOMETRY					
Based on USGS Discharge Summary Notes data ( Form 9-207 ) and regression analyses of measured discharge ( $Q$ ) with the hydraulic parameters of Width ( $W$ ), Area ( $A$ ), Mean Depth ( $d$ ) & Mean Velocity ( $u$ ), determine the <i>intercept coefficient</i> ( $a$ ) and the <i>slope exponent</i> ( $b$ ) values for a power function of the form $Y = aX^b$ , when $Y$ is one of the selected hydraulic parameters and $X$ is a given discharge value ( $Q$ ).					
	Width ( $W$ )	Depth ( $d$ )	Area ( $A$ )	Velocity ( $u$ )	
Intercept Coefficient: ( $a$ )					
Slope Exponent: ( $b$ )					
Hydraulic Radius: $R = A / W_p$		ft	Manning's "n" at Bankfull Stage	0.035	Coeff.
$"n" = 1.4865 [ ( Area ) ( Hydraulic Radius^{2/3} ) ( Slope^{1/2} ) ] / Q_{bkf}$					

**Worksheet 2-2.** Computations of velocity and bankfull discharge using various methods (Rosgen, 2006b; Rosgen and Silvey, 2007).

Bankfull VELOCITY / DISCHARGE Estimates										
Site	Red River-5-463.56				Location	Red River-5-463.56				
Date	10/6/2011	Stream Type	C6c-	Valley Type	X					
Observers	KD, JB				HUC	-- -- -- -- -- -- -- -- -- --				
INPUT VARIABLES				OUTPUT VARIABLES						
Bankfull Cross-sectional	1581.4	$A_{bkf}$ (ft <sup>2</sup> )		Bankfull Mean DEPTH	11.1	$D_{bkf}$ (ft)				
Bankfull WIDTH	143.1	$W_{bkf}$ (ft)		Wetted PERIMETER $\sim 2 * d_{bkf} + W_{bkf}$	165.2	$W_p$ (ft)				
$D_{84}$ @ Riffle	0.005	Dia. (mm)		$D_{84}$ mm / 304.8 =	0.00002	$D_{84}$ (ft)				
Bankfull SLOPE	0.00005	$S_{bkf}$ (ft / ft)		Hydraulic RADIUS $A_{bkf} / W_p$	9.6	R (ft)				
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )		Relative Roughness R (ft) / $D_{84}$ (ft)	583548					
Drainage AREA	5603.0	DA (mi <sup>2</sup> )		Shear Velocity $u^* = \sqrt{gRS}$	0.1	$u^*$ (ft / sec)				
ESTIMATION METHODS					Bankfull VELOCITY		Bankfull DISCHARGE			
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 \text{Log}\{ R / D_{84} \} ] u^*$					4.4	ft / sec	6884	cfs		
2. Roughness Coefficient: a) Manning's 'n' from friction factor / relative roughness (Figs. 2-18, 19) $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text"/>					1.3	ft / sec	2117	cfs		
2. Roughness Coefficient: b) Manning's 'n' from Jarrett ( USGS ): $n = 0.39S^{-.38R^{-.16}}$ n = <input type="text"/>					7.5	ft / sec	11853	cfs		
Note: This equation is for applications involving steep, step-pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for stream types A1, A2, A3, B1, B2, B3, C2 and E3.										
2. Roughness Coefficient: c) Manning's 'n' from Stream Type n = <input type="text" value="0.035"/>					1.3	ft / sec	2117	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.) HEC-RAS					1.5	ft / sec	2380	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.)						ft / sec		cfs		
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge Q = <input type="text" value="1.46"/> Yr. $u = Q / A$						ft / sec		cfs		
4. Continuity Equations: b) USGS Gage Data $u = Q / A$						ft / sec		cfs		
Options for using the $D_{84}$ term in the relative roughness relation (R/ $D_{84}$ ), when using estimation method 1.										
Option 1. For sand-bed channels: Measure the "protrusion height" ( $h_{sd}$ ) of sand dunes above channel bed elevations. Substitute an average sand dune protrusion height ( $h_{sd}$ in ft) for the $D_{84}$ term in est. method 1.										
Option 2. For boulder-dominated channels: Measure several "protrusion heights" ( $h_{bo}$ ) of boulders above channel bed elevations. Substitute an ave. boulder protrusion height ( $h_{bo}$ in ft) for the $D_{84}$ term in est. method 1.										
Option 3. For bedrock-dominated channels: Measure several "protrusion heights" ( $h_{br}$ ) of rock separations/steps/joints/ uplifted surfaces above channel bed elevations. Substitute an average bedrock protrusion height ( $h_{br}$ in feet) for the $D_{84}$ term in estimation method 1.										

**Worksheet 2-3.** Field form for Level II stream classification (Rosgen, 1996; Rosgen , 2006b).

Stream: <b>Red River-5-463.56</b>	
Basin: <b>Red River Basin</b>	Drainage Area: <b>4E+06</b> acres <b>5603</b> mi <sup>2</sup>
Location: <b>Red River-5-463.56</b>	
Twp.&Rge: -	Sec.&Qtr.: -
Cross-Section Monuments (Lat./Long.): -	Date: <b>10/6/2011</b>
Observers: <b>KD, JB</b>	Valley Type: <b>X</b>

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>143.1</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>11.1</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>1581.4</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>12.9</b>	ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>17.6</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>949.0</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>6.6</b>	ft/ft
<b>Channel Materials (Particle Size Index ) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>0.001</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.000049</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).	<b>2.4</b>	

<b>Stream Type</b>	<b>C6c-</b>	<b>See Classification Key (Figure 2-21)</b>
--------------------	-------------	---

**Worksheet 2-4.** Morphological relations, including dimensionless ratios of river reach sites (Rosgen, 2006b; Rosgen and Silvey 2007).

Stream: <b>Red River-5-463.56</b>		Location: <b>Red River-5-463.56</b>								
Observers: <b>KD, JB</b>		Date: <b>10/6/2011</b>		Valley Type: <b>X</b>		Stream Type: <b>C6c-</b>				
River Reach Summary Data										
Channel Dimension	Mean Riffle Depth ( $d_{bkt}$ )	<b>11.1</b>	ft	Riffle Width ( $W_{bkt}$ )	<b>143.1</b>	ft	Riffle Area ( $A_{bkt}$ )	<b>1581.4</b>	ft <sup>2</sup>	
	Mean Pool Depth ( $d_{bkfp}$ )		ft	Pool Width ( $W_{bkfp}$ )		ft	Pool Area ( $A_{bkfp}$ )		ft <sup>2</sup>	
	Mean Pool Depth/Mean Riffle Depth		$d_{bkfp}/d_{bkt}$	Pool Width/Riffle Width		$W_{bkfp}/W_{bkt}$	Pool Area / Riffle Area		$A_{bkfp}/A_{bkt}$	
	Max Riffle Depth ( $d_{maxrif}$ )	<b>17.6</b>	ft	Max Pool Depth ( $d_{maxp}$ )		ft	Max Riffle Depth/Mean Riffle Depth	<b>1.6</b>		
	Max Pool Depth/Mean Riffle Depth			Point Bar Slope		ft/ft	Inner Berm Width ( $W_{ib}$ )		ft	
	Inner Berm Depth ( $d_{ib}$ )		ft	Inner Berm Width/Depth Ratio			$W_{ib}/d_{ib}$	Inner Berm Area ( $A_{ib}$ )		ft <sup>2</sup>
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )				<b>1.5</b>	ft/s	Estimation Method		<b>HEC-RAS</b>	
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )				<b>2380</b>	cfs	Drainage Area		<b>5603</b>	mi <sup>2</sup>

Channel Pattern	Geometry			Dimensionless Geometry Ratios			
	Mean	Min	Max	Mean	Min	Max	
	Meander Wavelength ( $L_m$ )	<b>2449</b>			ft	Meander Length Ratio ( $L_m/W_{bkt}$ )	<b>17.1</b>
	Radius of Curvature ( $R_c$ )	<b>449</b>			ft	Radius of Curvature/Riffle Width ( $R_c/W_{bkt}$ )	<b>3.1</b>
	Belt Width ( $W_{bit}$ )	<b>1646</b>			ft	Meander Width Ratio ( $W_{bit}/W_{bkt}$ )	<b>11.5</b>
	Individual Pool Length				ft	Pool Length/Riffle Width	
	Pool to Pool Spacing				ft	Pool to Pool Spacing/Riffle Width	
Riffle Length				ft	Riffle Length/Riffle Width		

Channel Profile	Valley Slope (VS)		ft/ft	Average Water Surface Slope (S)		ft/ft	Sinuosity (VS/S)		
	Stream Length (SL)	<b>66116</b>	ft	Valley Length (VL)	<b>27371</b>	ft	Sinuosity (SL/VL)	<b>2.4</b>	
	Low Bank Height (LBH)	start	ft	Max Riffle Depth	start	ft	Bank-Height Ratio (BHR)	start	
		end	ft		end	ft	(LBH/Max Riffle Depth)	end	
	Facet Slopes			Dimensionless Slope Ratios			Mean	Min	Max
	Riffle Slope ( $S_{rif}$ )	<b>0.0</b>		ft/ft	Riffle Slope/Average Water Surface Slope ( $S_{rif}/S$ )	<b>1.0</b>			
	Run Slope ( $S_{run}$ )			ft/ft	Run Slope/Average Water Surface Slope ( $S_{run}/S$ )				
	Pool Slope ( $S_p$ )			ft/ft	Pool Slope/Average Water Surface Slope ( $S_p/S$ )				
	Glide Slope ( $S_g$ )			ft/ft	Glide Slope/Average Water Surface Slope ( $S_g/S$ )				
	Feature Midpoint <sup>a</sup>			Dimensionless Depth Ratios			Mean	Min	Max
	Max Riffle Depth ( $d_{maxrif}$ )	<b>17.6</b>		ft	Max Riffle Depth/Mean Riffle Depth ( $d_{maxrif}/d_{bkt}$ )	<b>1.6</b>			
	Max Run Depth ( $d_{maxrun}$ )			ft	Max Run Depth/Mean Riffle Depth ( $d_{maxrun}/d_{bkt}$ )				
	Max Pool Depth ( $d_{maxp}$ )			ft	Max Pool Depth/Mean Riffle Depth ( $d_{maxp}/d_{bkt}$ )				
Max Glide Depth ( $d_{maxg}$ )			ft	Max Glide Depth/Mean Riffle Depth ( $d_{maxg}/d_{bkt}$ )					

Channel Materials	Reach <sup>b</sup>		Riffle <sup>c</sup>	Bar	Reach <sup>b</sup>		Riffle <sup>c</sup>	Bar	Protrusion Height <sup>d</sup>	
	% Silt/Clay	<b>100</b>			$D_{16}$	<b>&lt;.001</b>				mm
	% Sand	<b>0</b>			$D_{35}$	<b>&lt;.001</b>				mm
	% Gravel	<b>0</b>			$D_{50}$	<b>0.001</b>				mm
	% Cobble	<b>0</b>			$D_{84}$	<b>0.005</b>				mm
	% Boulder	<b>0</b>			$D_{95}$	<b>0.0095</b>				mm
	% Bedrock	<b>0</b>			$D_{100}$	<b>0.12</b>				mm

<sup>a</sup> Min, max, mean depths are ave. mid-point values except pools: taken at deepest part of pool.

<sup>b</sup> Composite sample of riffles and pools within the designated reach.

<sup>c</sup> Active bed of a riffle.

<sup>d</sup> Height of roughness feature above bed.

Summary.... **USGS GAGE STATION** Data/Records for  
**STREAM CHANNEL CLASSIFICATION**

Station NAME:	Red River at Fargo, ND			Station Number:	N/A		
LOCATION:	Red River - 4 - 452.52						
Period of RECORD:	N/A		yr/s	Mean Annual DISCHARGE:	N/A		cfs
Drainage AREA:	3659520	acres	5718	mi <sup>2</sup>	Drainage Area Mn ELEV:	862.9	ft
Reference REACH SLOPE:			ft/ft	Valley Type:	X		
Stream Type:	C6c-		HUC: _____				

**"BANKFULL" CHARACTERISTICS**

Determined from FIELD MEASUREMENT			Determined from GAGE DATA Analysis			
Bankfull WIDTH ( $W_{bkf}$ )	159.5	ft	Bankfull WIDTH ( $W_{bkf}$ )		ft	
Bankfull Mean DEPTH ( $d_{bkf}$ )	10.3	ft	Bankfull MEAN DEPTH ( $d_{bkf}$ )		ft	
Bankfull Xsec AREA ( $A_{bkf}$ )	1633.0	ft <sup>2</sup>	Bankfull Xsec AREA ( $A_{bkf}$ )		ft <sup>2</sup>	
Wetted PERIMETER ( $W_p$ )	164.4	ft	Wetted PERIMETER ( $W_p$ )		ft	
Bankfull STAGE (Gage Ht)		ft	Bankfull STAGE (Gage Ht)		ft	
Est. Mean VELOCITY ( $u$ )	1.5	ft/sec	Mean VELOCITY ( $u$ )		ft/sec	
Est. Bkf. DISCHARGE ( $Q_{bkf}$ )	2380.0	cfs	Bankfull DISCHARGE ( $Q_{bkf}$ )		cfs	
Bankfull DISCHARGE associated with "field-determined" Bankfull STAGE					2380.0	cfs
Recurrence Interval ( Log-Pearson ) associated with "field-determined" Bankfull Discharge					1.26	yr/s

From the **Annual Peak Flow Frequency Analysis** data for the Gage Station, determine:

1.5 Year R.I. Discharge..... =	N/A	cfs	10 Year R.I. Discharge..... =	N/A	cfs
2.0 Year R.I. Discharge..... =	N/A	cfs	20 Year R.I. Discharge..... =	N/A	cfs
5.0 Year R.I. Discharge..... =	N/A	cfs	50 Year R.I. Discharge..... =	N/A	cfs

**MEANDER GEOMETRY**

Meander Length ( $L_m$ )	2750	ft	Radius of Curvature ( $R_C$ )	581.0	ft
Belt Width ( $W_{blt}$ )	1890	ft	Meander Width Ratio ( $W_{blt}/W_{bkf}$ )	11.85	ft/ft

**HYDRAULIC GEOMETRY**

Based on *USGS Discharge Summary Notes* data ( Form 9-207 ) and regression analyses of measured discharge ( $Q$ ) with the hydraulic parameters of Width ( $W$ ), Area ( $A$ ), Mean Depth ( $d$ ) & Mean Velocity ( $u$ ), determine the *intercept coefficient* ( $a$ ) and the *slope exponent* ( $b$ ) values for a power function of the form  $Y = aX^b$ , when  $Y$  is one of the selected hydraulic parameters and  $X$  is a given discharge value ( $Q$ ).

	Width ( $W$ )	Depth ( $d$ )	Area ( $A$ )	Velocity ( $u$ )
Intercept Coefficient: ( $a$ )				
Slope Exponent: ( $b$ )				

**Hydraulic Radius:**  $R = A / W_p$  \_\_\_\_\_ ft      **Manning's "n" at Bankfull Stage** **0.035** Coeff.

$$"n" = 1.4865 [ ( Area ) ( Hydraulic Radius^{2/3} ) ( Slope^{1/2} ) ] / Q_{bkf}$$

### Bankfull VELOCITY / DISCHARGE Estimates

Site	Red River	Location	Red River - 4 - 452.52												
Date	11/16/2010	Stream Type	C6c-	Valley Type	X										
Observers	KD, JB		HUC	0	9	0	2	0	1	0	4	0	5	0	6

INPUT VARIABLES			OUTPUT VARIABLES		
Bankfull Cross-sectional AREA	1633.0	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Mean DEPTH	10.3	$D_{bkf}$ (ft)
Bankfull WIDTH	159.5	$W_{bkf}$ (ft)	Wetted PERIMETER $\sim 2 * d_{bkf} + W_{bkf}$	180.1	$W_p$ (ft)
$D_{84}$ @ Riffle	0.6	Dia. (mm)	$D_{84}$ mm / 304.8 =	0.002	$D_{84}$ (ft)
Bankfull SLOPE	0.0002	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	9.1	R (ft)
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R (ft) / $D_{84}$ (ft)	4685	
Drainage AREA	5718.0	DA (mi <sup>2</sup> )	Shear Velocity $u^* = \sqrt{gRS}$	0.2	$u^*$ (ft / sec)

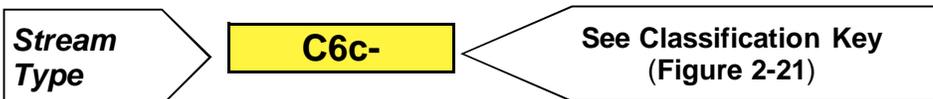
ESTIMATION METHODS	Bankfull VELOCITY		Bankfull	
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 \text{Log} \{ R / D_{84} \} ] u^*$	5.3	ft / sec	8589	cfs
2. Roughness Coefficient: a) Manning's 'n' from friction factor / relative roughness (Figs. 2-18, 19) $u = 1.4865 * R^{2/3} * S^{1/2} / n$ $n =$ <input type="text"/>	2.4	ft / sec	3932	cfs
2. Roughness Coefficient: b) Manning's 'n' from Jarrett ( USGS ): $n = 0.39S^{-3.8R^{-1.6}}$ $n =$ <input type="text"/> <small>Note: This equation is for applications involving steep, step-pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for stream types A1, A2, A3, B1, B2, B3, C2 and E3.</small>	8.3	ft / sec	13593	cfs
2. Roughness Coefficient: c) Manning's 'n' from Stream Type $u = 1.4865 * R^{2/3} * S^{1/2} / n$ $n =$ <input type="text" value="0.035"/>	2.4	ft / sec	3932	cfs
3. Other Methods (Hvy. Darcy-Weisbach, Chezy C, etc.) HEC-RAS	1.5	ft / sec	2380	cfs
3. Other Methods (Hvy. Darcy-Weisbach, Chezy C, etc.) <input type="text"/>		ft / sec		cfs
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge $Q =$ <input type="text" value="1.46"/> Yr. $u = Q / A$		ft / sec		cfs
4. Continuity Equations: b) USGS Gage Data $u = Q / A$		ft / sec		cfs

#### Options for using the $D_{84}$ term in the relative roughness relation ( $R/D_{84}$ ), when using estimation method 1.

- Option 1. For **sand-bed** channels: Measure the "**protrusion height**" ( $h_{sd}$ ) of sand dunes above channel bed elevations. Substitute an average sand dune protrusion height ( $h_{sd}$  in ft) for the  $D_{84}$  term in est. method 1.
- Option 2. For **boulder-dominated** channels: Measure several "**protrusion heights**" ( $h_{bo}$ ) of boulders above channel bed elevations. Substitute an ave. boulder protrusion height ( $h_{bo}$  in ft) for the  $D_{84}$  term in est. method 1.
- Option 3. For **bedrock-dominated** channels: Measure several "**protrusion heights**" ( $h_{br}$ ) of rock separations/steps/joints/uplifted surfaces above channel bed elevations. Substitute an average bedrock protrusion height ( $h_{br}$  in feet) for the  $D_{84}$  term in estimation method 1.

Stream:	<b>Red River</b>		
Basin:	<b>Red River Basin</b>	Drainage Area: <b>3659520</b> acres	<b>5718</b> mi <sup>2</sup>
Location:	<b>Red River - 4 - 452.52</b>		
Twp.&Rge: -	Sec.&Qtr.: -		
Cross-Section Monuments (Lat./Long.): -	Date: <b>11/16/2010</b>		
Observers: <b>KD, JB</b>	Valley Type: <b>X</b>		

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>159.5</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>10.3</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>1633.0</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>15.5</b>	ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>15.0</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{pa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>709</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{pa} / W_{bkf}$ ) (riffle section).	<b>4.4</b>	ft/ft
<b>Channel Materials (Particle Size Index ) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>0.0027</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.00017</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).	<b>2.2</b>	



Stream: **Red River** Location: **Red River - 4 - 452.52**  
 Observers: **KD, JB** Date: **11/16/2010** Valley Type: **X** Stream Type: **C6c-**

**River Reach Summary Data**

<b>Channel Dimension</b>	Mean Riffle Depth ( $d_{bkt}$ )	<b>10.3</b>	ft	Riffle Width ( $W_{bkt}$ )	<b>159.5</b>	ft	Riffle Area ( $A_{bkt}$ )	<b>1633.0</b>	ft <sup>2</sup>	
	Mean Pool Depth ( $d_{bkfp}$ )		ft	Pool Width ( $W_{bkfp}$ )		ft	Pool Area ( $A_{bkfp}$ )		ft <sup>2</sup>	
	Mean Pool Depth/Mean Riffle Depth		$d_{bkfp}/d_{bkt}$	Pool Width/Riffle Width		$W_{bkfp}/W_{bkt}$	Pool Area / Riffle Area		$A_{bkfp}/A_{bkt}$	
	Max Riffle Depth ( $d_{maxrif}$ )	<b>15.0</b>	ft	Max Pool Depth ( $d_{maxp}$ )		ft	Max Riffle Depth/Mean Riffle Depth	<b>1.5</b>		
	Max Pool Depth/Mean Riffle Depth			Point Bar Slope		ft/ft	Inner Berm Width ( $W_{ib}$ )		ft	
	Inner Berm Depth ( $d_b$ )		ft	Inner Berm Width/Depth Ratio			$W_{ib}/d_b$	Inner Berm Area ( $A_b$ )		ft <sup>2</sup>
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $\psi_{kt}$ )			<b>1.5</b>	ft/s	Estimation Method	<b>HEC-RAS</b>			
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )			<b>2380</b>	cfs	Drainage Area	<b>5718</b>			mi <sup>2</sup>

<b>Channel Pattern</b>	<b>Geometry</b>			<b>Dimensionless Geometry Ratios</b>					
		Mean	Min	Max		Mean	Min	Max	
	Meander Wavelength ( $L_m$ )	<b>2750</b>			ft	Meander Length Ratio ( $L_m/W_{bkt}$ )	<b>17.2</b>		
	Radius of Curvature ( $R_c$ )	<b>581</b>			ft	Radius of Curvature/Riffle Width ( $R_c/W_{bkt}$ )	<b>3.6</b>		
	Belt Width ( $W_{bit}$ )	<b>1890</b>			ft	Meander Width Ratio ( $W_{bit}/W_{bkt}$ )	<b>11.9</b>		
	Individual Pool Length				ft	Pool Length/Riffle Width			
	Pool to Pool Spacing				ft	Pool to Pool Spacing/Riffle Width			
Riffle Length				ft	Riffle Length/Riffle Width				

<b>Channel Profile</b>	Valley Slope (VS)		ft/ft	Average Water Surface Slope (S)		ft/ft	Sinuosity (VS/S)		
	Stream Length (SL)	<b>48061</b>	ft	Valley Length (VL)	<b>22157</b>	ft	Sinuosity (SL/VL)	<b>2.2</b>	
	Low Bank Height (LBH)	start: _____ end: _____	ft	Max Riffle Depth	start: _____ end: _____	ft	Bank-Height Ratio (BHR) (LBH/Max Riffle Depth)	start: _____ end: _____	
	<b>Facet Slopes</b>			<b>Dimensionless Slope Ratios</b>			Mean	Min	Max
	Riffle Slope ( $S_{rif}$ )	<b>0.0</b>		ft/ft	Riffle Slope/Average Water Surface Slope ( $S_{rif} / S$ )	<b>1.0</b>			
	Run Slope ( $S_{run}$ )			ft/ft	Run Slope/Average Water Surface Slope ( $S_{run} / S$ )				
	Pool Slope ( $S_p$ )			ft/ft	Pool Slope/Average Water Surface Slope ( $S_p / S$ )				
	Glide Slope ( $S_g$ )			ft/ft	Glide Slope/Average Water Surface Slope ( $S_g / S$ )				
	<b>Feature Midpoint<sup>a</sup></b>			<b>Dimensionless Depth Ratios</b>			Mean	Min	Max
	Max Riffle Depth ( $d_{maxrif}$ )	<b>15.0</b>		ft	Max Riffle Depth/Mean Riffle Depth ( $d_{maxrif} / d_{bkt}$ )	<b>1.5</b>			
Max Run Depth ( $d_{maxrun}$ )			ft	Max Run Depth/Mean Riffle Depth ( $d_{maxrun} / d_{bkt}$ )					
Max Pool Depth ( $d_{maxp}$ )			ft	Max Pool Depth/Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )					
Max Glide Depth ( $d_{maxg}$ )			ft	Max Glide Depth/Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )					

<b>Channel Materials</b>	<b>Reach<sup>b</sup></b>			<b>Riffle<sup>c</sup></b>			<b>Bar</b>			<b>Protrusion Height<sup>d</sup></b>		
	% Silt/Clay	<b>77</b>			$D_{16}$	<b>&lt;.001</b>						mm
	% Sand	<b>23</b>			$D_{35}$	<b>&lt;.001</b>						mm
	% Gravel	<b>0</b>			$D_{50}$	<b>0.0027</b>						mm
	% Cobble	<b>0</b>			$D_{84}$	<b>0.59</b>						mm
	% Boulder	<b>0</b>			$D_{95}$	<b>1.39</b>						mm
	% Bedrock	<b>0</b>			$D_{100}$	<b>2</b>						mm

**Worksheet 2-1.** Gage station and field data (Rosgen and Silvey, 2007).

Summary.... <b>USGS GAGE STATION</b> Data/Records for <b>STREAM CHANNEL CLASSIFICATION</b>					
Station NAME:	Red River-3-440.57			Station Number:	N/A
LOCATION:	Red River-3-440.57				
Period of RECORD:	N/A	yrs	Mean Annual DISCHARGE:	N/A	cfs
Drainage AREA:	3688320	acres	5763	mi <sup>2</sup>	Drainage Area Mn ELEV: 856.05 ft
Reference REACH SLOPE:		ft/ft	Valley Type:	X	
Stream Type:	C6c-		HUC:	-- -- -- -- -- -- -- -- -- --	
"BANKFULL" CHARACTERISTICS					
Determined from FIELD MEASUREMENT			Determined from GAGE DATA Analysis		
Bankfull WIDTH ( $W_{bkf}$ )	136.0	ft	Bankfull WIDTH ( $W_{bkf}$ )		ft
Bankfull Mean DEPTH ( $d_{bkf}$ )	9.8	ft	Bankfull MEAN DEPTH ( $d_{bkf}$ )		ft
Bankfull Xsec AREA ( $A_{bkf}$ )	1333.7	ft <sup>2</sup>	Bankfull Xsec AREA ( $A_{bkf}$ )		ft <sup>2</sup>
Wetted PERIMETER ( $W_p$ )	141.1	ft	Wetted PERIMETER ( $W_p$ )		ft
Bankfull STAGE (Gage Ht)		ft	Bankfull STAGE (Gage Ht)		ft
Est. Mean VELOCITY ( $u$ )	1.8	ft/sec	Mean VELOCITY ( $u$ )		ft/sec
Est. Bkf. DISCHARGE ( $Q_{bkf}$ )	2380.0	cfs	Bankfull DISCHARGE ( $Q_{bkf}$ )		cfs
Bankfull DISCHARGE associated with "field-determined" Bankfull STAGE				2380.0	cfs
Recurrence Interval ( Log-Pearson ) associated with "field-determined" Bankfull Discharge				1.3	yrs
From the Annual Peak Flow Frequency Analysis data for the Gage Station, determine:					
1.5 Year R.I. Discharge..... =	N/A	cfs	10 Year R.I. Discharge..... =	N/A	cfs
2.0 Year R.I. Discharge..... =	N/A	cfs	25 Year R.I. Discharge..... =	N/A	cfs
5.0 Year R.I. Discharge..... =	N/A	cfs	50 Year R.I. Discharge..... =	N/A	cfs
MEANDER GEOMETRY					
Meander Length ( $L_m$ )	1901	ft	Radius of Curvature ( $R_C$ )	280.0	ft
Belt Width ( $W_{blt}$ )	2945	ft	Meander Width Ratio ( $W_{blt}/W_{bkf}$ )	21.7	ft/ft
HYDRAULIC GEOMETRY					
Based on USGS Discharge Summary Notes data ( Form 9-207 ) and regression analyses of measured discharge ( $Q$ ) with the hydraulic parameters of Width ( $W$ ), Area ( $A$ ), Mean Depth ( $d$ ) & Mean Velocity ( $u$ ), determine the <i>intercept coefficient</i> ( $a$ ) and the <i>slope exponent</i> ( $b$ ) values for a power function of the form $Y = aX^b$ , when $Y$ is one of the selected hydraulic parameters and $X$ is a given discharge value ( $Q$ ).					
	Width ( $W$ )	Depth ( $d$ )	Area ( $A$ )	Velocity ( $u$ )	
Intercept Coefficient: ( $a$ )					
Slope Exponent: ( $b$ )					
Hydraulic Radius: $R = A / W_p$		ft	Manning's "n" at Bankfull Stage	0.03	Coeff.
$"n" = 1.4865 [ ( Area ) ( Hydraulic Radius^{2/3} ) ( Slope^{1/2} ) ] / Q_{bkf}$					

**Worksheet 2-2.** Computations of velocity and bankfull discharge using various methods (Rosgen, 2006b; Rosgen and Silvey, 2007).

Bankfull VELOCITY / DISCHARGE Estimates										
Site	Red River-3-440.57				Location	Red River-3-440.57				
Date	10/4/2011	Stream Type	C6c-	Valley Type	X					
Observers	KD, JB				HUC	-- -- -- -- -- -- -- -- -- --				
INPUT VARIABLES				OUTPUT VARIABLES						
Bankfull Cross-sectional	1333.7	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Mean DEPTH	9.8	$D_{bkf}$ (ft)					
Bankfull WIDTH	136.0	$W_{bkf}$ (ft)	Wetted PERIMETER ~ 2 * $d_{bkf}$ + $W_{bkf}$	155.6	$W_p$ (ft)					
$D_{84}$ @ Riffle	0.11	Dia. (mm)	$D_{84}$ mm / 304.8 =	0.0	$D_{84}$ (ft)					
Bankfull SLOPE	0.0001	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	8.6	R (ft)					
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R (ft) / $D_{84}$ (ft)	23752						
Drainage AREA	5763.0	DA (mi <sup>2</sup> )	Shear Velocity $u^* = \sqrt{gRS}$	0.1	$u^*$ (ft / sec)					
ESTIMATION METHODS				Bankfull VELOCITY		Bankfull DISCHARGE				
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 \text{Log}\{ R / D_{84} \} ] u^*$				3.8	ft / sec	5026	cfs			
2. Roughness Coefficient: a) Manning's 'n' from friction factor / relative roughness (Figs. 2-18, 19) $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text"/>				1.7	ft / sec	2275	cfs			
2. Roughness Coefficient: b) Manning's 'n' from Jarrett ( USGS ): $n = 0.39S^{-.38}R^{-.16}$ n = <input type="text"/> Note: This equation is for applications involving steep, step-pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for stream types A1, A2, A3, B1, B2, B3, C2 and E3.				7.1	ft / sec	9485	cfs			
2. Roughness Coefficient: c) Manning's 'n' from Stream Type $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text" value="0.03"/>				1.7	ft / sec	2275	cfs			
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.) HEC-RAS				1.8	ft / sec	2380	cfs			
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.)					ft / sec		cfs			
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge $Q = 1.46$ Yr. $u = Q / A$					ft / sec		cfs			
4. Continuity Equations: b) USGS Gage Data $u = Q / A$					ft / sec		cfs			
Options for using the $D_{84}$ term in the relative roughness relation ( $R/D_{84}$ ), when using estimation method 1.										
Option 1. For sand-bed channels: Measure the "protrusion height" ( $h_{sd}$ ) of sand dunes above channel bed elevations. Substitute an average sand dune protrusion height ( $h_{sd}$ in ft) for the $D_{84}$ term in est. method 1.										
Option 2. For boulder-dominated channels: Measure several "protrusion heights" ( $h_{bo}$ ) of boulders above channel bed elevations. Substitute an ave. boulder protrusion height ( $h_{bo}$ in ft) for the $D_{84}$ term in est. method 1.										
Option 3. For bedrock-dominated channels: Measure several "protrusion heights" ( $h_{br}$ ) of rock separations/steps/joints/uplifted surfaces above channel bed elevations. Substitute an average bedrock protrusion height ( $h_{br}$ in feet) for the $D_{84}$ term in estimation method 1.										

**Worksheet 2-3.** Field form for Level II stream classification (Rosgen, 1996; Rosgen , 2006b).

Stream: <b>Red River-3-440.57</b>	
Basin: <b>Red River Basin</b>	Drainage Area: <b>4E+06</b> acres <b>5763</b> mi <sup>2</sup>
Location: <b>Red River-3-440.57</b>	
Twp.&Rge: -	Sec.&Qtr.: -
Cross-Section Monuments (Lat./Long.): -	Date: <b>10/4/2011</b>
Observers: <b>KD, JB</b>	Valley Type: <b>X</b>

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>136.0</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>9.8</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>1333.7</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>13.9</b>	ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>13.5</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>619.3</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>4.6</b>	ft/ft
<b>Channel Materials (Particle Size Index ) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>0.026</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.000068</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).	<b>2.2</b>	

<b>Stream Type</b>	<b>C6c-</b>	<b>See Classification Key (Figure 2-21)</b>
--------------------	-------------	---

**Worksheet 2-4.** Morphological relations, including dimensionless ratios of river reach sites (Rosgen, 2006b; Rosgen and Silvey 2007).

Stream: <b>Red River-3-440.57</b>		Location: <b>Red River-3-440.57</b>								
Observers: <b>KD, JB</b>		Date: <b>10/4/2011</b>		Valley Type: <b>X</b>		Stream Type: <b>C6c-</b>				
<b>River Reach Summary Data</b>										
<b>Channel Dimension</b>	Mean Riffle Depth ( $d_{bkt}$ )	<b>9.8</b>	ft	Riffle Width ( $W_{bkt}$ )	<b>136.0</b>	ft	Riffle Area ( $A_{bkt}$ )	<b>1333.7</b>	ft <sup>2</sup>	
	Mean Pool Depth ( $d_{bkfp}$ )		ft	Pool Width ( $W_{bkfp}$ )		ft	Pool Area ( $A_{bkfp}$ )		ft <sup>2</sup>	
	Mean Pool Depth/Mean Riffle Depth		$d_{bkfp}/d_{bkt}$	Pool Width/Riffle Width		$W_{bkfp}/W_{bkt}$	Pool Area / Riffle Area		$A_{bkfp}/A_{bkt}$	
	Max Riffle Depth ( $d_{maxrif}$ )	<b>13.5</b>	ft	Max Pool Depth ( $d_{maxp}$ )		ft	Max Riffle Depth/Mean Riffle Depth	<b>1.4</b>		
	Max Pool Depth/Mean Riffle Depth			Point Bar Slope		ft/ft	Inner Berm Width ( $W_{ib}$ )		ft	
	Inner Berm Depth ( $d_{ib}$ )		ft	Inner Berm Width/Depth Ratio			$W_{ib}/d_{ib}$	Inner Berm Area ( $A_{ib}$ )		ft <sup>2</sup>
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )				<b>1.8</b>	ft/s	Estimation Method		<b>HEC-RAS</b>	
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )				<b>2380</b>	cfs	Drainage Area		<b>5763</b>	mi <sup>2</sup>

<b>Channel Pattern</b>	Geometry			Dimensionless Geometry Ratios			
	Mean	Min	Max	Mean	Min	Max	
	Meander Wavelength ( $L_m$ )	<b>1901</b>			ft	Meander Length Ratio ( $L_m/W_{bkt}$ )	<b>14.0</b>
	Radius of Curvature ( $R_c$ )	<b>280</b>			ft	Radius of Curvature/Riffle Width ( $R_c/W_{bkt}$ )	<b>2.1</b>
	Belt Width ( $W_{bit}$ )	<b>2945</b>			ft	Meander Width Ratio ( $W_{bit}/W_{bkt}$ )	<b>21.7</b>
	Individual Pool Length				ft	Pool Length/Riffle Width	
	Pool to Pool Spacing				ft	Pool to Pool Spacing/Riffle Width	
Riffle Length				ft	Riffle Length/Riffle Width		

<b>Channel Profile</b>	Valley Slope (VS)		ft/ft	Average Water Surface Slope (S)		ft/ft	Sinuosity (VS/S)		
	Stream Length (SL)	<b>108377</b>	ft	Valley Length (VL)	<b>50295</b>	ft	Sinuosity (SL/VL)	<b>2.2</b>	
	Low Bank Height (LBH)	start: _____ end: _____	ft	Max Riffle Depth	start: _____ end: _____	ft	Bank-Height Ratio (BHR) (LBH/Max Riffle Depth)	start: _____ end: _____	
	Facet Slopes			Dimensionless Slope Ratios			Mean	Min	Max
	Riffle Slope ( $S_{rif}$ )	<b>0.0</b>		ft/ft	Riffle Slope/Average Water Surface Slope ( $S_{rif} / S$ )	<b>1.0</b>			
	Run Slope ( $S_{run}$ )			ft/ft	Run Slope/Average Water Surface Slope ( $S_{run} / S$ )				
	Pool Slope ( $S_p$ )			ft/ft	Pool Slope/Average Water Surface Slope ( $S_p / S$ )				
	Glide Slope ( $S_g$ )			ft/ft	Glide Slope/Average Water Surface Slope ( $S_g / S$ )				
	Feature Midpoint <sup>a</sup>			Dimensionless Depth Ratios			Mean	Min	Max
	Max Riffle Depth ( $d_{maxrif}$ )	<b>13.5</b>		ft	Max Riffle Depth/Mean Riffle Depth ( $d_{maxrif} / d_{bkt}$ )	<b>1.4</b>			
	Max Run Depth ( $d_{maxrun}$ )			ft	Max Run Depth/Mean Riffle Depth ( $d_{maxrun} / d_{bkt}$ )				
	Max Pool Depth ( $d_{maxp}$ )			ft	Max Pool Depth/Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )				
Max Glide Depth ( $d_{maxg}$ )			ft	Max Glide Depth/Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )					

<b>Channel Materials</b>	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Protrusion Height <sup>d</sup>	
	% Silt/Clay	<b>83</b>			$D_{16}$	<b>0.0125</b>		mm
	% Sand	<b>15</b>			$D_{35}$	<b>0.023</b>		mm
	% Gravel	<b>2</b>			$D_{50}$	<b>0.026</b>		mm
	% Cobble	<b>0</b>			$D_{84}$	<b>0.11</b>		mm
	% Boulder	<b>0</b>			$D_{95}$	<b>1.9</b>		mm
	% Bedrock	<b>0</b>			$D_{100}$	<b>9.5</b>		mm

<sup>a</sup> Min, max, mean depths are ave. mid-point values except pools: taken at deepest part of pool.

<sup>b</sup> Composite sample of riffles and pools within the designated reach.

<sup>c</sup> Active bed of a riffle.

<sup>d</sup> Height of roughness feature above bed.

**Worksheet 2-1.** Gage station and field data (Rosgen and Silvey, 2007).

Summary.... <b>USGS GAGE STATION</b> Data/Records for <b>STREAM CHANNEL CLASSIFICATION</b>					
Station NAME:	Red River-2-419.14			Station Number:	N/A
LOCATION:	Red River-2-419.14				
Period of RECORD:	N/A yrs		Mean Annual DISCHARGE:	N/A cfs	
Drainage AREA:	7068160 acres	11044 mi <sup>2</sup>	Drainage Area Mn ELEV:	840.54 ft	
Reference REACH SLOPE:	ft/ft		Valley Type:	X	
Stream Type:	C6c-		HUC:	-- -- -- -- -- -- -- -- -- --	
"BANKFULL" CHARACTERISTICS					
Determined from FIELD MEASUREMENT			Determined from GAGE DATA Analysis		
Bankfull WIDTH ( $W_{bkf}$ )	150.6	ft	Bankfull WIDTH ( $W_{bkf}$ )		ft
Bankfull Mean DEPTH ( $d_{bkf}$ )	11.5	ft	Bankfull MEAN DEPTH ( $d_{bkf}$ )		ft
Bankfull Xsec AREA ( $A_{bkf}$ )	1725.4	ft <sup>2</sup>	Bankfull Xsec AREA ( $A_{bkf}$ )		ft <sup>2</sup>
Wetted PERIMETER ( $W_p$ )	156.9	ft	Wetted PERIMETER ( $W_p$ )		ft
Bankfull STAGE (Gage Ht)		ft	Bankfull STAGE (Gage Ht)		ft
Est. Mean VELOCITY ( $u$ )	2.5	ft/sec	Mean VELOCITY ( $u$ )		ft/sec
Est. Bkf. DISCHARGE ( $Q_{bkf}$ )	4280.0	cfs	Bankfull DISCHARGE ( $Q_{bkf}$ )		cfs
Bankfull DISCHARGE associated with "field-determined" Bankfull STAGE				4280.0	cfs
Recurrence Interval ( Log-Pearson ) associated with "field-determined" Bankfull Discharge				1.21	yrs
From the Annual Peak Flow Frequency Analysis data for the Gage Station, determine:					
1.5 Year R.I. Discharge..... =	N/A	cfs	10 Year R.I. Discharge..... =	N/A	cfs
2.0 Year R.I. Discharge..... =	N/A	cfs	25 Year R.I. Discharge..... =	N/A	cfs
5.0 Year R.I. Discharge..... =	N/A	cfs	50 Year R.I. Discharge..... =	N/A	cfs
MEANDER GEOMETRY					
Meander Length ( $L_m$ )	2248	ft	Radius of Curvature ( $R_C$ )	769.0	ft
Belt Width ( $W_{blt}$ )	3639	ft	Meander Width Ratio ( $W_{blt}/W_{bkf}$ )	24.16	ft/ft
HYDRAULIC GEOMETRY					
Based on USGS Discharge Summary Notes data ( Form 9-207 ) and regression analyses of measured discharge ( $Q$ ) with the hydraulic parameters of Width ( $W$ ), Area ( $A$ ), Mean Depth ( $d$ ) & Mean Velocity ( $u$ ), determine the <i>intercept coefficient</i> ( $a$ ) and the <i>slope exponent</i> ( $b$ ) values for a power function of the form $Y = aX^b$ , when $Y$ is one of the selected hydraulic parameters and $X$ is a given discharge value ( $Q$ ).					
	Width ( $W$ )	Depth ( $d$ )	Area ( $A$ )	Velocity ( $u$ )	
Intercept Coefficient: ( $a$ )					
Slope Exponent: ( $b$ )					
Hydraulic Radius: $R = A / W_p$		ft	Manning's "n" at Bankfull Stage	0.025	Coeff.
$"n" = 1.4865 [ ( Area ) ( Hydraulic Radius^{2/3} ) ( Slope^{1/2} ) ] / Q_{bkf}$					

**Worksheet 2-2.** Computations of velocity and bankfull discharge using various methods (Rosgen, 2006b; Rosgen and Silvey, 2007).

Bankfull VELOCITY / DISCHARGE Estimates										
Site	Red River-2-419.14				Location	Red River-2-419.14				
Date	9/29/2011	Stream Type	C6c-	Valley Type	X					
Observers	KD, JB				HUC	-- -- -- -- -- -- -- -- -- --				
INPUT VARIABLES				OUTPUT VARIABLES						
Bankfull Cross-sectional	1725.4	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Mean DEPTH	11.5	$D_{bkf}$ (ft)					
Bankfull WIDTH	150.6	$W_{bkf}$ (ft)	Wetted PERIMETER ~ 2 * $d_{bkf}$ + $W_{bkf}$	173.6	$W_p$ (ft)					
$D_{84}$ @ Riffle	0.0031	Dia. (mm)	$D_{84}$ mm / 304.8 =	0.0	$D_{84}$ (ft)					
Bankfull SLOPE	0.0001	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	9.9	R (ft)					
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R (ft) / $D_{84}$ (ft)	977363						
Drainage AREA	11044.0	DA (mi <sup>2</sup> )	Shear Velocity $u^* = \sqrt{gRS}$	0.2	$u^*$ (ft / sec)					
ESTIMATION METHODS				Bankfull VELOCITY		Bankfull DISCHARGE				
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 \text{Log}\{ R / D_{84} \} ] u^*$				5.5	ft / sec	9512	cfs			
2. Roughness Coefficient: a) Manning's 'n' from friction factor / relative roughness (Figs. 2-18, 19) $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text"/>				2.3	ft / sec	3979	cfs			
2. Roughness Coefficient: $u = 1.4865 * R^{2/3} * S^{1/2} / n$ b) Manning's 'n' from Jarrett ( USGS ): $n = 0.39S^{-.38R^{-.16}}$ n = <input type="text"/>				8.1	ft / sec	13938	cfs			
Note: This equation is for applications involving steep, step-pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for stream types A1, A2, A3, B1, B2, B3, C2 and E3.										
2. Roughness Coefficient: c) Manning's 'n' from Stream Type $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text" value="0.025"/>				2.3	ft / sec	3979	cfs			
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.) HEC-RAS				2.5	ft / sec	4280	cfs			
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.)					ft / sec		cfs			
4. Continuity Equations: a) Regional Curves $u = Q / A$ Return Period for Bankfull Discharge Q = <input type="text" value="1.46"/> Yr.					ft / sec		cfs			
4. Continuity Equations: b) USGS Gage Data $u = Q / A$					ft / sec		cfs			
Options for using the $D_{84}$ term in the relative roughness relation (R/ $D_{84}$ ), when using estimation method 1.										
Option 1. For sand-bed channels: Measure the "protrusion height" ( $h_{sd}$ ) of sand dunes above channel bed elevations. Substitute an average sand dune protrusion height ( $h_{sd}$ in ft) for the $D_{84}$ term in est. method 1.										
Option 2. For boulder-dominated channels: Measure several "protrusion heights" ( $h_{bo}$ ) of boulders above channel bed elevations. Substitute an ave. boulder protrusion height ( $h_{bo}$ in ft) for the $D_{84}$ term in est. method 1.										
Option 3. For bedrock-dominated channels: Measure several "protrusion heights" ( $h_{br}$ ) of rock separations/steps/joints/uplifted surfaces above channel bed elevations. Substitute an average bedrock protrusion height ( $h_{br}$ in feet) for the $D_{84}$ term in estimation method 1.										

**Worksheet 2-3.** Field form for Level II stream classification (Rosgen, 1996; Rosgen , 2006b).

Stream: <b>Red River-2-419.14</b>	
Basin: <b>Red River Basin</b>	Drainage Area: <b>7E+06</b> acres <b>11044</b> mi <sup>2</sup>
Location: <b>Red River-2-419.14</b>	
Twp.&Rge: - Sec.&Qtr.: -	
Cross-Section Monuments (Lat./Long.): - Date: <b>9/29/2011</b>	
Observers: <b>KD, JB</b> Valley Type: <b>X</b>	

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>150.6</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>11.5</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>1725.4</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>13.1</b>	ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>16.6</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>790.5</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>5.2</b>	ft/ft
<b>Channel Materials (Particle Size Index ) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>&lt;0.001</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.000070</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).	<b>2.2</b>	

<div style="border: 1px solid black; padding: 5px; display: inline-block;">Stream Type</div>	<div style="border: 1px solid black; padding: 5px; display: inline-block; background-color: yellow;"><b>C6c-</b></div>	<div style="border: 1px solid black; padding: 5px; display: inline-block;">See Classification Key (Figure 2-21)</div>
--	--	---

**Worksheet 2-4.** Morphological relations, including dimensionless ratios of river reach sites (Rosgen, 2006b; Rosgen and Silvey 2007).

Stream: <b>Red River-2-419.14</b>		Location: <b>Red River-2-419.14</b>								
Observers: <b>KD, JB</b>		Date: <b>9/29/2011</b>		Valley Type: <b>X</b>		Stream Type: <b>C6c-</b>				
River Reach Summary Data										
Channel Dimension	Mean Riffle Depth ( $d_{bkt}$ )	<b>11.5</b>	ft	Riffle Width ( $W_{bkt}$ )	<b>150.6</b>	ft	Riffle Area ( $A_{bkt}$ )	<b>1725.4</b>	ft <sup>2</sup>	
	Mean Pool Depth ( $d_{bkfp}$ )		ft	Pool Width ( $W_{bkfp}$ )		ft	Pool Area ( $A_{bkfp}$ )		ft <sup>2</sup>	
	Mean Pool Depth/Mean Riffle Depth		$d_{bkfp}/d_{bkt}$	Pool Width/Riffle Width		$W_{bkfp}/W_{bkt}$	Pool Area / Riffle Area		$A_{bkfp}/A_{bkt}$	
	Max Riffle Depth ( $d_{maxrif}$ )	<b>16.6</b>	ft	Max Pool Depth ( $d_{maxp}$ )		ft	Max Riffle Depth/Mean Riffle Depth	<b>1.4</b>		
	Max Pool Depth/Mean Riffle Depth			Point Bar Slope		ft/ft	Inner Berm Width ( $W_{ib}$ )		ft	
	Inner Berm Depth ( $d_{ib}$ )		ft	Inner Berm Width/Depth Ratio			$W_{ib}/d_{ib}$	Inner Berm Area ( $A_{ib}$ )		ft <sup>2</sup>
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )				<b>2.5</b>	ft/s	Estimation Method		<b>HEC-RAS</b>	
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )				<b>4280</b>	cfs	Drainage Area		<b>11044</b>	mi <sup>2</sup>

Channel Pattern	Geometry			Dimensionless Geometry Ratios			
	Mean	Min	Max	Mean	Min	Max	
	Meander Wavelength ( $L_m$ )	<b>2248</b>			ft	Meander Length Ratio ( $L_m/W_{bkt}$ )	<b>14.9</b>
	Radius of Curvature ( $R_c$ )	<b>769</b>			ft	Radius of Curvature/Riffle Width ( $R_c/W_{bkt}$ )	<b>5.1</b>
	Belt Width ( $W_{bit}$ )	<b>3639</b>			ft	Meander Width Ratio ( $W_{bit}/W_{bkt}$ )	<b>24.2</b>
	Individual Pool Length				ft	Pool Length/Riffle Width	
	Pool to Pool Spacing				ft	Pool to Pool Spacing/Riffle Width	
Riffle Length				ft	Riffle Length/Riffle Width		

Channel Profile	Valley Slope (VS)		ft/ft	Average Water Surface Slope (S)		ft/ft	Sinuosity (VS/S)		
	Stream Length (SL)	<b>56175</b>	ft	Valley Length (VL)	<b>25772</b>	ft	Sinuosity (SL/VL)	<b>2.2</b>	
	Low Bank Height (LBH)	start	ft	Max Riffle Depth	start	ft	Bank-Height Ratio (BHR)	start	
		end	ft		end	ft	(LBH/Max Riffle Depth)	end	
	Facet Slopes			Dimensionless Slope Ratios			Mean	Min	Max
	Riffle Slope ( $S_{rif}$ )	<b>0.0</b>		ft/ft	Riffle Slope/Average Water Surface Slope ( $S_{rif} / S$ )	<b>1.0</b>			
	Run Slope ( $S_{run}$ )			ft/ft	Run Slope/Average Water Surface Slope ( $S_{run} / S$ )				
	Pool Slope ( $S_p$ )			ft/ft	Pool Slope/Average Water Surface Slope ( $S_p / S$ )				
	Glide Slope ( $S_g$ )			ft/ft	Glide Slope/Average Water Surface Slope ( $S_g / S$ )				
	Feature Midpoint <sup>a</sup>			Dimensionless Depth Ratios			Mean	Min	Max
	Max Riffle Depth ( $d_{maxrif}$ )	<b>16.6</b>		ft	Max Riffle Depth/Mean Riffle Depth ( $d_{maxrif} / d_{bkt}$ )	<b>1.4</b>			
	Max Run Depth ( $d_{maxrun}$ )			ft	Max Run Depth/Mean Riffle Depth ( $d_{maxrun} / d_{bkt}$ )				
	Max Pool Depth ( $d_{maxp}$ )			ft	Max Pool Depth/Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )				
Max Glide Depth ( $d_{maxg}$ )			ft	Max Glide Depth/Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )					

Channel Materials	Reach <sup>b</sup>			Riffle <sup>c</sup>			Bar			Protrusion Height <sup>d</sup>		
	% Silt/Clay	<b>99</b>			$D_{16}$	<b>&lt;.001</b>						mm
	% Sand	<b>1</b>			$D_{35}$	<b>&lt;.001</b>					mm	
	% Gravel	<b>0</b>			$D_{50}$	<b>&lt;0.001</b>					mm	
	% Cobble	<b>0</b>			$D_{84}$	<b>0.0031</b>					mm	
	% Boulder	<b>0</b>			$D_{95}$	<b>0.0625</b>					mm	
	% Bedrock	<b>0</b>			$D_{100}$	<b>0.085</b>					mm	

<sup>a</sup> Min, max, mean depths are ave. mid-point values except pools: taken at deepest part of pool.

<sup>b</sup> Composite sample of riffles and pools within the designated reach.

<sup>c</sup> Active bed of a riffle.

<sup>d</sup> Height of roughness feature above bed.

**Worksheet 2-1.** Gage station and field data (Rosgen and Silvey, 2007).

Summary.... <b>USGS GAGE STATION</b> Data/Records for <b>STREAM CHANNEL CLASSIFICATION</b>					
Station NAME:	Red River-1-410.65			Station Number:	N/A
LOCATION:	Red River-1-410.65				
Period of RECORD:	N/A	yrs	Mean Annual DISCHARGE:	N/A	cfs
Drainage AREA:	7850880	acres	12267	mi <sup>2</sup>	Drainage Area Mn ELEV: 836.35 ft
Reference REACH SLOPE:		ft/ft	Valley Type:	X	
Stream Type:	C6c-		HUC:	-- -- -- -- --	
"BANKFULL" CHARACTERISTICS					
Determined from FIELD MEASUREMENT			Determined from GAGE DATA Analysis		
Bankfull WIDTH ( $W_{bkf}$ )	185.2	ft	Bankfull WIDTH ( $W_{bkf}$ )		ft
Bankfull Mean DEPTH ( $d_{bkf}$ )	11.9	ft	Bankfull MEAN DEPTH ( $d_{bkf}$ )		ft
Bankfull Xsec AREA ( $A_{bkf}$ )	2156.7	ft <sup>2</sup>	Bankfull Xsec AREA ( $A_{bkf}$ )		ft <sup>2</sup>
Wetted PERIMETER ( $W_p$ )	187.4	ft	Wetted PERIMETER ( $W_p$ )		ft
Bankfull STAGE (Gage Ht)		ft	Bankfull STAGE (Gage Ht)		ft
Est. Mean VELOCITY ( $u$ )	2.2	ft/sec	Mean VELOCITY ( $u$ )		ft/sec
Est. Bkf. DISCHARGE ( $Q_{bkf}$ )	4700.0	cfs	Bankfull DISCHARGE ( $Q_{bkf}$ )		cfs
Bankfull DISCHARGE associated with "field-determined" Bankfull STAGE				4700.0	cfs
Recurrence Interval ( Log-Pearson ) associated with "field-determined" Bankfull Discharge				1.19	yrs
From the Annual Peak Flow Frequency Analysis data for the Gage Station, determine:					
1.5 Year R.I. Discharge..... =	N/A	cfs	10 Year R.I. Discharge..... =	N/A	cfs
2.0 Year R.I. Discharge..... =	N/A	cfs	25 Year R.I. Discharge..... =	N/A	cfs
5.0 Year R.I. Discharge..... =	N/A	cfs	50 Year R.I. Discharge..... =	N/A	cfs
MEANDER GEOMETRY					
Meander Length ( $L_m$ )	2066	ft	Radius of Curvature ( $R_C$ )	433.0	ft
Belt Width ( $W_{blt}$ )	2330	ft	Meander Width Ratio ( $W_{blt}/W_{bkf}$ )	12.6	ft/ft
HYDRAULIC GEOMETRY					
Based on USGS Discharge Summary Notes data ( Form 9-207 ) and regression analyses of measured discharge ( $Q$ ) with the hydraulic parameters of Width ( $W$ ), Area ( $A$ ), Mean Depth ( $d$ ) & Mean Velocity ( $u$ ), determine the <i>intercept coefficient</i> ( $a$ ) and the <i>slope exponent</i> ( $b$ ) values for a power function of the form $Y = aX^b$ , when $Y$ is one of the selected hydraulic parameters and $X$ is a given discharge value ( $Q$ ).					
	Width ( $W$ )	Depth ( $d$ )	Area ( $A$ )	Velocity ( $u$ )	
Intercept Coefficient: ( $a$ )					
Slope Exponent: ( $b$ )					
Hydraulic Radius: $R = A / W_p$		ft	Manning's "n" at Bankfull Stage	0.025	Coeff.
$"n" = 1.4865 [ ( Area ) ( Hydraulic Radius^{2/3} ) ( Slope^{1/2} ) ] / Q_{bkf}$					

**Worksheet 2-2.** Computations of velocity and bankfull discharge using various methods (Rosgen, 2006b; Rosgen and Silvey, 2007).

Bankfull VELOCITY / DISCHARGE Estimates										
Site	Red River-1-410.65				Location	Red River-1-410.65				
Date	9/28/2011	Stream Type	C6c-	Valley Type	X					
Observers	KD, JB				HUC	-- -- -- -- -- -- -- -- -- --				
INPUT VARIABLES				OUTPUT VARIABLES						
Bankfull Cross-sectional	2156.7	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Mean DEPTH	11.9	$D_{bkf}$ (ft)					
Bankfull WIDTH	185.2	$W_{bkf}$ (ft)	Wetted PERIMETER ~ 2 * $d_{bkf}$ + $W_{bkf}$	208.9	$W_p$ (ft)					
$D_{84}$ @ Riffle	0.027	Dia. (mm)	$D_{84}$ mm / 304.8 =	0.0001	$D_{84}$ (ft)					
Bankfull SLOPE	0.0001	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	10.3	R (ft)					
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R (ft) / $D_{84}$ (ft)	116545						
Drainage AREA	12267.0	DA (mi <sup>2</sup> )	Shear Velocity	0.1	$u^*$ (ft / sec)					
ESTIMATION METHODS				Bankfull VELOCITY		Bankfull DISCHARGE				
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 \text{Log}\{ R / D_{84} \} ] u^*$				4.6	ft / sec	9863	cfs			
2. Roughness Coefficient: a) Manning's 'n' from friction factor / relative roughness (Figs. 2-18, 19) $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text"/>				2.2	ft / sec	4840	cfs			
2. Roughness Coefficient: $u = 1.4865 * R^{2/3} * S^{1/2} / n$ b) Manning's 'n' from Jarrett ( USGS ): $n = 0.39 S^{-.38} R^{-.16}$ n = <input type="text"/>				8.2	ft / sec	17751	cfs			
Note: This equation is for applications involving steep, step-pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for stream types A1, A2, A3, B1, B2, B3, C2 and E3.										
2. Roughness Coefficient: c) Manning's 'n' from Stream Type $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text" value="0.025"/>				2.2	ft / sec	4840	cfs			
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.) HEC-RAS				2.2	ft / sec	4700	cfs			
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.)					ft / sec		cfs			
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge Q = <input type="text" value="1.46"/> Yr. $u = Q / A$					ft / sec		cfs			
4. Continuity Equations: b) USGS Gage Data $u = Q / A$					ft / sec		cfs			
Options for using the $D_{84}$ term in the relative roughness relation ( $R/D_{84}$ ), when using estimation method 1.										
Option 1. For sand-bed channels: Measure the "protrusion height" ( $h_{sd}$ ) of sand dunes above channel bed elevations. Substitute an average sand dune protrusion height ( $h_{sd}$ in ft) for the $D_{84}$ term in est. method 1.										
Option 2. For boulder-dominated channels: Measure several "protrusion heights" ( $h_{bo}$ ) of boulders above channel bed elevations. Substitute an ave. boulder protrusion height ( $h_{bo}$ in ft) for the $D_{84}$ term in est. method 1.										
Option 3. For bedrock-dominated channels: Measure several "protrusion heights" ( $h_{br}$ ) of rock separations/steps/joints/uplifted surfaces above channel bed elevations. Substitute an average bedrock protrusion height ( $h_{br}$ in feet) for the $D_{84}$ term in estimation method 1.										

**Worksheet 2-3.** Field form for Level II stream classification (Rosgen, 1996; Rosgen , 2006b).

Stream: <b>Red River-1-410.65</b>	
Basin: <b>Red River Basin</b>	Drainage Area: <b>8E+06</b> acres <b>12267</b> mi <sup>2</sup>
Location: <b>Red River-1-410.65</b>	
Twp.&Rge: - Sec.&Qtr.: -	
Cross-Section Monuments (Lat./Long.): - Date: <b>9/28/2011</b>	
Observers: <b>KD, JB</b> Valley Type: <b>X</b>	

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>185.2</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>11.9</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>2156.7</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>15.6</b>	ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>17.9</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>683.3</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>3.7</b>	ft/ft
<b>Channel Materials (Particle Size Index ) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>0.0018</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.000063</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).	<b>2.0</b>	

<b>Stream Type</b>	<b>C6c-</b>	<b>See Classification Key (Figure 2-21)</b>
--------------------	-------------	---

**Worksheet 2-4.** Morphological relations, including dimensionless ratios of river reach sites (Rosgen, 2006b; Rosgen and Silvey 2007).

Stream: <b>Red River-1-410.65</b>		Location: <b>Red River-1-410.65</b>								
Observers: <b>KD, JB</b>		Date: <b>9/28/2011</b>		Valley Type: <b>X</b>		Stream Type: <b>C6c-</b>				
<b>River Reach Summary Data</b>										
Channel Dimension	Mean Riffle Depth ( $d_{bkt}$ )	<b>11.9</b>	ft	Riffle Width ( $W_{bkt}$ )	<b>185.2</b>	ft	Riffle Area ( $A_{bkt}$ )	<b>2156.7</b>	ft <sup>2</sup>	
	Mean Pool Depth ( $d_{bkfp}$ )		ft	Pool Width ( $W_{bkfp}$ )		ft	Pool Area ( $A_{bkfp}$ )		ft <sup>2</sup>	
	Mean Pool Depth/Mean Riffle Depth		$d_{bkfp}/d_{bkt}$	Pool Width/Riffle Width		$W_{bkfp}/W_{bkt}$	Pool Area / Riffle Area		$A_{bkfp}/A_{bkt}$	
	Max Riffle Depth ( $d_{maxrif}$ )	<b>17.9</b>	ft	Max Pool Depth ( $d_{maxp}$ )		ft	Max Riffle Depth/Mean Riffle Depth	<b>1.5</b>		
	Max Pool Depth/Mean Riffle Depth			Point Bar Slope		ft/ft	Inner Berm Width ( $W_{ib}$ )		ft	
	Inner Berm Depth ( $d_{ib}$ )		ft	Inner Berm Width/Depth Ratio			$W_{ib}/d_{ib}$	Inner Berm Area ( $A_{ib}$ )		ft <sup>2</sup>
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )				<b>2.2</b>	ft/s	Estimation Method		<b>HEC-RAS</b>	
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )				<b>4700</b>	cfs	Drainage Area		<b>12267</b>	mi <sup>2</sup>

Channel Pattern	Geometry	Mean	Min	Max	Dimensionless Geometry Ratios			Mean	Min	Max
	Meander Wavelength ( $L_m$ )	<b>2066</b>			ft	Meander Length Ratio ( $L_m/W_{bkt}$ )		<b>11.2</b>		
	Radius of Curvature ( $R_c$ )	<b>433</b>			ft	Radius of Curvature/Riffle Width ( $R_c/W_{bkt}$ )		<b>2.3</b>		
	Belt Width ( $W_{bit}$ )	<b>2330</b>			ft	Meander Width Ratio ( $W_{bit}/W_{bkt}$ )		<b>12.6</b>		
	Individual Pool Length				ft	Pool Length/Riffle Width				
	Pool to Pool Spacing				ft	Pool to Pool Spacing/Riffle Width				
	Riffle Length				ft	Riffle Length/Riffle Width				

Channel Profile	Valley Slope (VS)		ft/ft	Average Water Surface Slope (S)		ft/ft	Sinuosity (VS/S)				
	Stream Length (SL)	<b>65270</b>	ft	Valley Length (VL)	<b>33364</b>	ft	Sinuosity (SL/VL)	<b>2.0</b>			
	Low Bank Height (LBH)	start	ft	Max Riffle Depth	start	ft	Bank-Height Ratio (BHR)	start			
		end	ft		end	ft	(LBH/Max Riffle Depth)	end			
	<b>Facet Slopes</b>		Mean	Min	Max	<b>Dimensionless Slope Ratios</b>			Mean	Min	Max
	Riffle Slope ( $S_{rif}$ )	<b>0.0</b>			ft/ft	Riffle Slope/Average Water Surface Slope ( $S_{rif} / S$ )		<b>1.0</b>			
	Run Slope ( $S_{run}$ )				ft/ft	Run Slope/Average Water Surface Slope ( $S_{run} / S$ )					
	Pool Slope ( $S_p$ )				ft/ft	Pool Slope/Average Water Surface Slope ( $S_p / S$ )					
	Glide Slope ( $S_g$ )				ft/ft	Glide Slope/Average Water Surface Slope ( $S_g / S$ )					
	<b>Feature Midpoint<sup>a</sup></b>		Mean	Min	Max	<b>Dimensionless Depth Ratios</b>			Mean	Min	Max
	Max Riffle Depth ( $d_{maxrif}$ )	<b>17.9</b>			ft	Max Riffle Depth/Mean Riffle Depth ( $d_{maxrif} / d_{bkt}$ )		<b>1.5</b>			
	Max Run Depth ( $d_{maxrun}$ )				ft	Max Run Depth/Mean Riffle Depth ( $d_{maxrun} / d_{bkt}$ )					
	Max Pool Depth ( $d_{maxp}$ )				ft	Max Pool Depth/Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )					
	Max Glide Depth ( $d_{maxg}$ )				ft	Max Glide Depth/Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )					

Channel Materials		Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Protrusion Height <sup>d</sup>	
	% Silt/Clay	<b>98</b>			$D_{16}$	<b>&lt;.001</b>			mm
	% Sand	<b>2</b>			$D_{35}$	<b>&lt;.001</b>			mm
	% Gravel	<b>0</b>			$D_{50}$	<b>0.0018</b>			mm
	% Cobble	<b>0</b>			$D_{84}$	<b>0.027</b>			mm
	% Boulder	<b>0</b>			$D_{95}$	<b>0.063</b>			mm
	% Bedrock	<b>0</b>			$D_{100}$	<b>0.23</b>			mm

<sup>a</sup> Min, max, mean depths are ave. mid-point values except pools: taken at deepest part of pool.

<sup>b</sup> Composite sample of riffles and pools within the designated reach.

<sup>c</sup> Active bed of a riffle.

<sup>d</sup> Height of roughness feature above bed.

**Worksheet 2-1.** Gage station and field data (Rosgen and Silvey, 2007).

Summary.... <b>USGS GAGE STATION</b> Data/Records for <b>STREAM CHANNEL CLASSIFICATION</b>					
Station NAME:	Maple River - 2 - 11.39			Station Number:	N/A
LOCATION:	Maple River - 2 - 11.39				
Period of RECORD:	N/A	yrs	Mean Annual DISCHARGE:	N/A	cfs
Drainage AREA:	934400	acres	1460	mi <sup>2</sup>	Drainage Area Mn ELEV: 885.5 ft
Reference REACH SLOPE:		ft/ft	Valley Type:	X	
Stream Type:	E6		HUC:	-- -- -- -- --	
"BANKFULL" CHARACTERISTICS					
Determined from FIELD MEASUREMENT			Determined from GAGE DATA Analysis		
Bankfull WIDTH ( $W_{bkf}$ )	72.1	ft	Bankfull WIDTH ( $W_{bkf}$ )		ft
Bankfull Mean DEPTH ( $d_{bkf}$ )	6.5	ft	Bankfull MEAN DEPTH ( $d_{bkf}$ )		ft
Bankfull Xsec AREA ( $A_{bkf}$ )	463.0	ft <sup>2</sup>	Bankfull Xsec AREA ( $A_{bkf}$ )		ft <sup>2</sup>
Wetted PERIMETER ( $W_p$ )	77.0	ft	Wetted PERIMETER ( $W_p$ )		ft
Bankfull STAGE (Gage Ht)		ft	Bankfull STAGE (Gage Ht)		ft
Est. Mean VELOCITY ( $u$ )	1.4	ft/sec	Mean VELOCITY ( $u$ )		ft/sec
Est. Bkf. DISCHARGE ( $Q_{bkf}$ )	650.0	cfs	Bankfull DISCHARGE ( $Q_{bkf}$ )		cfs
Bankfull DISCHARGE associated with "field-determined" Bankfull STAGE				650.0	cfs
Recurrence Interval ( Log-Pearson ) associated with "field-determined" Bankfull Discharge				1.16	yrs
From the Annual Peak Flow Frequency Analysis data for the Gage Station, determine:					
1.5 Year R.I. Discharge..... =	N/A	cfs	10 Year R.I. Discharge..... =	N/A	cfs
2.0 Year R.I. Discharge..... =	N/A	cfs	25 Year R.I. Discharge..... =	N/A	cfs
5.0 Year R.I. Discharge..... =	N/A	cfs	50 Year R.I. Discharge..... =	N/A	cfs
MEANDER GEOMETRY					
Meander Length ( $L_m$ )	1831	ft	Radius of Curvature ( $R_C$ )	261.0	ft
Belt Width ( $W_{blt}$ )	2333	ft	Meander Width Ratio ( $W_{blt}/W_{bkf}$ )	32.4	ft/ft
HYDRAULIC GEOMETRY					
Based on <i>USGS Discharge Summary Notes</i> data ( Form 9-207 ) and regression analyses of measured discharge ( $Q$ ) with the hydraulic parameters of Width ( $W$ ), Area ( $A$ ), Mean Depth ( $d$ ) & Mean Velocity ( $u$ ), determine the <i>intercept coefficient</i> ( $a$ ) and the <i>slope exponent</i> ( $b$ ) values for a power function of the form $Y = aX^b$ , when $Y$ is one of the selected hydraulic parameters and $X$ is a given discharge value ( $Q$ ).					
	Width ( $W$ )	Depth ( $d$ )	Area ( $A$ )	Velocity ( $u$ )	
Intercept Coefficient: ( $a$ )					
Slope Exponent: ( $b$ )					
Hydraulic Radius: $R = A / W_p$		ft	Manning's "n" at Bankfull Stage	0.03	Coeff.
$"n" = 1.4865 [ ( Area ) ( Hydraulic Radius^{2/3} ) ( Slope^{1/2} ) ] / Q_{bkf}$					

**Worksheet 2-2.** Computations of velocity and bankfull discharge using various methods (Rosgen, 2006b; Rosgen and Silvey, 2007).

Bankfull VELOCITY / DISCHARGE Estimates									
Site	Maple River - 2 - 11.39			Location	Maple River - 2 - 11.39				
Date	11/20/2010	Stream Type	E6	Valley Type	X				
Observers	KP, AL			HUC	-- -- -- -- -- -- -- -- -- --				
INPUT VARIABLES				OUTPUT VARIABLES					
Bankfull Cross-sectional	463.0	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Mean DEPTH	6.5	$D_{bkf}$ (ft)				
Bankfull WIDTH	72.1	$W_{bkf}$ (ft)	Wetted PERIMETER ~ 2 * $d_{bkf}$ + $W_{bkf}$	85.1	$W_p$ (ft)				
$D_{84}$ @ Riffle	0.018	Dia. (mm)	$D_{84}$ mm / 304.8 =	0.0	$D_{84}$ (ft)				
Bankfull SLOPE	0.0001	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	5.4	R (ft)				
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R (ft) / $D_{84}$ (ft)	92181					
Drainage AREA	1460.0	DA (mi <sup>2</sup> )	Shear Velocity $u^* = \sqrt{gRS}$	0.1	$u^*$ (ft / sec)				
ESTIMATION METHODS				Bankfull VELOCITY		Bankfull DISCHARGE			
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 \text{Log}\{ R / D_{84} \} ] u^*$				3.4	ft / sec	1573	cfs		
2. Roughness Coefficient: a) Manning's 'n' from friction factor / relative roughness (Figs. 2-18, 19) $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text"/>				1.3	ft / sec	589	cfs		
2. Roughness Coefficient: $u = 1.4865 * R^{2/3} * S^{1/2} / n$ b) Manning's 'n' from Jarrett ( USGS ): $n = 0.39S^{-.38}R^{-.16}$ n = <input type="text"/>				4.9	ft / sec	2268	cfs		
Note: This equation is for applications involving steep, step-pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for stream types A1, A2, A3, B1, B2, B3, C2 and E3.									
2. Roughness Coefficient: c) Manning's 'n' from Stream Type $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = .03				1.3	ft / sec	589	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.) HEC-RAS				1.4	ft / sec	650	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.)					ft / sec		cfs		
4. Continuity Equations: a) Regional Curves $u = Q / A$ Return Period for Bankfull Discharge Q = 1.46 Yr.					ft / sec		cfs		
4. Continuity Equations: b) USGS Gage Data $u = Q / A$					ft / sec		cfs		
Options for using the $D_{84}$ term in the relative roughness relation ( $R/D_{84}$ ), when using estimation method 1.									
Option 1. For sand-bed channels: Measure the "protrusion height" ( $h_{sd}$ ) of sand dunes above channel bed elevations. Substitute an average sand dune protrusion height ( $h_{sd}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 2. For boulder-dominated channels: Measure several "protrusion heights" ( $h_{bo}$ ) of boulders above channel bed elevations. Substitute an ave. boulder protrusion height ( $h_{bo}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 3. For bedrock-dominated channels: Measure several "protrusion heights" ( $h_{br}$ ) of rock separations/steps/joints/uplifted surfaces above channel bed elevations. Substitute an average bedrock protrusion height ( $h_{br}$ in feet) for the $D_{84}$ term in estimation method 1.									

**Worksheet 2-3.** Field form for Level II stream classification (Rosgen, 1996; Rosgen , 2006b).

Stream: <b>Maple River - 2 - 11.39</b>	
Basin: <b>Red River Basin</b>	Drainage Area: <b>934400</b> acres <b>1460</b> mi <sup>2</sup>
Location: <b>Maple River - 2 - 11.39</b>	
Twp.&Rge: -	Sec.&Qtr.: -
Cross-Section Monuments (Lat./Long.): -	Date: <b>11/20/2010</b>
Observers: <b>KP, AL</b>	Valley Type: <b>X</b>

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>72.1</b> ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>6.5</b> ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>463.0</b> ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>11.1</b> ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>9.0</b> ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>672.0</b> ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>9.3</b> ft/ft
<b>Channel Materials (Particle Size Index ) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>0.001</b> mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.000069</b> ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).	<b>1.7</b>

<div style="border: 1px solid black; padding: 5px; display: inline-block;"> <b>Stream Type</b> </div>	<div style="border: 1px solid black; padding: 5px; display: inline-block; background-color: yellow;"> <b>E6</b> </div>	<div style="border: 1px solid black; padding: 5px; display: inline-block;"> <b>See Classification Key (Figure 2-21)</b> </div>
---	--	--

**Worksheet 2-4.** Morphological relations, including dimensionless ratios of river reach sites (Rosgen, 2006b; Rosgen and Silvey 2007).

Stream: <b>Maple River - 2 - 11.39</b>		Location: <b>Maple River - 2 - 11.39</b>								
Observers: <b>KP, AL</b>		Date: <b>11/20/2010</b>		Valley Type: <b>X</b>		Stream Type: <b>E6</b>				
<b>River Reach Summary Data</b>										
<b>Channel Dimension</b>	Mean Riffle Depth ( $d_{bkt}$ )	<b>6.5</b>	ft	Riffle Width ( $W_{bkt}$ )	<b>72.1</b>	ft	Riffle Area ( $A_{bkt}$ )	<b>463.0</b>	ft <sup>2</sup>	
	Mean Pool Depth ( $d_{bkfp}$ )		ft	Pool Width ( $W_{bkfp}$ )		ft	Pool Area ( $A_{bkfp}$ )		ft <sup>2</sup>	
	Mean Pool Depth/Mean Riffle Depth		$d_{bkfp}/d_{bkt}$	Pool Width/Riffle Width		$W_{bkfp}/W_{bkt}$	Pool Area / Riffle Area		$A_{bkfp}/A_{bkt}$	
	Max Riffle Depth ( $d_{maxrif}$ )	<b>9.0</b>	ft	Max Pool Depth ( $d_{maxp}$ )		ft	Max Riffle Depth/Mean Riffle Depth	<b>1.4</b>		
	Max Pool Depth/Mean Riffle Depth			Point Bar Slope		ft/ft	Inner Berm Width ( $W_{ib}$ )		ft	
	Inner Berm Depth ( $d_{ib}$ )		ft	Inner Berm Width/Depth Ratio			$W_{ib}/d_{ib}$	Inner Berm Area ( $A_{ib}$ )		ft <sup>2</sup>
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )			<b>1.4</b>		ft/s	Estimation Method	<b>HEC-RAS</b>		
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )			<b>650</b>		cfs	Drainage Area	<b>1460</b>	mi <sup>2</sup>	

<b>Channel Pattern</b>	Geometry			Dimensionless Geometry Ratios			
	Mean	Min	Max	Mean	Min	Max	
	Meander Wavelength ( $L_m$ )	<b>1831</b>			ft	Meander Length Ratio ( $L_m/W_{bkt}$ )	<b>25.4</b>
	Radius of Curvature ( $R_c$ )	<b>261</b>			ft	Radius of Curvature/Riffle Width ( $R_c/W_{bkt}$ )	<b>3.6</b>
	Belt Width ( $W_{bit}$ )	<b>2333</b>			ft	Meander Width Ratio ( $W_{bit}/W_{bkt}$ )	<b>32.4</b>
	Individual Pool Length				ft	Pool Length/Riffle Width	
	Pool to Pool Spacing				ft	Pool to Pool Spacing/Riffle Width	
Riffle Length				ft	Riffle Length/Riffle Width		

<b>Channel Profile</b>	Valley Slope (VS)		ft/ft	Average Water Surface Slope (S)		ft/ft	Sinuosity (VS/S)		
	Stream Length (SL)	<b>34852</b>	ft	Valley Length (VL)	<b>20900</b>	ft	Sinuosity (SL/VL)	<b>1.7</b>	
	Low Bank Height (LBH)	start	ft	Max Riffle Depth	start	ft	Bank-Height Ratio (BHR)	start	
		end	ft		end	ft	(LBH/Max Riffle Depth)	end	
	Facet Slopes			Dimensionless Slope Ratios			Mean Min Max		
	Riffle Slope ( $S_{rif}$ )	<b>0.0</b>		ft/ft	Riffle Slope/Average Water Surface Slope ( $S_{rif} / S$ )	<b>1.0</b>			
	Run Slope ( $S_{run}$ )			ft/ft	Run Slope/Average Water Surface Slope ( $S_{run} / S$ )				
	Pool Slope ( $S_p$ )			ft/ft	Pool Slope/Average Water Surface Slope ( $S_p / S$ )				
	Glide Slope ( $S_g$ )			ft/ft	Glide Slope/Average Water Surface Slope ( $S_g / S$ )				
	Feature Midpoint <sup>a</sup>			Dimensionless Depth Ratios			Mean Min Max		
	Max Riffle Depth ( $d_{maxrif}$ )	<b>9.0</b>		ft	Max Riffle Depth/Mean Riffle Depth ( $d_{maxrif} / d_{bkt}$ )	<b>1.4</b>			
	Max Run Depth ( $d_{maxrun}$ )			ft	Max Run Depth/Mean Riffle Depth ( $d_{maxrun} / d_{bkt}$ )				
	Max Pool Depth ( $d_{maxp}$ )			ft	Max Pool Depth/Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )				
Max Glide Depth ( $d_{maxg}$ )			ft	Max Glide Depth/Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )					

<b>Channel Materials</b>	Reach <sup>b</sup>			Riffle <sup>c</sup>			Bar			Protrusion Height <sup>d</sup>		
	% Silt/Clay	<b>97</b>			$D_{16}$	<b>&lt;.001</b>						mm
	% Sand	<b>3</b>			$D_{35}$	<b>&lt;.001</b>					mm	
	% Gravel	<b>0</b>			$D_{50}$	<b>0.001</b>					mm	
	% Cobble	<b>0</b>			$D_{84}$	<b>0.018</b>					mm	
	% Boulder	<b>0</b>			$D_{95}$	<b>0.07</b>					mm	
	% Bedrock	<b>0</b>			$D_{100}$	<b>4.75</b>					mm	

<sup>a</sup> Min, max, mean depths are ave. mid-point values except pools: taken at deepest part of pool.

<sup>b</sup> Composite sample of riffles and pools within the designated reach.

<sup>c</sup> Active bed of a riffle.

<sup>d</sup> Height of roughness feature above bed.

**Worksheet 2-1.** Gage station and field data (Rosgen and Silvey, 2007).

Summary.... <b>USGS GAGE STATION</b> Data/Records for <b>STREAM CHANNEL CLASSIFICATION</b>						
Station NAME:	Maple River-1-0.78			Station Number:	N/A	
LOCATION:	Maple River-1-0.78					
Period of RECORD:	N/A		yr/s	Mean Annual DISCHARGE:	N/A cfs	
Drainage AREA:	948480	acres	1482	mi <sup>2</sup>	Drainage Area Mn ELEV:	874.5 ft
Reference REACH SLOPE:			ft/ft		Valley Type:	X
Stream Type:	E6		HUC: _____			
"BANKFULL" CHARACTERISTICS						
Determined from FIELD MEASUREMENT			Determined from GAGE DATA Analysis			
Bankfull WIDTH ( $W_{bkf}$ )	68.5	ft	Bankfull WIDTH ( $W_{bkf}$ )		ft	
Bankfull Mean DEPTH ( $d_{bkf}$ )	5.8	ft	Bankfull MEAN DEPTH ( $d_{bkf}$ )		ft	
Bankfull Xsec AREA ( $A_{bkf}$ )	399.1	ft <sup>2</sup>	Bankfull Xsec AREA ( $A_{bkf}$ )		ft <sup>2</sup>	
Wetted PERIMETER ( $W_p$ )	72.5	ft	Wetted PERIMETER ( $W_p$ )		ft	
Bankfull STAGE (Gage Ht)		ft	Bankfull STAGE (Gage Ht)		ft	
Est. Mean VELOCITY ( $u$ )	1.6	ft/sec	Mean VELOCITY ( $u$ )		ft/sec	
Est. Bkf. DISCHARGE ( $Q_{bkf}$ )	650.0	cfs	Bankfull DISCHARGE ( $Q_{bkf}$ )		cfs	
Bankfull DISCHARGE associated with "field-determined" Bankfull STAGE				650.0	cfs	
Recurrence Interval ( Log-Pearson ) associated with "field-determined" Bankfull Discharge				1.2	yr/s	
From the Annual Peak Flow Frequency Analysis data for the Gage Station, determine:						
1.5 Year R.I. Discharge..... =	N/A	cfs	10 Year R.I. Discharge..... =	N/A	cfs	
2.0 Year R.I. Discharge..... =	N/A	cfs	25 Year R.I. Discharge..... =	N/A	cfs	
5.0 Year R.I. Discharge..... =	N/A	cfs	50 Year R.I. Discharge..... =	N/A	cfs	
MEANDER GEOMETRY						
Meander Length ( $L_m$ )	739	ft	Radius of Curvature ( $R_C$ )	153.0	ft	
Belt Width ( $W_{blt}$ )	1284	ft	Meander Width Ratio ( $W_{blt}/W_{bkf}$ )	18.7	ft/ft	
HYDRAULIC GEOMETRY						
Based on <i>USGS Discharge Summary Notes</i> data ( Form 9-207 ) and regression analyses of measured discharge ( $Q$ ) with the hydraulic parameters of Width ( $W$ ), Area ( $A$ ), Mean Depth ( $d$ ) & Mean Velocity ( $u$ ), determine the <i>intercept coefficient</i> ( $a$ ) and the <i>slope exponent</i> ( $b$ ) values for a power function of the form $Y = aX^b$ , when $Y$ is one of the selected hydraulic parameters and $X$ is a given discharge value ( $Q$ ).						
	Width ( $W$ )	Depth ( $d$ )	Area ( $A$ )	Velocity ( $u$ )		
Intercept Coefficient: ( $a$ )						
Slope Exponent: ( $b$ )						
Hydraulic Radius: $R = A / W_p$		ft	Manning's "n" at Bankfull Stage	0.030	Coeff.	
$"n" = 1.4865 [ ( Area ) ( Hydraulic Radius^{2/3} ) ( Slope^{1/2} ) ] / Q_{bkf}$						

**Worksheet 2-2.** Computations of velocity and bankfull discharge using various methods (Rosgen, 2006b; Rosgen and Silvey, 2007).

Bankfull VELOCITY / DISCHARGE Estimates									
Site	Maple River-1-0.78			Location	Maple River-1-0.78				
Date	11/16/2010	Stream Type	E6	Valley Type	X				
Observers	KP, AL			HUC	-- -- -- -- -- -- -- -- -- --				
INPUT VARIABLES				OUTPUT VARIABLES					
Bankfull Cross-sectional	399.1	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Mean DEPTH	5.8	$D_{bkf}$ (ft)				
Bankfull WIDTH	68.5	$W_{bkf}$ (ft)	Wetted PERIMETER $\sim 2 * d_{bkf} + W_{bkf}$	80.2	$W_p$ (ft)				
$D_{84}$ @ Riffle	1.1	Dia. (mm)	$D_{84}$ mm / 304.8 =	0.0	$D_{84}$ (ft)				
Bankfull SLOPE	0.0001	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	5.0	R (ft)				
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R (ft) / $D_{84}$ (ft)	1380					
Drainage AREA	1482.0	DA (mi <sup>2</sup> )	Shear Velocity $u^* = \sqrt{gRS}$	0.1	$u^*$ (ft / sec)				
ESTIMATION METHODS				Bankfull VELOCITY		Bankfull DISCHARGE			
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 \text{Log}\{ R / D_{84} \} ] u^*$				2.8	ft / sec	1102	cfs		
2. Roughness Coefficient: a) Manning's 'n' from friction factor / relative roughness (Figs. 2-18, 19) $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text"/>				1.5	ft / sec	610	cfs		
2. Roughness Coefficient: b) Manning's 'n' from Jarrett ( USGS ): $n = 0.39S^{-.38}R^{-.16}$ n = <input type="text"/> Note: This equation is for applications involving steep, step-pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for stream types A1, A2, A3, B1, B2, B3, C2 and E3.				4.8	ft / sec	1925	cfs		
2. Roughness Coefficient: c) Manning's 'n' from Stream Type $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text" value="0.03"/>				1.5	ft / sec	610	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.) HEC-RAS				1.6	ft / sec	650	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.)					ft / sec		cfs		
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge Q = <input type="text" value="1.46"/> Yr. $u = Q / A$					ft / sec		cfs		
4. Continuity Equations: b) USGS Gage Data $u = Q / A$					ft / sec		cfs		
Options for using the $D_{84}$ term in the relative roughness relation ( $R/D_{84}$ ), when using estimation method 1.									
Option 1. For sand-bed channels: Measure the "protrusion height" ( $h_{sd}$ ) of sand dunes above channel bed elevations. Substitute an average sand dune protrusion height ( $h_{sd}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 2. For boulder-dominated channels: Measure several "protrusion heights" ( $h_{bo}$ ) of boulders above channel bed elevations. Substitute an ave. boulder protrusion height ( $h_{bo}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 3. For bedrock-dominated channels: Measure several "protrusion heights" ( $h_{br}$ ) of rock separations/steps/joints/uplifted surfaces above channel bed elevations. Substitute an average bedrock protrusion height ( $h_{br}$ in feet) for the $D_{84}$ term in estimation method 1.									

**Worksheet 2-3.** Field form for Level II stream classification (Rosgen, 1996; Rosgen , 2006b).

Stream: <b>Maple River-1-0.78</b>	
Basin: <b>Red River Basin</b>	Drainage Area: <b>948480</b> acres <b>1482</b> mi <sup>2</sup>
Location: <b>Maple River-1-0.78</b>	
Twp.&Rge: -	Sec.&Qtr.: -
Cross-Section Monuments (Lat./Long.): -	Date: <b>11/16/2010</b>
Observers: <b>KP, AL</b>	Valley Type: <b>X</b>

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>68.5</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>5.8</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>399.1</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>11.7</b>	ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>9.1</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>377.3</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>5.5</b>	ft/ft
<b>Channel Materials (Particle Size Index ) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>0.0091</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.00011</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length ( $SL / VL$ ); or estimated from a ratio of valley slope divided by channel slope ( $VS / S$ ).	<b>2.2</b>	

<div style="border: 1px solid black; padding: 5px; display: inline-block;"> <b>Stream Type</b> </div>	<div style="border: 1px solid black; padding: 5px; display: inline-block; background-color: yellow;"> <b>E6</b> </div>	<div style="border: 1px solid black; padding: 5px; display: inline-block;"> <b>See Classification Key (Figure 2-21)</b> </div>
---	--	--

**Worksheet 2-4.** Morphological relations, including dimensionless ratios of river reach sites (Rosgen, 2006b; Rosgen and Silvey 2007).

Stream: <b>Maple River-1-0.78</b>		Location: <b>Maple River-1-0.78</b>								
Observers: <b>KP, AL</b>		Date: <b>11/16/2010</b>		Valley Type: <b>X</b>		Stream Type: <b>E6</b>				
<b>River Reach Summary Data</b>										
<b>Channel Dimension</b>	Mean Riffle Depth ( $d_{bkt}$ )	<b>5.8</b>	ft	Riffle Width ( $W_{bkt}$ )	<b>68.5</b>	ft	Riffle Area ( $A_{bkt}$ )	<b>399.1</b>	ft <sup>2</sup>	
	Mean Pool Depth ( $d_{bkfp}$ )		ft	Pool Width ( $W_{bkfp}$ )		ft	Pool Area ( $A_{bkfp}$ )		ft <sup>2</sup>	
	Mean Pool Depth/Mean Riffle Depth		$d_{bkfp}/d_{bkt}$	Pool Width/Riffle Width		$W_{bkfp}/W_{bkt}$	Pool Area / Riffle Area		$A_{bkfp}/A_{bkt}$	
	Max Riffle Depth ( $d_{maxrif}$ )	<b>9.1</b>	ft	Max Pool Depth ( $d_{maxp}$ )		ft	Max Riffle Depth/Mean Riffle Depth	<b>1.6</b>		
	Max Pool Depth/Mean Riffle Depth			Point Bar Slope		ft/ft	Inner Berm Width ( $W_{ib}$ )		ft	
	Inner Berm Depth ( $d_{ib}$ )		ft	Inner Berm Width/Depth Ratio			$W_{ib}/d_{ib}$	Inner Berm Area ( $A_{ib}$ )		ft <sup>2</sup>
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )				<b>1.6</b>	ft/s	Estimation Method		<b>HEC-RAS</b>	
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )				<b>650</b>	cfs	Drainage Area		<b>1482</b>	mi <sup>2</sup>

<b>Channel Pattern</b>	Geometry			Dimensionless Geometry Ratios			
	Mean	Min	Max	Mean	Min	Max	
	Meander Wavelength ( $L_m$ )	<b>739</b>			ft	Meander Length Ratio ( $L_m/W_{bkt}$ )	<b>10.8</b>
	Radius of Curvature ( $R_c$ )	<b>153</b>			ft	Radius of Curvature/Riffle Width ( $R_c/W_{bkt}$ )	<b>2.2</b>
	Belt Width ( $W_{bit}$ )	<b>1284</b>			ft	Meander Width Ratio ( $W_{bit}/W_{bkt}$ )	<b>18.7</b>
	Individual Pool Length				ft	Pool Length/Riffle Width	
	Pool to Pool Spacing				ft	Pool to Pool Spacing/Riffle Width	
Riffle Length				ft	Riffle Length/Riffle Width		

<b>Channel Profile</b>	Valley Slope (VS)		ft/ft	Average Water Surface Slope (S)		ft/ft	Sinuosity (VS/S)		
	Stream Length (SL)	<b>36138</b>	ft	Valley Length (VL)	<b>16792</b>	ft	Sinuosity (SL/VL)	<b>2.2</b>	
	Low Bank Height (LBH)	start	ft	Max Riffle Depth	start	ft	Bank-Height Ratio (BHR)	start	
		end	ft		end	ft	(LBH/Max Riffle Depth)	end	
	Facet Slopes			Dimensionless Slope Ratios			Mean	Min	Max
	Riffle Slope ( $S_{rif}$ )	<b>0.0</b>		ft/ft	Riffle Slope/Average Water Surface Slope ( $S_{rif} / S$ )	<b>1.0</b>			
	Run Slope ( $S_{run}$ )			ft/ft	Run Slope/Average Water Surface Slope ( $S_{run} / S$ )				
	Pool Slope ( $S_p$ )			ft/ft	Pool Slope/Average Water Surface Slope ( $S_p / S$ )				
	Glide Slope ( $S_g$ )			ft/ft	Glide Slope/Average Water Surface Slope ( $S_g / S$ )				
	Feature Midpoint <sup>a</sup>			Dimensionless Depth Ratios			Mean	Min	Max
	Max Riffle Depth ( $d_{maxrif}$ )	<b>9.1</b>		ft	Max Riffle Depth/Mean Riffle Depth ( $d_{maxrif} / d_{bkt}$ )	<b>1.6</b>			
	Max Run Depth ( $d_{maxrun}$ )			ft	Max Run Depth/Mean Riffle Depth ( $d_{maxrun} / d_{bkt}$ )				
	Max Pool Depth ( $d_{maxp}$ )			ft	Max Pool Depth/Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )				
	Max Glide Depth ( $d_{maxg}$ )			ft	Max Glide Depth/Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )				

<b>Channel Materials</b>	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Protrusion Height <sup>d</sup>	
	% Silt/Clay	<b>57</b>			$D_{16}$	<b>&lt;.001</b>		mm
	% Sand	<b>33</b>			$D_{35}$	<b>0.0019</b>		mm
	% Gravel	<b>0</b>			$D_{50}$	<b>0.0091</b>		mm
	% Cobble	<b>0</b>			$D_{84}$	<b>1.1</b>		mm
	% Boulder	<b>0</b>			$D_{95}$	<b>2.96</b>		mm
	% Bedrock	<b>0</b>			$D_{100}$	<b>4.75</b>		mm

<sup>a</sup> Min, max, mean depths are ave. mid-point values except pools: taken at deepest part of pool.

<sup>b</sup> Composite sample of riffles and pools within the designated reach.

<sup>c</sup> Active bed of a riffle.

<sup>d</sup> Height of roughness feature above bed.

Summary.... **USGS GAGE STATION** Data/Records for  
**STREAM CHANNEL CLASSIFICATION**

Station NAME:	Lower Rush River-2-6.03			Station Number:	N/A	
LOCATION:	Lower Rush River-2-6.03					
Period of RECORD:	N/A		yr/s	Mean Annual DISCHARGE:	N/A cfs	
Drainage AREA:	34144	acres	53.4	mi <sup>2</sup>	Drainage Area Mn ELEV:	N/A ft
Reference REACH SLOPE:			ft/ft		Valley Type:	X
Stream Type:	B6c		HUC: _____			

**"BANKFULL" CHARACTERISTICS**

Determined from FIELD MEASUREMENT			Determined from GAGE DATA Analysis		
Bankfull WIDTH ( $W_{bkf}$ )	63.1	ft	Bankfull WIDTH ( $W_{bkf}$ )		ft
Bankfull Mean DEPTH ( $d_{bkf}$ )	1.6	ft	Bankfull MEAN DEPTH ( $d_{bkf}$ )		ft
Bankfull Xsec AREA ( $A_{bkf}$ )	108.6	ft <sup>2</sup>	Bankfull Xsec AREA ( $A_{bkf}$ )		ft <sup>2</sup>
Wetted PERIMETER ( $W_p$ )	63.6	ft	Wetted PERIMETER ( $W_p$ )		ft
Bankfull STAGE (Gage Ht)		ft	Bankfull STAGE (Gage Ht)		ft
Est. Mean VELOCITY ( $u$ )	0.7	ft/sec	Mean VELOCITY ( $u$ )		ft/sec
Est. Bkf. DISCHARGE ( $Q_{bkf}$ )	60.0	cfs	Bankfull DISCHARGE ( $Q_{bkf}$ )		cfs
Bankfull DISCHARGE associated with "field-determined" Bankfull STAGE					60.0 cfs
Recurrence Interval ( Log-Pearson ) associated with "field-determined" Bankfull Discharge					1.1 yrs

From the **Annual Peak Flow Frequency Analysis** data for the Gage Station, determine:

1.5 Year R.I. Discharge..... =	N/A	cfs	10 Year R.I. Discharge..... =	N/A	cfs
2.0 Year R.I. Discharge..... =	N/A	cfs	25 Year R.I. Discharge..... =	N/A	cfs
5.0 Year R.I. Discharge..... =	N/A	cfs	50 Year R.I. Discharge..... =	N/A	cfs

**MEANDER GEOMETRY**

Meander Length ( $L_m$ )	1532	ft	Radius of Curvature ( $R_C$ )	230.0	ft
Belt Width ( $W_{blt}$ )	663	ft	Meander Width Ratio ( $W_{blt}/W_{bkf}$ )	10.5	ft/ft

**HYDRAULIC GEOMETRY**

Based on *USGS Discharge Summary Notes* data ( Form 9-207 ) and regression analyses of measured discharge ( $Q$ ) with the hydraulic parameters of Width ( $W$ ), Area ( $A$ ), Mean Depth ( $d$ ) & Mean Velocity ( $u$ ), determine the *intercept coefficient* ( $a$ ) and the *slope exponent* ( $b$ ) values for a power function of the form  $Y = aX^b$ , when  $Y$  is one of the selected hydraulic parameters and  $X$  is a given discharge value ( $Q$ ).

	Width ( $W$ )	Depth ( $d$ )	Area ( $A$ )	Velocity ( $u$ )
Intercept Coefficient: ( $a$ )				
Slope Exponent: ( $b$ )				

**Hydraulic Radius:**  $R = A / W_p$  \_\_\_\_\_ ft      **Manning's "n" at Bankfull Stage** **0.06** Coeff.

$"n" = 1.4865 [ ( \text{Area} ) ( \text{Hydraulic Radius}^{2/3} ) ( \text{Slope}^{1/2} ) ] / Q_{bkf}$

**Bankfull VELOCITY / DISCHARGE Estimates**

Site	Lower Rush River-2-6.04			Location	Lower Rush River-2-6.03		
Date	11/18/2010	Stream Type	B6c	Valley Type	X		
Observers	KP, AL			HUC	-- -- -- -- -- -- -- -- -- --		

INPUT VARIABLES			OUTPUT VARIABLES		
Bankfull Cross-sectional AREA	108.6	$A_{b\text{bkf}}$ (ft <sup>2</sup> )	Bankfull Mean DEPTH	1.6	$D_{b\text{bkf}}$ (ft)
Bankfull WIDTH	63.1	$W_{b\text{bkf}}$ (ft)	Wetted PERIMETER ~ 2 * $d_{b\text{bkf}}$ + $W_{b\text{bkf}}$	66.4	$W_p$ (ft)
$D_{84}$ @ Riffle	0.032	Dia. (mm)	$D_{84}$ mm / 304.8 =	0.0001	$D_{84}$ (ft)
Bankfull SLOPE	0.0001	$S_{b\text{bkf}}$ (ft / ft)	Hydraulic RADIUS $A_{b\text{bkf}} / W_p$	1.6	R (ft)
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R (ft) / $D_{84}$ (ft)	15588	
Drainage AREA	53.4	DA (mi <sup>2</sup> )	Shear Velocity $u^* = \sqrt{gRS}$	0.06	$u^*$ (ft / sec)

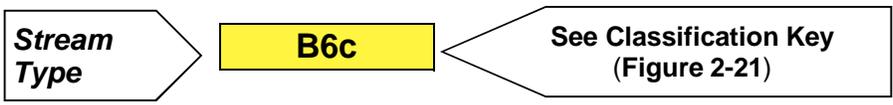
ESTIMATION METHODS	Bankfull VELOCITY		Bankfull DISCHARGE	
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66\text{Log}\{ R / D_{84} \} ] u^*$	1.6	ft / sec	171	cfs
2. Roughness Coefficient: a) Manning's 'n' from friction factor / relative roughness (Figs. 2-18, 19) $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text"/>	0.3	ft / sec	33	cfs
2. Roughness Coefficient: b) Manning's 'n' from Jarrett ( USGS ): $n = 0.39S^{-.38R^{-.16}}$ n = <input type="text"/> Note: This equation is for applications involving steep, step-pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for stream types A1, A2, A3, B1, B2, B3, C2 and E3.	1.8	ft / sec	196	cfs
2. Roughness Coefficient: c) Manning's 'n' from Stream Type $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text" value="0.055"/>	0.3	ft / sec	33	cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.) HEC-RAS	0.7	ft / sec	60	cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.)		ft / sec		cfs
4. Continuity Equations: a) Regional Curves $u = Q / A$ Return Period for Bankfull Discharge Q = <input type="text" value="1.46"/> Yr.		ft / sec		cfs
4. Continuity Equations: b) USGS Gage Data $u = Q / A$		ft / sec		cfs

**Options for using the  $D_{84}$  term in the relative roughness relation (R/ $D_{84}$ ), when using estimation method 1.**

- Option 1. For **sand-bed** channels: Measure the "**protrusion height**" ( $h_{sd}$ ) of sand dunes above channel bed elevations. Substitute an average sand dune protrusion height ( $h_{sd}$  in ft) for the  $D_{84}$  term in est. method 1.
- Option 2. For **boulder-dominated** channels: Measure several "**protrusion heights**" ( $h_{bo}$ ) of boulders above channel bed elevations. Substitute an ave. boulder protrusion height ( $h_{bo}$  in ft) for the  $D_{84}$  term in est. method 1.
- Option 3. For **bedrock-dominated** channels: Measure several "**protrusion heights**" ( $h_{br}$ ) of rock separations/steps/joints/uplifted surfaces above channel bed elevations. Substitute an average bedrock protrusion height ( $h_{br}$  in feet) for the  $D_{84}$  term in estimation method 1.

Stream:	<b>Lower Rush River</b>		
Basin:	<b>Red River Basin</b>	Drainage Area: <b>34144</b> acres	<b>53.4</b> mi <sup>2</sup>
Location:	<b>Lower Rush River-2-6.03</b>		
Twp.&Rge: -	Sec.&Qtr.: -		
Cross-Section Monuments (Lat./Long.): -	Date: <b>11/18/2010</b>		
Observers: <b>KP, AL</b>	Valley Type: <b>X</b>		

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>63.1</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>1.6</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>108.6</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>38.7</b>	ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>2.9</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>90.5</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>1.4</b>	ft/ft
<b>Channel Materials (Particle Size Index ) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>0.0019</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.000066</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).	<b>1.3</b>	



Stream: <b>Lower Rush River</b>		Location: <b>Lower Rush River-2-6.03</b>										
Observers: <b>KP, AL</b>		Date: <b>11/18/2010</b>		Valley Type: <b>X</b>		Stream Type: <b>B6c</b>						
<b>River Reach Summary Data</b>												
<b>Channel Dimension</b>	Mean Riffle Depth ( $d_{bkt}$ )	<b>1.6</b>	ft	Riffle Width ( $W_{bkt}$ )	<b>63.1</b>	ft	Riffle Area ( $A_{bkt}$ )	<b>108.6</b>	ft <sup>2</sup>			
	Mean Pool Depth ( $d_{bkfp}$ )		ft	Pool Width ( $W_{bkfp}$ )		ft	Pool Area ( $A_{bkfp}$ )		ft <sup>2</sup>			
	Mean Pool Depth/Mean Riffle Depth		$d_{bkfp}/d_{bkt}$	Pool Width/Riffle Width		$W_{bkfp}/W_{bkt}$	Pool Area / Riffle Area		$A_{bkfp}/A_{bkt}$			
	Max Riffle Depth ( $d_{maxrif}$ )	<b>2.9</b>	ft	Max Pool Depth ( $d_{maxp}$ )		ft	Max Riffle Depth/Mean Riffle Depth	<b>1.8</b>				
	Max Pool Depth/Mean Riffle Depth			Point Bar Slope		ft/ft	Inner Berm Width ( $W_{ib}$ )		ft			
	Inner Berm Depth ( $d_{ib}$ )		ft	Inner Berm Width/Depth Ratio		$W_{ib}/d_{ib}$	Inner Berm Area ( $A_{ib}$ )		ft <sup>2</sup>			
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )			<b>0.7</b>	ft/s	Estimation Method	<b>HEC-RAS</b>					
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )			<b>60</b>	cfs	Drainage Area	<b>53.4</b>	mi <sup>2</sup>				
<b>Channel Pattern</b>	<b>Geometry</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Dimensionless Geometry Ratios</b>			<b>Mean</b>	<b>Min</b>	<b>Max</b>		
	Meander Wavelength ( $L_m$ )	<b>1532</b>			ft	Meander Length Ratio ( $L_m/W_{bkt}$ )	<b>24.3</b>					
	Radius of Curvature ( $R_c$ )	<b>230</b>			ft	Radius of Curvature/Riffle Width ( $R_c/W_{bkt}$ )	<b>3.6</b>					
	Belt Width ( $W_{bit}$ )	<b>663</b>			ft	Meander Width Ratio ( $W_{bit}/W_{bkt}$ )	<b>10.5</b>					
	Individual Pool Length				ft	Pool Length/Riffle Width						
	Pool to Pool Spacing				ft	Pool to Pool Spacing/Riffle Width						
	Riffle Length				ft	Riffle Length/Riffle Width						
<b>Channel Profile</b>	Valley Slope (VS)				ft/ft	Average Water Surface Slope (S)				ft/ft	Sinuosity (VS/S)	
	Stream Length (SL)	<b>37133</b>			ft	Valley Length (VL)	<b>29667</b>			ft	Sinuosity (SL/VL)	<b>1.3</b>
	Low Bank Height (LBH)	start			ft	Max Riffle Depth	start			ft	Bank-Height Ratio (BHR) (LBH/Max Riffle Depth)	start
		end			ft		end			ft		end
	<b>Facet Slopes</b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Dimensionless Slope Ratios</b>			<b>Mean</b>	<b>Min</b>	<b>Max</b>		
	Riffle Slope ( $S_{rif}$ )	<b>0.0</b>			ft/ft	Riffle Slope/Average Water Surface Slope ( $S_{rif} / S$ )	<b>1.0</b>					
	Run Slope ( $S_{run}$ )				ft/ft	Run Slope/Average Water Surface Slope ( $S_{run} / S$ )						
	Pool Slope ( $S_p$ )				ft/ft	Pool Slope/Average Water Surface Slope ( $S_p / S$ )						
	Glide Slope ( $S_g$ )				ft/ft	Glide Slope/Average Water Surface Slope ( $S_g / S$ )						
	<b>Feature Midpoint<sup>a</sup></b>	<b>Mean</b>	<b>Min</b>	<b>Max</b>	<b>Dimensionless Depth Ratios</b>			<b>Mean</b>	<b>Min</b>	<b>Max</b>		
	Max Riffle Depth ( $d_{maxrif}$ )	<b>2.9</b>			ft	Max Riffle Depth/Mean Riffle Depth ( $d_{maxrif} / d_{bkt}$ )	<b>1.8</b>					
Max Run Depth ( $d_{maxrun}$ )				ft	Max Run Depth/Mean Riffle Depth ( $d_{maxrun} / d_{bkt}$ )							
Max Pool Depth ( $d_{maxp}$ )				ft	Max Pool Depth/Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )							
Max Glide Depth ( $d_{maxg}$ )				ft	Max Glide Depth/Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )							
<b>Channel Materials</b>		<b>Reach<sup>b</sup></b>	<b>Riffle<sup>c</sup></b>	<b>Bar</b>	<b>Reach<sup>b</sup></b>	<b>Riffle<sup>c</sup></b>	<b>Bar</b>	<b>Protrusion Height<sup>d</sup></b>				
	% Silt/Clay	<b>97</b>			D <sub>16</sub>	<b>&lt;.001</b>					mm	
	% Sand	<b>3</b>			D <sub>35</sub>	<b>&lt;.001</b>					mm	
	% Gravel	<b>0</b>			D <sub>50</sub>	<b>0.0019</b>					mm	
	% Cobble	<b>0</b>			D <sub>84</sub>	<b>0.032</b>					mm	
	% Boulder	<b>0</b>			D <sub>95</sub>	<b>0.058</b>					mm	
	% Bedrock	<b>0</b>			D <sub>100</sub>	<b>2</b>					mm	

<sup>a</sup> Min, max, mean depths are ave. mid-point values except pools: taken at deepest part of pool.

<sup>b</sup> Composite sample of riffles and pools within the designated reach.

<sup>c</sup> Active bed of a riffle.

<sup>d</sup> Height of roughness feature above bed.

**Worksheet 2-1.** Gage station and field data (Rosgen and Silvey, 2007).

Summary.... <b>USGS GAGE STATION</b> Data/Records for <b>STREAM CHANNEL CLASSIFICATION</b>						
Station NAME:	Lower Rush River-1-1.10			Station Number:	N/A	
LOCATION:	Lower Rush River-1-1.10					
Period of RECORD:	N/A		yr/s	Mean Annual DISCHARGE:	N/A cfs	
Drainage AREA:	38009.6	acres	59.4	mi <sup>2</sup>	Drainage Area Mn ELEV:	880.9 ft
Reference REACH SLOPE:			ft/ft		Valley Type:	X
Stream Type:	B6c		HUC: _____			
"BANKFULL" CHARACTERISTICS						
Determined from FIELD MEASUREMENT			Determined from GAGE DATA Analysis			
Bankfull WIDTH ( $W_{bkf}$ )	45.3	ft	Bankfull WIDTH ( $W_{bkf}$ )		ft	
Bankfull Mean DEPTH ( $d_{bkf}$ )	1.8	ft	Bankfull MEAN DEPTH ( $d_{bkf}$ )		ft	
Bankfull Xsec AREA ( $A_{bkf}$ )	80.5	ft <sup>2</sup>	Bankfull Xsec AREA ( $A_{bkf}$ )		ft <sup>2</sup>	
Wetted PERIMETER ( $W_p$ )	45.8	ft	Wetted PERIMETER ( $W_p$ )		ft	
Bankfull STAGE (Gage Ht)		ft	Bankfull STAGE (Gage Ht)		ft	
Est. Mean VELOCITY ( $u$ )	0.8	ft/sec	Mean VELOCITY ( $u$ )		ft/sec	
Est. Bkf. DISCHARGE ( $Q_{bkf}$ )	65.0	cfs	Bankfull DISCHARGE ( $Q_{bkf}$ )		cfs	
Bankfull DISCHARGE associated with "field-determined" Bankfull STAGE				65.0	cfs	
Recurrence Interval ( Log-Pearson ) associated with "field-determined" Bankfull Discharge				1.1	yr/s	
From the Annual Peak Flow Frequency Analysis data for the Gage Station, determine:						
1.5 Year R.I. Discharge..... =	N/A	cfs	10 Year R.I. Discharge..... =	N/A	cfs	
2.0 Year R.I. Discharge.....=	N/A	cfs	25 Year R.I. Discharge.....=	N/A	cfs	
5.0 Year R.I. Discharge.....=	N/A	cfs	50 Year R.I. Discharge..... =	N/A	cfs	
MEANDER GEOMETRY						
Meander Length ( $L_m$ )		ft	Radius of Curvature ( $R_C$ )		ft	
Belt Width ( $W_{blt}$ )		ft	Meander Width Ratio ( $W_{blt}/W_{bkf}$ )	0.00	ft/ft	
HYDRAULIC GEOMETRY						
Based on <i>USGS Discharge Summary Notes</i> data ( Form 9-207 ) and regression analyses of measured discharge ( $Q$ ) with the hydraulic parameters of Width ( $W$ ), Area ( $A$ ), Mean Depth ( $d$ ) & Mean Velocity ( $u$ ), determine the <i>intercept coefficient</i> ( $a$ ) and the <i>slope exponent</i> ( $b$ ) values for a power function of the form $Y = aX^b$ , when $Y$ is one of the selected hydraulic parameters and $X$ is a given discharge value ( $Q$ ).						
	Width ( $W$ )	Depth ( $d$ )	Area ( $A$ )	Velocity ( $u$ )		
Intercept Coefficient: ( $a$ )						
Slope Exponent: ( $b$ )						
Hydraulic Radius: $R = A / W_p$		ft	Manning's "n" at Bankfull Stage	0.05	Coeff.	
$"n" = 1.4865 [ ( Area ) ( Hydraulic Radius^{2/3} ) ( Slope^{1/2} ) ] / Q_{bkf}$						

**Worksheet 2-2.** Computations of velocity and bankfull discharge using various methods (Rosgen, 2006b; Rosgen and Silvey, 2007).

Bankfull VELOCITY / DISCHARGE Estimates									
Site	Lower Rush River-1-1.10			Location	Lower Rush River-1-1.10				
Date	9/29/2011	Stream Type	B6c	Valley Type	X				
Observers	KP, AL			HUC	-- -- -- -- -- -- -- -- -- --				
INPUT VARIABLES				OUTPUT VARIABLES					
Bankfull Cross-sectional	80.5	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Mean DEPTH	1.8	$D_{bkf}$ (ft)				
Bankfull WIDTH	45.3	$W_{bkf}$ (ft)	Wetted PERIMETER ~ 2 * $d_{bkf}$ + $W_{bkf}$	48.9	$W_p$ (ft)				
$D_{84}$ @ Riffle	0.0022	Dia. (mm)	$D_{84}$ mm / 304.8 =	0.0	$D_{84}$ (ft)				
Bankfull SLOPE	0.0003	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	1.6	R (ft)				
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R (ft) / $D_{84}$ (ft)	228195					
Drainage AREA	59.4	DA (mi <sup>2</sup> )	Shear Velocity $u^* = \sqrt{gRS}$	0.1	$u^*$ (ft / sec)				
ESTIMATION METHODS				Bankfull VELOCITY		Bankfull DISCHARGE			
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66\text{Log}\{ R / D_{84} \} ] u^*$				4.5	ft / sec	360	cfs		
2. Roughness Coefficient: a) Manning's 'n' from friction factor / relative roughness (Figs. 2-18, 19) $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text"/>				0.8	ft / sec	62	cfs		
2. Roughness Coefficient: b) Manning's 'n' from Jarrett ( USGS ): $n = 0.39S^{-.38}R^{-.16}$ n = <input type="text"/> Note: This equation is for applications involving steep, step-pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for stream types A1, A2, A3, B1, B2, B3, C2 and E3.				2.2	ft / sec	178	cfs		
2. Roughness Coefficient: c) Manning's 'n' from Stream Type $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = .050				0.8	ft / sec	62	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.) HEC-RAS				0.8	ft / sec	65	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.)					ft / sec		cfs		
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge $Q = 1.46$ Yr. $u = Q / A$					ft / sec		cfs		
4. Continuity Equations: b) USGS Gage Data $u = Q / A$					ft / sec		cfs		
Options for using the $D_{84}$ term in the relative roughness relation (R/ $D_{84}$ ), when using estimation method 1.									
Option 1. For sand-bed channels: Measure the "protrusion height" ( $h_{sd}$ ) of sand dunes above channel bed elevations. Substitute an average sand dune protrusion height ( $h_{sd}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 2. For boulder-dominated channels: Measure several "protrusion heights" ( $h_{bo}$ ) of boulders above channel bed elevations. Substitute an ave. boulder protrusion height ( $h_{bo}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 3. For bedrock-dominated channels: Measure several "protrusion heights" ( $h_{br}$ ) of rock separations/steps/joints/uplifted surfaces above channel bed elevations. Substitute an average bedrock protrusion height ( $h_{br}$ in feet) for the $D_{84}$ term in estimation method 1.									

**Worksheet 2-3.** Field form for Level II stream classification (Rosgen, 1996; Rosgen , 2006b).

Stream: <b>Lower Rush River-1-1.10</b>	
Basin: <b>Red River Basin</b>	Drainage Area: <b>38010</b> acres <b>59.4</b> mi <sup>2</sup>
Location: <b>Lower Rush River-1-1.10</b>	
Twp.&Rge: - Sec.&Qtr.: -	
Cross-Section Monuments (Lat./Long.): - Date: <b>9/29/2011</b>	
Observers: <b>KP, AL</b> Valley Type: <b>X</b>	

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>45.3</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>1.8</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>80.5</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>25.5</b>	ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>2.9</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>72.2</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>1.6</b>	ft/ft
<b>Channel Materials (Particle Size Index ) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>&lt;0.001</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.0003</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).		

<b>Stream Type</b>	<b>B6c</b>	<b>See Classification Key (Figure 2-21)</b>
--------------------	------------	---

**Worksheet 2-4.** Morphological relations, including dimensionless ratios of river reach sites (Rosgen, 2006b; Rosgen and Silvey 2007).

Stream: <b>Lower Rush River-1-1.10</b>		Location: <b>Lower Rush River-1-1.10</b>								
Observers: <b>KP, AL</b>		Date: <b>9/29/2011</b>		Valley Type: <b>X</b>		Stream Type: <b>B6c</b>				
<b>River Reach Summary Data</b>										
<b>Channel Dimension</b>	Mean Riffle Depth ( $d_{bkt}$ )	<b>1.8</b>	ft	Riffle Width ( $W_{bkt}$ )	<b>45.3</b>	ft	Riffle Area ( $A_{bkt}$ )	<b>80.5</b>	ft <sup>2</sup>	
	Mean Pool Depth ( $d_{bkfp}$ )		ft	Pool Width ( $W_{bkfp}$ )		ft	Pool Area ( $A_{bkfp}$ )		ft <sup>2</sup>	
	Mean Pool Depth/Mean Riffle Depth		$d_{bkfp}/d_{bkt}$	Pool Width/Riffle Width		$W_{bkfp}/W_{bkt}$	Pool Area / Riffle Area		$A_{bkfp}/A_{bkt}$	
	Max Riffle Depth ( $d_{maxrif}$ )	<b>2.9</b>	ft	Max Pool Depth ( $d_{maxp}$ )		ft	Max Riffle Depth/Mean Riffle Depth	<b>1.6</b>		
	Max Pool Depth/Mean Riffle Depth			Point Bar Slope		ft/ft	Inner Berm Width ( $W_{ib}$ )		ft	
	Inner Berm Depth ( $d_{ib}$ )		ft	Inner Berm Width/Depth Ratio			$W_{ib}/d_{ib}$	Inner Berm Area ( $A_{ib}$ )		ft <sup>2</sup>
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )				<b>0.8</b>	ft/s	Estimation Method		<b>HEC-RAS</b>	
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )				<b>65</b>	cfs	Drainage Area		<b>59.4</b>	mi <sup>2</sup>

<b>Channel Pattern</b>	Geometry			Dimensionless Geometry Ratios			
	Mean	Min	Max	Mean	Min	Max	
	Meander Wavelength ( $L_m$ )	<b>0</b>			ft	Meander Length Ratio ( $L_m/W_{bkt}$ )	<b>0.0</b>
	Radius of Curvature ( $R_c$ )	<b>0</b>			ft	Radius of Curvature/Riffle Width ( $R_c/W_{bkt}$ )	<b>0.0</b>
	Belt Width ( $W_{bit}$ )	<b>0</b>			ft	Meander Width Ratio ( $W_{bit}/W_{bkt}$ )	<b>0.0</b>
	Individual Pool Length				ft	Pool Length/Riffle Width	
	Pool to Pool Spacing				ft	Pool to Pool Spacing/Riffle Width	
Riffle Length				ft	Riffle Length/Riffle Width		

<b>Channel Profile</b>	Valley Slope (VS)		ft/ft	Average Water Surface Slope (S)		ft/ft	Sinuosity (VS/S)		
	Stream Length (SL)	<b>37133</b>	ft	Valley Length (VL)	<b>29667</b>	ft	Sinuosity (SL/VL)	<b>1.3</b>	
	Low Bank Height (LBH)	start: end:	ft	Max Riffle Depth	start: end:	ft	Bank-Height Ratio (BHR) (LBH/Max Riffle Depth)	start: end:	
	Facet Slopes			Dimensionless Slope Ratios			Mean	Min	Max
	Riffle Slope ( $S_{rif}$ )	<b>0.0</b>		ft/ft	Riffle Slope/Average Water Surface Slope ( $S_{rif} / S$ )	<b>1.0</b>			
	Run Slope ( $S_{run}$ )			ft/ft	Run Slope/Average Water Surface Slope ( $S_{run} / S$ )				
	Pool Slope ( $S_p$ )			ft/ft	Pool Slope/Average Water Surface Slope ( $S_p / S$ )				
	Glide Slope ( $S_g$ )			ft/ft	Glide Slope/Average Water Surface Slope ( $S_g / S$ )				
	Feature Midpoint <sup>a</sup>			Dimensionless Depth Ratios			Mean	Min	Max
	Max Riffle Depth ( $d_{maxrif}$ )	<b>2.9</b>		ft	Max Riffle Depth/Mean Riffle Depth ( $d_{maxrif} / d_{bkt}$ )	<b>1.6</b>			
	Max Run Depth ( $d_{maxrun}$ )			ft	Max Run Depth/Mean Riffle Depth ( $d_{maxrun} / d_{bkt}$ )				
	Max Pool Depth ( $d_{maxp}$ )			ft	Max Pool Depth/Mean Riffle Depth ( $d_{maxp} / d_{bkt}$ )				
	Max Glide Depth ( $d_{maxg}$ )			ft	Max Glide Depth/Mean Riffle Depth ( $d_{maxg} / d_{bkt}$ )				

<b>Channel Materials</b>	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Protrusion Height <sup>d</sup>	
	% Silt/Clay	<b>99</b>			$D_{16}$	<b>&lt;0.001</b>		mm
	% Sand	<b>1</b>			$D_{35}$	<b>&lt;0.001</b>		mm
	% Gravel	<b>0</b>			$D_{50}$	<b>&lt;0.001</b>		mm
	% Cobble	<b>0</b>			$D_{84}$	<b>0.0022</b>		mm
	% Boulder	<b>0</b>			$D_{95}$	<b>0.028</b>		mm
	% Bedrock	<b>0</b>			$D_{100}$	<b>0.2</b>		mm

<sup>a</sup> Min, max, mean depths are ave. mid-point values except pools: taken at deepest part of pool.

<sup>b</sup> Composite sample of riffles and pools within the designated reach.

<sup>c</sup> Active bed of a riffle.

<sup>d</sup> Height of roughness feature above bed.

**Worksheet 2-1.** Gage station and field data (Rosgen and Silvey, 2007).

Summary.... <b>USGS GAGE STATION</b> Data/Records for <b>STREAM CHANNEL CLASSIFICATION</b>					
Station NAME:	Wolverton Creek-2-2.02			Station Number:	N/A
LOCATION:	Wolverton Creek-2-2.02				
Period of RECORD:	N/A	yrs	Mean Annual DISCHARGE:	N/A	cfs
Drainage AREA:	63443.2	acres	99.13	mi <sup>2</sup>	Drainage Area Mn ELEV: 893.45 ft
Reference REACH SLOPE:		ft/ft	Valley Type:	X	
Stream Type:	E6		HUC:	_ _ _ _ _	
"BANKFULL" CHARACTERISTICS					
Determined from FIELD MEASUREMENT			Determined from GAGE DATA Analysis		
Bankfull WIDTH ( $W_{bkf}$ )	24.2	ft	Bankfull WIDTH ( $W_{bkf}$ )		ft
Bankfull Mean DEPTH ( $d_{bkf}$ )	3.2	ft	Bankfull MEAN DEPTH ( $d_{bkf}$ )		ft
Bankfull Xsec AREA ( $A_{bkf}$ )	73.1	ft <sup>2</sup>	Bankfull Xsec AREA ( $A_{bkf}$ )		ft <sup>2</sup>
Wetted PERIMETER ( $W_p$ )	27.4	ft	Wetted PERIMETER ( $W_p$ )		ft
Bankfull STAGE (Gage Ht)		ft	Bankfull STAGE (Gage Ht)		ft
Est. Mean VELOCITY ( $u$ )	1.8	ft/sec	Mean VELOCITY ( $u$ )		ft/sec
Est. Bkf. DISCHARGE ( $Q_{bkf}$ )	130.0	cfs	Bankfull DISCHARGE ( $Q_{bkf}$ )		cfs
Bankfull DISCHARGE associated with "field-determined" Bankfull STAGE				130.0	cfs
Recurrence Interval ( Log-Pearson ) associated with "field-determined" Bankfull Discharge				1.2	yrs
From the Annual Peak Flow Frequency Analysis data for the Gage Station, determine:					
1.5 Year R.I. Discharge..... =	N/A	cfs	10 Year R.I. Discharge..... =	N/A	cfs
2.0 Year R.I. Discharge.....=	N/A	cfs	25 Year R.I. Discharge.....=	N/A	cfs
5.0 Year R.I. Discharge.....=	N/A	cfs	50 Year R.I. Discharge..... =	N/A	cfs
MEANDER GEOMETRY					
Meander Length ( $L_m$ )	625	ft	Radius of Curvature ( $R_C$ )	171.0	ft
Belt Width ( $W_{blt}$ )	207	ft	Meander Width Ratio ( $W_{blt}/W_{bkf}$ )	8.6	ft/ft
HYDRAULIC GEOMETRY					
Based on <i>USGS Discharge Summary Notes</i> data ( Form 9-207 ) and regression analyses of measured discharge ( $Q$ ) with the hydraulic parameters of Width ( $W$ ), Area ( $A$ ), Mean Depth ( $d$ ) & Mean Velocity ( $u$ ), determine the <i>intercept coefficient</i> ( $a$ ) and the <i>slope exponent</i> ( $b$ ) values for a power function of the form $Y = aX^b$ , when $Y$ is one of the selected hydraulic parameters and $X$ is a given discharge value ( $Q$ ).					
	Width ( $W$ )	Depth ( $d$ )	Area ( $A$ )	Velocity ( $u$ )	
Intercept Coefficient: ( $a$ )					
Slope Exponent: ( $b$ )					
Hydraulic Radius: $R = A / W_p$		ft	Manning's "n" at Bankfull Stage	0.035	Coeff.
$"n" = 1.4865 [ ( Area ) ( Hydraulic Radius^{2/3} ) ( Slope^{1/2} ) ] / Q_{bkf}$					

**Worksheet 2-2.** Computations of velocity and bankfull discharge using various methods (Rosgen, 2006b; Rosgen and Silvey, 2007).

Bankfull VELOCITY / DISCHARGE Estimates									
Site	Wolverton Creek-2-2.02			Location	Wolverton Creek-2-2.02				
Date	9/28/2011	Stream Type	E6	Valley Type	X				
Observers	KP, AL			HUC	-- -- -- -- -- -- -- -- -- --				
INPUT VARIABLES				OUTPUT VARIABLES					
Bankfull Cross-sectional	73.1	$A_{bkf}$ (ft <sup>2</sup> )	Bankfull Mean DEPTH	3.2	$D_{bkf}$ (ft)				
Bankfull WIDTH	24.2	$W_{bkf}$ (ft)	Wetted PERIMETER ~ 2 * $d_{bkf}$ + $W_{bkf}$	30.5	$W_p$ (ft)				
$D_{84}$ @ Riffle	0.039	Dia. (mm)	$D_{84}$ mm / 304.8 =	0.00	$D_{84}$ (ft)				
Bankfull SLOPE	0.0011	$S_{bkf}$ (ft / ft)	Hydraulic RADIUS $A_{bkf} / W_p$	2.4	R (ft)				
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness R (ft) / $D_{84}$ (ft)	18714					
Drainage AREA	99.1	DA (mi <sup>2</sup> )	Shear Velocity $u^* = \sqrt{gRS}$	0.3	$u^*$ (ft / sec)				
ESTIMATION METHODS				Bankfull VELOCITY		Bankfull DISCHARGE			
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 \text{Log}\{ R / D_{84} \} ] u^*$				7.9	ft / sec	575	cfs		
2. Roughness Coefficient: a) Manning's 'n' from friction factor / relative roughness (Figs. 2-18, 19) $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text"/>				2.5	ft / sec	184	cfs		
2. Roughness Coefficient: $u = 1.4865 * R^{2/3} * S^{1/2} / n$ b) Manning's 'n' from Jarrett ( USGS ): $n = 0.39S^{-.38}R^{-.16}$ n = <input type="text"/>				3.5	ft / sec	253	cfs		
Note: This equation is for applications involving steep, step-pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for stream types A1, A2, A3, B1, B2, B3, C2 and E3.									
2. Roughness Coefficient: c) Manning's 'n' from Stream Type $u = 1.4865 * R^{2/3} * S^{1/2} / n$ n = <input type="text" value="0.035"/>				2.5	ft / sec	184	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.) HEC-RAS				1.8	ft / sec	130	cfs		
3. Other Methods (Hev. Darcy-Weisbach, Chezy C. etc.)					ft / sec		cfs		
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge Q = <input type="text" value="1.46"/> Yr. $u = Q / A$					ft / sec		cfs		
4. Continuity Equations: b) USGS Gage Data $u = Q / A$					ft / sec		cfs		
Options for using the $D_{84}$ term in the relative roughness relation ( $R/D_{84}$ ), when using estimation method 1.									
Option 1. For sand-bed channels: Measure the "protrusion height" ( $h_{sd}$ ) of sand dunes above channel bed elevations. Substitute an average sand dune protrusion height ( $h_{sd}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 2. For boulder-dominated channels: Measure several "protrusion heights" ( $h_{bo}$ ) of boulders above channel bed elevations. Substitute an ave. boulder protrusion height ( $h_{bo}$ in ft) for the $D_{84}$ term in est. method 1.									
Option 3. For bedrock-dominated channels: Measure several "protrusion heights" ( $h_{br}$ ) of rock separations/steps/joints/uplifted surfaces above channel bed elevations. Substitute an average bedrock protrusion height ( $h_{br}$ in feet) for the $D_{84}$ term in estimation method 1.									

**Worksheet 2-3.** Field form for Level II stream classification (Rosgen, 1996; Rosgen, 2006b).

Stream: <b>Wolverton Creek-2-2.02</b>	
Basin: <b>Red River Basin</b>	Drainage Area: <b>63443</b> acres <b>99.13</b> mi <sup>2</sup>
Location: <b>Wolverton Creek-2-2.02</b>	
Twp.&Rge: - Sec.&Qtr.: -	
Cross-Section Monuments (Lat./Long.): - Date: <b>9/28/2011</b>	
Observers: <b>KP, AL</b> Valley Type: <b>X</b>	

<b>Bankfull WIDTH (<math>W_{bkf}</math>)</b> WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	<b>24.2</b>	ft
<b>Bankfull DEPTH (<math>d_{bkf}</math>)</b> Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section ( $d_{bkf} = A / W_{bkf}$ ).	<b>3.2</b>	ft
<b>Bankfull X-Section AREA (<math>A_{bkf}</math>)</b> AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	<b>73.1</b>	ft <sup>2</sup>
<b>Width/Depth Ratio (<math>W_{bkf} / d_{bkf}</math>)</b> Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	<b>7.6</b>	ft/ft
<b>Maximum DEPTH (<math>d_{mbkf}</math>)</b> Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	<b>4.8</b>	ft
<b>WIDTH of Flood-Prone Area (<math>W_{fpa}</math>)</b> Twice maximum DEPTH, or ( $2 \times d_{mbkf}$ ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	<b>129.0</b>	ft
<b>Entrenchment Ratio (ER)</b> The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa} / W_{bkf}$ ) (riffle section).	<b>5.3</b>	ft/ft
<b>Channel Materials (Particle Size Index) <math>D_{50}</math></b> The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	<b>0.0016</b>	mm
<b>Water Surface SLOPE (S)</b> Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	<b>0.0011</b>	ft/ft
<b>Channel SINUOSITY (k)</b> Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).	<b>1.3</b>	

<div style="border: 1px solid black; padding: 5px; display: inline-block;"> <b>Stream Type</b> </div>	<div style="border: 1px solid black; padding: 5px; display: inline-block; background-color: yellow;"> <b>E6</b> </div>	<div style="border: 1px solid black; padding: 5px; display: inline-block;"> <b>See Classification Key (Figure 2-21)</b> </div>
---	--	--

**Worksheet 2-4.** Morphological relations, including dimensionless ratios of river reach sites (Rosgen, 2006b; Rosgen and Silvey 2007).

Stream: <b>Wolverton Creek-2-2.02</b>		Location: <b>Wolverton Creek-2-2.02</b>								
Observers: <b>KP, AL</b>		Date: <b>9/28/2011</b>		Valley Type: <b>X</b>		Stream Type: <b>E6</b>				
<b>River Reach Summary Data</b>										
<b>Channel Dimension</b>	Mean Riffle Depth ( $d_{bkt}$ )	<b>3.2</b>	ft	Riffle Width ( $W_{bkt}$ )	<b>24.2</b>	ft	Riffle Area ( $A_{bkt}$ )	<b>73.1</b>	ft <sup>2</sup>	
	Mean Pool Depth ( $d_{bkfp}$ )		ft	Pool Width ( $W_{bkfp}$ )		ft	Pool Area ( $A_{bkfp}$ )		ft <sup>2</sup>	
	Mean Pool Depth/Mean Riffle Depth		$d_{bkfp}/d_{bkt}$	Pool Width/Riffle Width		$W_{bkfp}/W_{bkt}$	Pool Area / Riffle Area		$A_{bkfp}/A_{bkt}$	
	Max Riffle Depth ( $d_{maxrif}$ )	<b>4.8</b>	ft	Max Pool Depth ( $d_{maxp}$ )		ft	Max Riffle Depth/Mean Riffle Depth	<b>1.5</b>		
	Max Pool Depth/Mean Riffle Depth			Point Bar Slope		ft/ft	Inner Berm Width ( $W_{ib}$ )		ft	
	Inner Berm Depth ( $d_{ib}$ )		ft	Inner Berm Width/Depth Ratio			$W_{ib}/d_{ib}$	Inner Berm Area ( $A_{ib}$ )		ft <sup>2</sup>
	Streamflow: Estimated Mean Velocity at Bankfull Stage ( $u_{bkt}$ )			<b>1.8</b>	ft/s	Estimation Method	<b>HEC-RAS</b>			
	Streamflow: Estimated Discharge at Bankfull Stage ( $Q_{bkt}$ )			<b>130</b>	cfs	Drainage Area	<b>99.1</b>	mi <sup>2</sup>		

<b>Channel Pattern</b>	Geometry			Dimensionless Geometry Ratios			
	Mean	Min	Max	Mean	Min	Max	
	Meander Wavelength ( $L_m$ )	<b>625</b>			ft	Meander Length Ratio ( $L_m/W_{bkt}$ )	<b>25.8</b>
	Radius of Curvature ( $R_c$ )	<b>171</b>			ft	Radius of Curvature/Riffle Width ( $R_c/W_{bkt}$ )	<b>7.1</b>
	Belt Width ( $W_{bit}$ )	<b>207</b>			ft	Meander Width Ratio ( $W_{bit}/W_{bkt}$ )	<b>8.6</b>
	Individual Pool Length				ft	Pool Length/Riffle Width	
	Pool to Pool Spacing				ft	Pool to Pool Spacing/Riffle Width	
Riffle Length				ft	Riffle Length/Riffle Width		

<b>Channel Profile</b>	Valley Slope (VS)		ft/ft	Average Water Surface Slope (S)		ft/ft	Sinuosity (VS/S)		
	Stream Length (SL)	<b>23172</b>	ft	Valley Length (VL)	<b>18342</b>	ft	Sinuosity (SL/VL)	<b>1.3</b>	
	Low Bank Height (LBH)	start	ft	Max Riffle Depth	start	ft	Bank-Height Ratio (BHR)	start	
		end	ft		end	ft	(LBH/Max Riffle Depth)	end	
	Facet Slopes			Dimensionless Slope Ratios			Mean	Min	Max
	Riffle Slope ( $S_{rif}$ )	<b>0.0</b>		ft/ft	Riffle Slope/Average Water Surface Slope ( $S_{rif}/S$ )	<b>1.0</b>			
	Run Slope ( $S_{run}$ )			ft/ft	Run Slope/Average Water Surface Slope ( $S_{run}/S$ )				
	Pool Slope ( $S_p$ )			ft/ft	Pool Slope/Average Water Surface Slope ( $S_p/S$ )				
	Glide Slope ( $S_g$ )			ft/ft	Glide Slope/Average Water Surface Slope ( $S_g/S$ )				
	Feature Midpoint <sup>a</sup>			Dimensionless Depth Ratios			Mean	Min	Max
	Max Riffle Depth ( $d_{maxrif}$ )	<b>4.8</b>		ft	Max Riffle Depth/Mean Riffle Depth ( $d_{maxrif}/d_{bkt}$ )	<b>1.5</b>			
	Max Run Depth ( $d_{maxrun}$ )			ft	Max Run Depth/Mean Riffle Depth ( $d_{maxrun}/d_{bkt}$ )				
Max Pool Depth ( $d_{maxp}$ )			ft	Max Pool Depth/Mean Riffle Depth ( $d_{maxp}/d_{bkt}$ )					
Max Glide Depth ( $d_{maxg}$ )			ft	Max Glide Depth/Mean Riffle Depth ( $d_{maxg}/d_{bkt}$ )					

<b>Channel Materials</b>	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Reach <sup>b</sup>	Riffle <sup>c</sup>	Bar	Protrusion Height <sup>d</sup>	
	% Silt/Clay	<b>91</b>			$D_{16}$	<b>&lt;.001</b>		mm
	% Sand	<b>9</b>			$D_{35}$	<b>&lt;.001</b>		mm
	% Gravel	<b>0</b>			$D_{50}$	<b>0.0016</b>		mm
	% Cobble	<b>0</b>			$D_{84}$	<b>0.039</b>		mm
	% Boulder	<b>0</b>			$D_{95}$	<b>0.22</b>		mm
	% Bedrock	<b>0</b>			$D_{100}$	<b>4.75</b>		mm

<sup>a</sup> Min, max, mean depths are ave. mid-point values except pools: taken at deepest part of pool.

<sup>b</sup> Composite sample of riffles and pools within the designated reach.

<sup>c</sup> Active bed of a riffle.

<sup>d</sup> Height of roughness feature above bed.